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| Re : | IEEE 802.16m-08/016 - Call for Contributions on Project 802.16m System Description Document (SDD), shoot for "Hybrid ARQ (protocol and timing)" topic. |
| Abstract | We apply a signal constellation rearrangement to the Chase combining scheme for the HARQ scheme supported in IEEE802.16e. We present the basic idea of the proposed scheme and evaluate the packet error rate performance. The performance of the proposed scheme can be drastically improved for both 16QAM and 64QAM. |
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# Enhanced HARQ scheme with Signal Constellation Rearrangement 

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## 1. Introduction

Chase combining (CC) [1] is one of the HARQ schemes supported in IEEE802.16e [2]. In this contribution, we present a HARQ bit-mapping scheme, called "signal constellation rearrangement (CoRe)" for CC in the case of 16QAM and 64QAM [3][4].
The proposed scheme "CC with CoRe" shows a significant performance gain with respect to the original CC without CoRe. Therefore, CoRe should be included in the system description document (SDD).

## 2. Signal constellation rearrangement for quadrature amplitude modulation

### 2.1. Basic idea

The $2^{M}$-QAM modulated symbol consists of $M$-bits. For the $2^{M}$-QAM with $M$ larger than 2 (e.g. 8QAM (PSK),16QAM, 64QAM, 256QAM,...), the reliabilities of the bits Gray-mapped onto the modulated symbol vary from the most significant bits (MSBs) $i_{1}$ and $q_{1}$ to the least significant bits (LSBs) $i_{2}$ and $q_{2}$ as shown in Figure 1 and in the Appendix. As the reliability variations between these two different kinds of bits increase, the error rate performance is getting worse with respect to having equal bit reliabilities. Considering a HARQ scheme retransmitting (at least partially) identical symbols and employing an identical signal constellation and mapping for all transmissions, the variations in bit reliabilities increase over retransmissions (i.e. the original CC). Particularly, this is the case when soft-combining the received packets by maximal ratio combining (MRC) at modulation symbol level or by adding LLRs at bit level. By rearranging the signal constellations for retransmissions the proposed scheme averages out the bit reliabilities over the retransmissions.

### 2.1.1.Signal constellation rearrangement for 16QAM and 64QAM

Figure 1 shows the signal constellation in the case of 16QAM supported in IEEE802.16e. The bit $i_{1}, i_{2}, q_{1}$ and $q_{2}$, is located to the $1^{\text {st }}$ bit, $2^{\text {nd }}$ bit, $3^{\text {rd }}$ bit and $4^{\text {th }}$ bit (i.e. $i_{1} i_{2} q_{1} q_{2}$ ) within a symbol. Due to Gray-mapping bit $i_{1}$ and $q_{1}$ is on average more reliable than $i_{2}$ and $q_{2}$.


Figure 1. Signal constellation with Gray-mapping in the case of 16QAM

As we present in the previous section 2.1, there are variations in the mean bit reliabilities depending on the significance of the bit within a symbol. Therefore, we use the simple rearrangement rule such as reordering and inversion of the logical bit values according to Table 1 to average out the bit reliabilities over the retransmissions.

Table 1. Rearrangement rule for each transmission in the case of 16QAM

| Transmissio <br> $\mathbf{n}$ No. | Bit pattern | Explanation |
| :---: | :---: | :--- |
| 1 | $i_{1} i_{2} q_{1} q_{2}$ | - None |
| 2 | $i_{2} \bar{i}_{1} q_{2} \bar{q}_{1}$ | - Swapping $i_{1}$ with $i_{2}$ and $q_{1}$ with $q_{2} /$ logical inversion of $i_{1}$ and $q_{1}$ |
| 3 | $i_{2} i_{1} q_{2} q_{1}$ | - Swapping $i_{1}$ with $i_{2}$ and $q_{1}$ with $q_{2}$ |
| 4 | $i_{1} \bar{i}_{2} q_{1} \bar{q}_{2}$ | - Logical inversion of $i_{2}$ and $q_{2}$ |
| Further <br> transmission |  | - Repeatedly using the signal constellations form $1^{\text {st }}-4^{\text {th }}$ transmissions |

The same rearrangement rule as 16QAM can be applicable for 64QAM. In this case there are 3 levels of bit reliabilities. Figure 2 shows the signal constellation in the case of 64QAM supported in IEEE802.16e and Table 2 shows the rearrangement rule for each transmission in the case of 64QAM.


Figure 2. Signal constellation with Gray-mapping in the case of 64QAM

Table 2. Rearrangement rule for each transmission in the case of 64QAM

| Transmissio <br> n No. | Bit pattern | Explanation |
| :---: | :---: | :--- |
| 1 | $i_{1} i_{2} i_{3} q_{1} q_{2} q_{3}$ | - None <br> 2 |
| $i_{2} i_{3} q_{1} q_{2} q_{3} q_{1}$ | 1-bit circular shift for the in-phase and orthogonal components <br> individually |  |
| 3 | $i_{3} i_{1} i_{2} q_{3} q_{1} q_{2}$ | -2-bits circular shift for the in-phase and orthogonal components <br> individually <br> 4 <br> $i_{1} \bar{i}_{2} \bar{i}_{3} q_{1} \bar{q}_{2} \bar{q}_{3}$- Logical inversion of $i_{2}, i_{3}, q_{2}$ and $q_{3}$ <br> 6$i_{2} \bar{i}_{3} \bar{i}_{1} q_{2} \bar{q}_{3} \bar{q}_{1}$ |
| - 1-bit circular shift for the in-phase and orthogonal components <br> individually <br> - Logical inversion of $i_{1}, i_{3}, q_{1}$ and $q_{3}$ |  |  |
| Further <br> transmission | $i_{3} \bar{i} \bar{i}_{2} q_{3} \bar{q}_{1} \bar{q}_{2}$ | - 2-bits circular shift for the in-phase and orthogonal components <br> individually <br> - Logical inversion of $i_{1}, i_{2}, q_{1}$ and $q_{2}$ |

## 3. Simulation results

Table 3 provides a list of simulation parameters.

Table 3. Simulation parameters

| Parameter | Value |
| :---: | :---: |
| Carrier frequency | 2.5 Ghz |
| System bandwidth | 10 MHz |
| FFT size | 1024 |
| Sub-carrier frequency spacing $\left(f_{s}\right)$ | 10.94 kHz |
| Useful symbol interval $\left(T_{s}=1 / f_{s}\right)$ | 91.4 usec |
| Guard interval $\left(T_{s}=T_{s} / 8\right)$ | 11.4 usec |
| Number of information bits for packet | 128bits(16QAM) / 192bits(64QAM) |
| Antenna configuration | 1 -by-1 |
| Channel coding | Turbo coding (original rate $=1 / 3)$ |
| MCS | 16QAM/64QAM, R=1/2 |
| Channel model | AWGN |
| Channel estimation | Ideal |
| Maximum number of transmissions | 4(16QAM) / 6(64QAM) |

### 3.1. Comparison between the original chase combining and the chase combining with constellation rearrangement in the case of 16QAM

Figure 3 shows the packet error rate (PER) performance as a function of the average received signal energy per information bit-to-AWGN power spectrum density ratio ( $\mathrm{E}_{\mathrm{b}} / \mathrm{N}_{0}$ ) with the number of transmission as a parameter in the case of 16QAM. The performance gain for $\mathrm{PER}=10^{-1}$ of the CC with CoRe over the original CC is about 1.4 dB for the $2^{\text {nd }}$ transmission, about 2.1 dB for the $3^{\text {rd }}$ transmission and about 2.9 dB for the $4^{\text {th }}$ transmission. The performance gain is increasing in proportion to the number of transmissions, because the effect of averaging out the reliabilities is improved.


Figure 3. Packet error rate vs. average received $E_{b} / N_{0}$ in the case of 16QAM

### 3.2. Comparison between the original Chase combining and the Chase combining with constellation rearrangement in the case of 64QAM

Figure 4 shows the PER performance as a function of the average received $E_{b} / N_{0}$ with the number of transmission as a parameter in the case of 64QAM. The performance gain for $\mathrm{PER}=10^{-1}$ of the CC with CoRe over the original CC is about 2.1 dB for the $2^{\text {nd }}$ transmission, about 3.2 dB for the $3^{\text {rd }}$ transmission, about 4.5 dB for the $4^{\text {th }}$ transmission, about 5.4 dB for the $5^{\text {th }}$ transmission and about 6.0 dB for the $6^{\text {th }}$ transmission. The performance gain is improved proportionally to the number of transmissions for the same reason as for the 16QAM case.


Figure 4. Packet error rate vs. average received $E_{b} / N_{0}$ in the case of 64QAM

### 3.3. Performance gain with constellation rearrangement comparison between 16QAM-case and 64QAM-case

Table 4 shows a performance gain for $\mathrm{PER}=10^{-1}$ of the CC with CoRe over the original CC both in the case of 16QAM and 64QAM. From Table X it can be observed that a performance gain in the case of 64-QAM is larger than that in the case of 16QAM for each transmission. In a word, CoRe is more effective in higher modulation level (or higher coding rate).

Table. 4 Diversity gain with CoRe comparison between 16QAM-case and 64QAM-case for PER=10 ${ }^{-1}$

| Number of transmissions | 16QAM | 64QAM |
| :---: | :---: | :---: |
| $1^{\text {st }}$ transmission | 0 dB | 0 dB |
| $2^{\text {nd }}$ transmission | 1.4 dB | 2.1 dB |
| $3^{\text {rd }}$ transmission | 2.1 dB | 3.2 dB |
| $4^{\text {th }}$ transmission | 2.9 dB | 4.5 dB |
| $5^{\text {th }}$ transmission |  | 5.4 dB |
| $6^{\text {th }}$ transmission |  | 6.0 dB |

## 4. Conclusion

In this contribution a Chase combining scheme with signal constellation rearrangement is presented. By averaging out the bit reliabilities over the retransmissions, CC with CoRe shows a significantly improved packet error rate performance compared to the original CC for both 16QAM and 64QAM. The performance gain is improving with an increasing number of retransmissions, especially in the case of 64QAM.

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We proved the efficiency of applying the CoRe to the CC. Therefore, CC with CoRe shall be described in the SDD as shown below.

## Begin Proposed Text

X. HARQ

A Chase combining scheme with signal constellation rearrangement for 16QAM and 64QAM modulation shall be used.

End of Text Proposal

## 5. Reference

[1] D. Chase, "Code combining: A maximum-likelihood decoding approach for combining an arbitrary number of noisy packets," IEEE Trans. Commun., Vol. COM-33, pp. 385-393, May 1985.
[2] IEEE Std. 802.16e-2005, "Part 16: Air Interface for Broadband Wireless Access Systems," Approved 7 December 2005.
[3] 802.16m-07/292r1, ITRI, "Enhanced HARQ technique using Constellation Rearrangement"
[4] R1-01-0237, Panasonic, "enhanced HARQ method with signal constellation rearrangement, " 3GPP TSG RAN WG1, Las Vegas, USA February 27- March 2, 2001.
[5] S. Le Goff, A. Glavieux, C. Berrou, "Turbo-codes and high spectral efficiency modulation," IEEE SUPERCOMM/ICC '94, vol.2, pp.645-649, 1994
[6] Ch. Wengerter, A. Golitschek Edler von Elbwart, E. Seidel, G. Velev, M.P. Schmitt, "Advanced hybrid ARQ technique employing a signal constellation rearrangement," IEEE VTC 2002 Fall, vol. 4, pp. 2002-2006, 2002.

## 6. Appendix

One possible implementation described in Section 2.2 is to use the same the signal constellation for all transmissions as shown in Figure 1 and reorder and inverse the logical bit values according to Table 1. There is another implementation that the ordering of the bit-to-symbol mapping is identical for all transmissions, however, the signal constellations for each transmission are changed. In this section we analyze the advantageous effect of the $L L R$ averaging for the quadrature amplitude modulation, based on this implementation in the case of 16QAM and 64QAM. It is noted that this implementation can achieve an identical averaging of the bit reliabilities as described in Section 2.

The $L L R$ which is a soft-metric for the reliability of a demodulated bit $b(=0$ or 1$)$ from a received modulation symbol $r=x+j y$ is defined as follows[5],

$$
L L R\left(b_{p}\right)=\ln \frac{\operatorname{Pr}(b=1 \mid r)}{\operatorname{Pr}(b=0 \mid r)},(1)
$$

where $p$ in $b_{p}$ denotes the bit position. As can be seen from Figure 1, the mappings of the in-phase component bits and the quadrature component bits on the signal constellation are orthogonal. Therefore, it is sufficient to focus on the in-phase component bits $i_{1}$ and $i_{2}$. The same conclusions then apply for $q_{1}$ and $q_{2}$. The $L L R$ is given by the following equations [6],

$$
L L R\left(b_{p}\right)=\ln \frac{\operatorname{Pr}(b=1 \mid r)}{\operatorname{Pr}(b=0 \mid r)}=\ln \left[\frac{\sum_{b=1} \exp \left(-K\left(x-x_{k}^{(1)}\right)^{2}\right)}{\sum_{b=0}^{\exp }\left(-K\left(x-x_{k}^{(0)}\right)^{2}\right)}\right],(1)
$$

where $x$ denotes the in-phase component of the normalized received modulation symbol $r, x_{k}^{(b)}$ denotes the in-phase component of the normalized transmit modulation symbol and $K$ is a factor proportional to the signal-to-noise ratio(SNR).
By using the following approximation,

$$
\begin{equation*}
\ln \left[\left(-\sum_{b=1} \exp \left(z_{j}\right)\right)\right] \approx \max \left(-z_{j}\right)=\min \left(z_{j}\right), \tag{2}
\end{equation*}
$$

equation (1) can be approximated by the following equation,

$$
\begin{align*}
\operatorname{LLR}\left(b_{p}\right) & \approx K\left[\min _{b=0}\left|x-x_{k}^{(0)}\right|^{2}-\min _{b=1}\left|x-x_{k}^{(1)}\right|^{2}\right] \\
& =K\left[\min _{b=0}\left(x_{k}^{(0)^{2}}-2 x_{k}^{(0)} x\right)-\min _{b=1}\left(x_{k}^{(1)^{2}}-2 x_{k}^{(1)} x\right)\right] . \tag{3}
\end{align*}
$$

### 6.1. 16QAM case

Under the assumption of a uniform signal constellation $x_{1}=3 x_{0}$ in the case of 16QAM equations (1) can be fairly good approximated by the following equations.

$$
\begin{align*}
& \operatorname{LLR}\left(b=i_{1}\right) \approx\left\{\begin{array}{cc}
-8 K x_{0} x-8 K x_{0}{ }^{2} & ,\left(x<-2 x_{0}\right) \\
-4 K x_{0} x & ,\left(-2 x_{0} \leq x<2 x_{0}\right) \\
-8 K x_{0} x+8 K x_{0}^{2} & ,\left(2 x_{0} \leq x\right)
\end{array},\right.  \tag{4}\\
& \operatorname{LLR}\left(b=i_{2}\right) \approx\left\{\begin{array}{c}
4 K x_{0} x-8 K x_{0}{ }^{2}, \\
-4<0) \\
-4 K x_{0} x-8 K x_{0}^{2},(0 \leq x)
\end{array}\right.
\end{align*}
$$

Table 5 shows the mean $L L R$ s for bits mapped on the in-phase component of the signal constellation for the mapping in the case of 16QAM as shown in figure 1 according to equation (3) (substituting $4 K x_{0}^{2}$ by A). In case of transmitted modulation symbols $01 q_{1} q_{2}$ and $11 q_{1} q_{2}$, where $q_{1}$ and $q_{2}$ are arbitrary, the magnitude of the mean $\operatorname{LLR}\left(i_{1}\right)$ is higher than of the mean $\operatorname{LLR}\left(i_{2}\right)$. This represents that the actual $\operatorname{LLR}$ for $i_{1}$ depends on the content of $i_{2}$; e.g. in Figure $1 i_{1}$ has a higher mean reliability in case the logical value for $i_{2}$ is equal to " 1 " (the leftmost and rightmost columns). Hence, assuming a uniform distribution of transmitted modulation symbols, on average, $50 \%$ of the MSBs $i_{1}$ have about three times the magnitude in $L L R$ of $i_{2}$.

Table 5. Mean LLRs for bits mapped on the in-phase component of the signal constellation for the mapping in figure 1 accoding to equation (3)

| Symbol $\left(\boldsymbol{i}_{1} \boldsymbol{i}_{2} q_{1} q_{\mathbf{2}}\right)$ | Mean value of $\boldsymbol{x}$ | Mean $\boldsymbol{L L R}\left(\boldsymbol{i}_{\mathbf{1}}\right)$ | Mean $\boldsymbol{L L R}\left(\boldsymbol{i}_{\mathbf{2}}\right)$ |
| :---: | :---: | :---: | :---: |
| $00 q_{1} q_{2}$ | $x_{0}$ | $-4 K x_{0}^{2}=-A$ | $-4 K x_{0}^{2}=-A$ |
| $01 q_{1} q_{2}$ | $x_{1}$ | $-16 K x_{0}^{2}=-4 A$ | $4 K x_{0}^{2}=A$ |
| $10 q_{1} q_{2}$ | $-x_{0}$ | $4 K x_{0}^{2}=A$ | $-4 K x_{0}^{2}=-A$ |
| $11 q_{1} q_{2}$ | $-x_{1}$ | $16 K x_{0}^{2}=4 A$ | $4 K x_{0}^{2}=A$ |

From Table 5 it can be observed that there are variations in the mean bit reliabilities for multilevel modulation formats depending on the significance of the bit within a symbol and on the content of the transmitted modulation symbol.
Figure 5 shows the signal constellation in the case of 16QAM for each transmission and Table 6 shows $L L R \mathrm{~s}$ for bits mapped on the in-phase component of the signal constellation according to the mappings for the $1^{\text {st }}$ transmission to $4^{\text {th }}$ transmission. Assuming a superior decoding performance for uniformly distributed LLRs of all transmitted bits, the objective is to find mapping rules for retransmissions with the constellations from Figure 5 that equalize the mean $L L R \mathrm{~s}$ after combining. Using the mappings for requested retransmissions according to Table 6 the soft-combined $L L R \mathrm{~s}$ after requested retransmissions are averaged. This is shown in Table 7 for an AWGN channel, where the soft-combined $L L R \mathrm{~s}$ for $i_{1}$ and $i_{2}$ after each transmission are given with and without applying the CoRe. It is noted that exactly the same principle applies to the $q_{1}$ and $q_{2}$ bits mapped onto the quadrature component. From Table 7 it can be observed that in case of 16QAM for an AWGN channel the averaging is perfect after 4 requested transmissions, hence, a total of 4 different mappings is sufficient.


Figure 5. The signal constellation in the case of 16QAM for each transmission

Table 6. LLRs for bits mapped on the in-phase component of the signal constellation according to mapping according to mapping the $1^{\text {st }}$ transmission to $4^{\text {th }}$ transmission

| Symbol$\left(i_{1} i_{2} q_{1} q_{2}\right)$ | $1^{\text {st }}$ transmission |  | $2^{\text {nd }}$ transmission |  | $3^{\text {rd }}$ transmission |  | $4^{\text {th }}$ transmission |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\begin{gathered} \text { Mean } \\ L L R\left(i_{1}\right) \end{gathered}$ | $\begin{gathered} \text { Mean } \\ L L R\left(i_{2}\right) \end{gathered}$ | $\begin{gathered} \text { Mean } \\ L L R\left(i_{1}\right) \end{gathered}$ | $\begin{gathered} \text { Mean } \\ L L R\left(i_{2}\right) \end{gathered}$ | $\begin{gathered} \text { Mean } \\ L L R\left(i_{2}\right) \end{gathered}$ | $\begin{gathered} \text { Mean } \\ L L R\left(i_{2}\right) \\ \hline \end{gathered}$ | Mean $L L R\left(i_{1}\right)$ | Mean <br> $L L R\left(i_{2}\right)$ |
| $00 q_{1} q_{2}$ | -A | -A | -A | -4A | -A | -A | -4A | -A |
| $01 q_{1} q_{2}$ | -4A | A | -A | 4A | -A | A | -A | A |
| $10 q_{1} q_{2}$ | A | -A | A | -A | A | -4A | 4A | -A |
| $11 q_{1} q_{2}$ | 4A | A | A | A | A | 4A | A | A |

Table 7. Cumulative $\operatorname{LLRs}$ for bits mapped on the in-phase component of the signal constellation for an AWGN channel

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| Transmiss ion No. | Correspon ding figure | $\begin{aligned} & \text { Symbol } \\ & \left(i_{1} i_{2} q_{1} q_{2}\right) \end{aligned}$ | With CoRe |  | Without CoRe |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | $\begin{gathered} \text { Mean } L L R \\ \left(i_{1}\right) \\ \hline \end{gathered}$ | $\begin{gathered} \hline \text { Mean } L L R \\ \left(i_{2}\right) \\ \hline \end{gathered}$ | $\begin{gathered} \hline \text { Mean } L L R \\ \left(i_{1}\right) \\ \hline \end{gathered}$ | Mean $L L R\left(i_{2}\right)$ |
| 1 | Figure 5(a) | $00 q_{1} q_{2}$ | -A | -A | -A | -A |
|  |  | $01 q_{1} q_{2}$ | -4A | A | -4A | A |
|  |  | $10 q_{1} q_{2}$ | A | -A | A | -A |
|  |  | $11 q_{1} q_{2}$ | 4A | A | 4A | A |
| 2 | Figure 5(b) | $00 q_{1} q_{2}$ | -2A | $-5 \mathrm{~A}$ | -2A | -2A |
|  |  | $01 q_{1} q_{2}$ | -5A | 5A | -8A | 2A |
|  |  | $10 q_{1} q_{2}$ | 2A | -2A | 2A | -2A |
|  |  | $11 q_{1} q_{2}$ | 5A | 2A | 8A | 2A |
| 3 | Figure 5(c) | $00 q_{1} q_{2}$ | -3A | -6A | -3A | -3A |
|  |  | $01 q_{1} q_{2}$ | -6A | 6A | -12A | 3A |
|  |  | $10 q_{1} q_{2}$ | 3A | -6A | 3A | -3A |
|  |  | $11 q_{1} q_{2}$ | 6A | 6A | 12A | 3A |
| 4 | Figure 5(d) | $00 q_{1} q_{2}$ | -7A | -7A | -4A | -4A |
|  |  | $01 q_{1} q_{2}$ | -7A | 7A | -16A | 4A |
|  |  | $10 q_{1} q_{2}$ | 7A | -7A | 4A | -4A |
|  |  | $11 q_{1} q_{2}$ | 7A | 7A | 16A | 4A |

### 6.2. 64QAM case

Under the assumption of a uniform signal constellation $x_{1}=3 x_{0}, x_{2}=5 x_{0}, x_{3}=7 x_{0}$ for 64QAM, equations (1) can be fairly good approximated by the following equations.

$$
\begin{align*}
& \operatorname{LLR}\left(b=i_{1}\right) \approx\left\{\begin{array}{cc}
-16 K x_{0} x-48 K x_{0}{ }^{2} & ,\left(x<-6 x_{0}\right) \\
-12 K x_{0} x-24 K x_{0}{ }^{2} & ,\left(-6 x_{0} \leq x<-4 x_{0}\right) \\
-8 K x_{0} x-8 K x_{0}{ }^{2} & \left(-4 x_{0} \leq x<-2 x_{0}\right) \\
-4 K x_{0} x & ,\left(-2 x_{0} \leq x<2 x_{0}\right) \\
-8 K x_{0} x+8 K x_{0}{ }^{2} & ,\left(2 x_{0} \leq x<4 x_{0}\right) \\
-12 K x_{0} x+24 K x_{0}{ }^{2} & ,\left(4 x_{0} \leq x<6 x_{0}\right) \\
-16 K x_{0} x+48 K x_{0}{ }^{2} & ,\left(6 x_{0} \leq x\right)
\end{array}\right. \\
& \operatorname{LLR}\left(b=i_{2}\right) \approx\left\{\begin{array}{cc}
-8 K x_{0} x-40 K x_{0}{ }^{2} & ,\left(x<-6 x_{0}\right) \\
-4 K x_{0} x-16 K x_{0}{ }^{2}, & ,\left(-6 x_{0} \leq x<-2 x_{0}\right) \\
-8 K x_{0} x-24 K x_{0}{ }^{2} & ,\left(-2 x_{0} \leq x<0\right) \\
8 K x_{0} x-24 K x_{0}{ }^{2} & ,\left(0 \leq x<2 x_{0}\right) \\
4 K x_{0} x-16 K x_{0}{ }^{2} & ,\left(2 x_{0} \leq x<6 x_{0}\right) \\
8 K x_{0} x-40 K x_{0}{ }^{2} & ,\left(6 x_{0} \leq x\right) \\
\operatorname{LLR}\left(b=i_{3}\right) \approx\left\{\begin{array}{cc}
-4 K x_{0} x-24 K x_{0}{ }^{2} & ,\left(x<-4 x_{0}\right) \\
4 K x_{0} x+8 K x_{0}{ }^{2} & ,\left(-4 x_{0} \leq x<0\right) \\
-4 K x_{0} x+8 K x_{0}{ }^{2} & ,\left(0 \leq x<4 x_{0}\right) \\
4 K x_{0} x-24 K x_{0}{ }^{2} & ,\left(4 x_{0} \leq x\right)
\end{array},\right.
\end{array} .\right.
\end{align*}
$$

Table 8 shows the mean $L L R$ s for bits mapped on the in-phase component of the signal constellation for the
mapping in the case of 64 QAM as shown in figure 2 according to equation (4) (substituting $4 K x_{0}^{2}$ by A ).
The $L L R$ of $i_{1}$ and $i_{2}$ depends on the content of the other bits. On the other hand, The magnitude in $L L R$ of $i_{3}$ is always constant.

Table 8. Mean LLRs for bits mapped on the in-phase component of the signal constellation for the mapping in Figure 2 accoding to equation (4)

| Symbol $\left(\boldsymbol{i}_{1} \boldsymbol{i}_{2} \boldsymbol{i}_{3} q_{1} q_{2} q_{3}\right)$ | Mean value of $\boldsymbol{x}$ | Mean $\boldsymbol{L L R}\left(\boldsymbol{i}_{\mathbf{1}}\right)$ | Mean $\boldsymbol{L L R}\left(\boldsymbol{i}_{\mathbf{2}}\right)$ | Mean $\boldsymbol{L L R}\left(\boldsymbol{i}_{\mathbf{3}}\right)$ |
| :---: | :---: | :---: | :---: | :---: |
| $000 q_{1} q_{2} q_{3}$ | $x_{1}$ | $-16 K x_{0}^{2}=-4 A$ | $-4 K x_{0}^{2}=-A$ | $-4 K x_{0}^{2}=-A$ |
| $001 q_{1} q_{2} q_{3}$ | $x_{0}$ | $-4 K x_{0}^{2}=-A$ | $-16 K x_{0}^{2}=-4 A$ | $4 K x_{0}^{2}=A$ |
| $010 q_{1} q_{2} q_{3}$ | $x_{2}$ | $-36 K x_{0}^{2}=-9 A$ | $4 K x_{0}^{2}=A$ | $-4 K x_{0}^{2}=-A$ |
| $011 q_{1} q_{2} q_{3}$ | $x_{3}$ | $-64 K x_{0}^{2}=-16 A$ | $16 K x_{0}^{2}=4 A$ | $4 K x_{0}^{2}=A$ |
| $100 q_{1} q_{2} q_{3}$ | $-x_{1}$ | $16 K x_{0}^{2}=4 A$ | $-4 K x_{0}^{2}=-A$ | $-4 K x_{0}^{2}=-A$ |
| $101 q_{1} q_{2} q_{3}$ | $-x_{0}$ | $4 K x_{0}^{2}=A$ | $-16 K x_{0}^{2}=-4 A$ | $4 K x_{0}^{2}=A$ |
| $110 q_{1} q_{2} q_{3}$ | $-x_{2}$ | $36 K x_{0}^{2}=9 A$ | $4 K x_{0}^{2}=A$ | $-4 K x_{0}^{2}=-A$ |
| $111 q_{1} q_{2} q_{3}$ | $-x_{3}$ | $64 K x_{0}^{2}=16 A$ | $16 K x_{0}^{2}=4 A$ | $4 K x_{0}^{2}=A$ |

Figure 6 shows the signal constellation in the case of 64QAM for each transmission and Table 8 shows LLRs for bits mapped on the in-phase component of the signal constellation according to the mappings for the $1^{\text {st }}$ transmission to $6^{\text {th }}$ transmission. Assuming a superior decoding performance for uniformly distributed LLRs of all transmitted bits, the objective is to find mapping rules for retransmissions with the constellations from Figure 6 that equalize the mean $L L R$ s after combining. Using the mappings for requested retransmissions according to Table 8 the soft-combined $L L R \mathrm{~s}$ after requested retransmissions are averaged. This is shown in Table 9 for an AWGN channel, where the soft-combined LLRs for $i_{1}, i_{2}$ and $i_{3}$ after each transmission are given with and without applying the CoRe. It is noted that exactly the same principle applies to the $q_{1}, q_{2}$ and $q_{3}$ bits mapped onto the quadrature component. From Table 9 it can be observed that in case of 64QAM for an AWGN channel the averaging is perfect after 6 requested transmissions, hence, a total of 6 different mappings is sufficient.

(a) $1^{\text {st }}$ transmission
(b) $2^{\text {nd }}$ transmission

(c) $3^{\text {rd }}$ transmission
(d) $4^{\text {th }}$ transmission

(e) $5^{\text {th }}$ transmission

(f) $6^{\text {th }}$ transmission

Figure 6. The signal constellation in the case of 64QAM for each transmission

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Table 8. $L L R$ s for bits mapped on the in-phase component of the signal constellation according to mapping according to mapping the $1^{\text {st }}$ transmission to $4^{\text {th }}$ transmission

| $\begin{gathered} \text { Symbol } \\ \left(i_{1} i_{2} i_{3} q_{1} q_{2} q_{3}\right) \end{gathered}$ | $1^{\text {st }}$ transmission |  |  | $2^{\text {nd }}$ transmission |  |  | $3^{\text {rd }}$ transmission |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Mean LLR <br> $\left(i_{1}\right)$ | Mean LLR <br> $\left(i_{2}\right)$ | Mean LLR <br> $\left(i_{3}\right)$ | Mean LLR <br> $\left(i_{1}\right)$ | Mean LLR <br> $\left(i_{2}\right)$ | Mean LLR <br> $\left(i_{3}\right)$ | Mean LLR <br> $\left(i_{1}\right)$ | Mean LLR <br> $\left(i_{2}\right)$ | Mean LLR <br> ( $i_{3}$ ) |
| $000 q_{1} q_{2} q_{3}$ | -4A | -A | -A | -A | -4A | -A | -A | -A | -4A |
| $001 q_{1} q_{2} q_{3}$ | -A | -4A | A | -A | -9A | A | -A | -A | 4A |
| $010 q_{1} q_{2} q_{3}$ | -9A | A | -A | -A | 4A | -A | -4A | A | -A |
| $011 q_{1} q_{2} q_{3}$ | -16A | 4A | A | -A | 9A | A | -4A | A | A |
| $100 q_{1} q_{2} q_{3}$ | 4A | -A | -A | A | -A | -4A | A | -A | -9A |
| $101 q_{1} q_{2} q_{3}$ | A | -4A | A | A | -16A | 4A | A | -A | 9A |
| $110 q_{1} q_{2} q_{3}$ | 9A | A | -A | A | A | -4A | 4A | A | -16A |
| $111 q_{1} q_{2} q_{3}$ | 16A | 4A | A | A | 16A | 4A | 4A | A | 16A |


| $\begin{gathered} \text { Symbol } \\ { }_{\left(i_{1} i_{2} i_{3} q_{1} q_{2} q_{3}\right)}^{\text {Sy }} \end{gathered}$ | $4^{\text {th }}$ transmission |  |  | $5^{\text {th }}$ transmission |  |  | $6^{\text {th }}$ transmission |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\begin{gathered} \hline \text { Mean } \\ L L R \\ \left(i_{1}\right) \\ \hline \end{gathered}$ | Mean LLR <br> $\left(i_{2}\right)$ | $\begin{gathered} \hline \text { Mean } \\ L L R \\ \left(i_{3}\right) \\ \hline \end{gathered}$ | Mean LLR <br> $\left(i_{1}\right)$ | Mean LLR <br> $\left(i_{2}\right)$ | Mean LLR <br> ( $i_{3}$ ) | $\begin{gathered} \hline \text { Mean } \\ L L R \\ \left(i_{1}\right) \\ \hline \end{gathered}$ | $\begin{gathered} \text { Mean } \\ L L R \\ \left(i_{2}\right) \\ \hline \end{gathered}$ | $\begin{gathered} \text { Mean } \\ L L R \\ \left(i_{3}\right) \\ \hline \end{gathered}$ |
| $000 q_{1} q_{2} q_{3}$ | -16A | -4A | -A | -A | -16A | -4A | -4A | -A | -16A |
| $001 q_{1} q_{2} q_{3}$ | -9A | -A | A | -A | -A | 4A | -4A | -A | 16A |
| $010 q_{1} q_{2} q_{3}$ | -A | 4A | -A | -A | 16A | -4A | -A | A | -9A |
| $011 q_{1} q_{2} q_{3}$ | -4A | A | A | -A | A | 4A | -A | A | 9A |
| $100 q_{1} q_{2} q_{3}$ | 16A | -4A | -A | A | -9A | -A | 4A | -A | -A |
| $101 q_{1} q_{2} q_{3}$ | 9A | -A | A | A | -4A | A | 4A | -A | A |
| $110 q_{1} q_{2} q_{3}$ | A | 4A | -A | A | 9A | -A | A | A | -4A |
| $111 q_{1} q_{2} q_{3}$ | 4A | A | A | A | 4A | A | A | A | 4A |

Table 9. Cumulative $\operatorname{LLRs}$ for bits mapped on the in-phase component of the signal constellation for an AWGN channel

| Transmi ssion No. | Correspond ing figure | Symbol $\left(i_{1} i_{2} q_{1} q_{2}\right)$ | With CoRe |  |  | Without CoRe |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | $\begin{gathered} \text { Mean } \\ L L R\left(i_{1}\right) \end{gathered}$ | $\begin{gathered} \text { Mean } \\ L L R\left(i_{2}\right) \\ \hline \end{gathered}$ | $\begin{array}{\|c\|} \hline \text { Mean } \\ L L R\left(i_{3}\right) \\ \hline \end{array}$ | $\begin{gathered} \text { Mean } \\ L L R\left(i_{1}\right) \\ \hline \end{gathered}$ | $\begin{gathered} \hline \text { Mean } \\ L L R\left(i_{2}\right) \\ \hline \end{gathered}$ | Mean $L L R\left(i_{3}\right)$ |
| 1 | Figure 6(a) | $000 q_{1} q_{2} q_{3}$ | -4A | -A | -A | -4A | -A | -A |
|  |  | $001 q_{1} q_{2} q_{3}$ | -A | -4A | A | -A | -4A | A |
|  |  | $010 q_{1} q_{2} q_{3}$ | -9A | A | -A | -9A | A | -A |
|  |  | $011 q_{1} q_{2} q_{3}$ | -16A | 4A | A | -16A | 4A | A |
|  |  | $100 q_{1} q_{2} q_{3}$ | 4A | -A | -A | 4A | -A | -A |
|  |  | $101 q_{1} q_{2} q_{3}$ | A | -4A | A | A | -4A | A |
|  |  | $110 q_{1} q_{2} q_{3}$ | 9A | A | -A | 9A | A | -A |
|  |  | $111 q_{1} q_{2} q_{3}$ | 16A | 4A | A | 16A | 4A | A |
| 2 | Figure 6(b) | $000 q_{1} q_{2} q_{3}$ | -5A | -5A | -2A | -8A | -2A | -2A |
|  |  | $001 q_{1} q_{2} q_{3}$ | -2A | -13A | 2A | -2A | -8A | 2A |
|  |  | $010 q_{1} q_{2} q_{3}$ | -10A | 5A | -2A | -18A | 2A | -2A |
|  |  | $011 q_{1} q_{2} q_{3}$ | -17A | 13A | 2A | -32A | 8A | 2A |
|  |  | $100 q_{1} q_{2} q_{3}$ | 5A | -2A | -5A | 8A | -2A | -2A |

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|  |  | $101 q_{1} q_{2} q_{3}$ | 2A | -20A | 5A | 2A | -8A | 2A |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $110 q_{1} q_{2} q_{3}$ | 10A | 2A | -5A | 18A | 2A | -2A |
|  |  | $111 q_{1} q_{2} q_{3}$ | 17A | 20A | 5A | 32A | 8A | 2A |
| 3 | Figure 6(c) | $000 q_{1} q_{2} q_{3}$ | -6A | -6A | -6A | -12A | -3A | -3A |
|  |  | $001 q_{1} q_{2} q_{3}$ | -3A | -14A | 6A | -3A | -12A | 3A |
|  |  | $010 q_{1} q_{2} q_{3}$ | -14A | 6A | -3A | -27A | 3A | -3A |
|  |  | $011 q_{1} q_{2} q_{3}$ | -21A | 14A | 3 | -48A | 12A | 3A |
|  |  | $100 q_{1} q_{2} q_{3}$ | 6A | -3A | -14A | 12A | -3A | -3A |
|  |  | $101 q_{1} q_{2} q_{3}$ | 3A | -21A | 14A | 3A | -12A | 3A |
|  |  | $110 q_{1} q_{2} q_{3}$ | 14A | 3A | -21A | 27A | 3A | -3A |
|  |  | $111 q_{1} q_{2} q_{3}$ | 21A | 21A | 21A | 48A | 12A | 3A |
| 4 | Figure 6(d) | $000 q_{1} q_{2} q_{3}$ | -22A | -10A | -7A | -16A | -4A | -4A |
|  |  | $001 q_{1} q_{2} q_{3}$ | -12A | -15A | 7A | -4A | -16A | 4A |
|  |  | $010 q_{1} q_{2} q_{3}$ | -15A | 10A | -4A | -36A | 4A | -4A |
|  |  | $011 q_{1} q_{2} q_{3}$ | -25A | 15A | 4A | -64A | 16A | 4A |
|  |  | $100 q_{1} q_{2} q_{3}$ | 22 A | -7A | -15A | 16A | -4A | -4A |
|  |  | $101 q_{1} q_{2} q_{3}$ | 12A | -22A | 15A | 4A | -16A | 4A |
|  |  | $110 q_{1} q_{2} q_{3}$ | 15A | 7A | -22A | 36A | 4A | -4A |
|  |  | $111 q_{1} q_{2} q_{3}$ | 25A | 22A | 22A | 64A | 16A | 4A |
| 5 | Figure 6(e) | $000 q_{1} q_{2} q_{3}$ | -23A | -26A | -11A | -20A | -5A | -5A |
|  |  | $001 q_{1} q_{2} q_{3}$ | -13A | -16A | 11A | -5A | -20A | 5A |
|  |  | $010 q_{1} q_{2} q_{3}$ | -16A | 26A | -8A | -45A | 5A | -5A |
|  |  | $011 q_{1} q_{2} q_{3}$ | -26A | 16A | 8A | -80A | 20A | 5A |
|  |  | $100 q_{1} q_{2} q_{3}$ | 23A | -16A | -16A | 20A | -5A | -5A |
|  |  | $101 q_{1} q_{2} q_{3}$ | 13A | -26A | 16A | 5A | -20A | 5A |
|  |  | $110 q_{1} q_{2} q_{3}$ | 16A | 16A | -23A | 45A | 5A | -5A |
|  |  | $111 q_{1} q_{2} q_{3}$ | 26A | 26A | 23A | 80A | 20A | 5A |
| 6 | Figure 6(f) | $000 q_{1} q_{2} q_{3}$ | -27A | -27A | -27A | -24A | -6A | -6A |
|  |  | $001 q_{1} q_{2} q_{3}$ | -17A | -17A | 27A | -6A | -24A | 6A |
|  |  | $010 q_{1} q_{2} q_{3}$ | -17A | 27A | -17A | -54A | 6A | -6A |
|  |  | $011 q_{1} q_{2} q_{3}$ | -27A | 17A | 17A | -96A | 24A | 6A |
|  |  | $100 q_{1} q_{2} q_{3}$ | 27A | -17A | -17A | 24A | -6A | -6A |
|  |  | $101 q_{1} q_{2} q_{3}$ | 17A | -27A | 17A | 6A | -24A | 6A |
|  |  | $110 q_{1} q_{2} q_{3}$ | 17A | 17A | -27A | 54A | 6A | -6A |
|  |  | $111 q_{1} q_{2} q_{3}$ | 27A | 27A | 27A | 96A | 24A | 6A |

