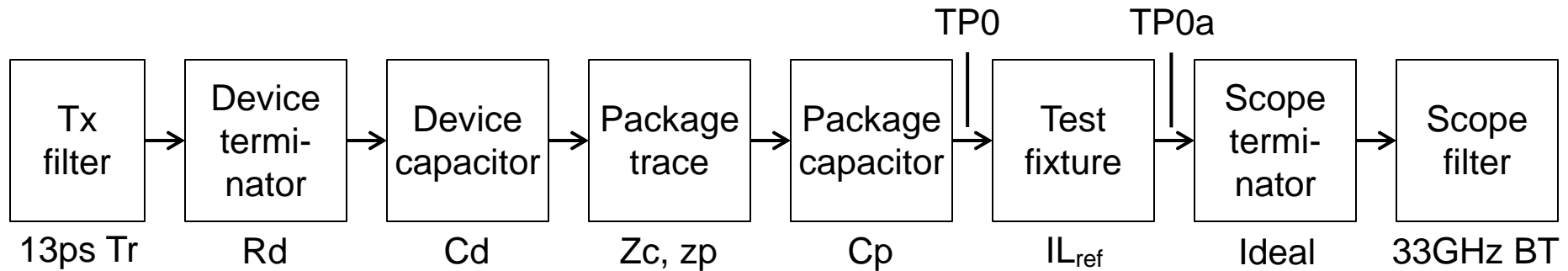


# Comment #41: Effects of the change from $N_p=13$ to $N_p=200$

Yasuo Hidaka  
Fujitsu Laboratories of America, Inc.

IEEE P802.3bs Task Force  
Electrical Ad hoc, October 24, 2016

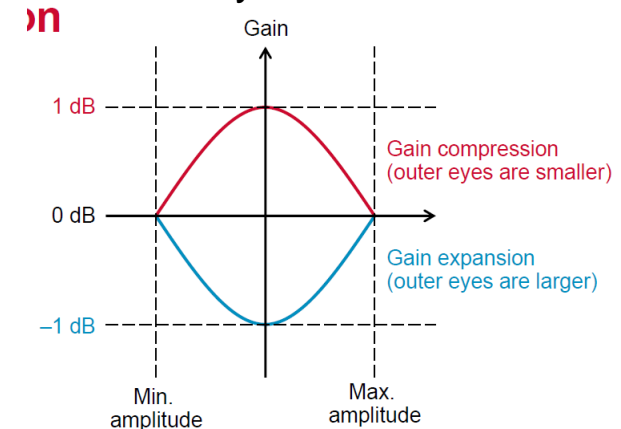
- $N_p$  was changed from 13 to 200 in Draft D2.1.
- A larger  $N_p$  value increases the steady-state voltage  $v_f$ , because a longer filtered pulse will capture more long-term ISI.
  - On the other hand, peak of the filtered pulse does not change.
- As a result, the ratio of the linear fit pulse peak to  $v_f$  is reduced.
- In order to keep the requirement for Tx same, we should adjust  $v_f$  and the ratio of the linear fit pulse peak to  $v_f$  consistently with the change to  $N_p$ .
- I noticed this problem while I was conducting a different study for P802.3cd project



- Tx filter:  $S_{21} = (\text{EQ93A-46} | T_r = 13\text{ps}, \beta = 2)$  (i.e. 13ps 20-80% Tr)
- Device terminator:  $S_{21} = 1, S_{22} = \frac{R_d - 50\Omega}{R_d + 50\Omega}$  (i.e. same as Tx in COM)
- Device capacitor:  $S = (\text{EQ93A-8} | C = C_d)$
- Package trace:  $S = (\text{EQ93A-13,14} | \text{Table93A-3 except } Z_c, z_p)$
- Package capacitor:  $S = (\text{EQ93A-8} | C = C_p)$
- Test fixture:  $|S_{21}| = 10^{-(\text{EQ93-1})/20}, \angle S_{21} = \text{minimum phase}(|S_{21}|)$
- Scope terminator:  $S_{21} = 1, S_{11} = 0$  (i.e. ideal)
- Scope filter: 4-th order Bessel-Thomson LPF with 33GHz 3dB BW
  - $\omega_0 = 98.28967142447435 \text{ G rad/s}$

1. Get  $S_{21}$  of the entire model from 1MHz to  $f_{max}$  with 1MHz step
  - $f_{max} = 26.5625\text{GHz} \times M \div 2$ , where  $M = 32$
2. Get a single-bit pulse response
3. Get a linear cycle response of PRBS13Q with ideal levels
4. Cancel the DC offset of the linear cycle response of PRBS13Q
5. Get a non-linear cycle response of PRBS13Q by gain expansion / compression (similar to a methodology in healey\_3bs\_02\_0916)
  - Simulated from -1.0dB to +1.0dB with 0.2dB step
6. Get V0, V1, V2, and V3 per 120D.3.1.2.1
7. Get Vmid, ES1, and ES2 per 120D.3.1.2
8. Get  $ES = (ES1 + ES2) / 2$  per 120D.3.1.3
9. Get linear fit pulse  $p(k)$  and error  $e(k)$  per 120D.3.1.3, 94.3.12.5.2, 85.8.3.3.5
  - $D_p = 2$  and  $N_p = 13$  or 200
10. Get steady-state voltage  $v_f$  and linear fit pulse peak  $p_{max}$  per 120D.3.1.4
11. Get  $\sigma_e$  from  $e(k)$ , then get SNDR per 120D.3.1.6
  - $\sigma_n$  is always set to  $p_{max} \times 10^{(-50/20)}$  (i.e. -50dB) to have noise floor

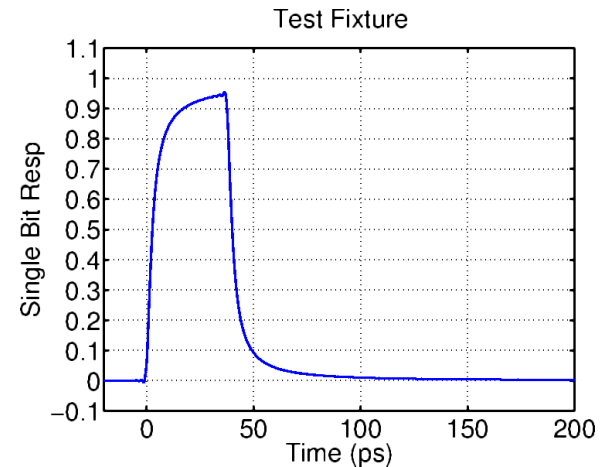
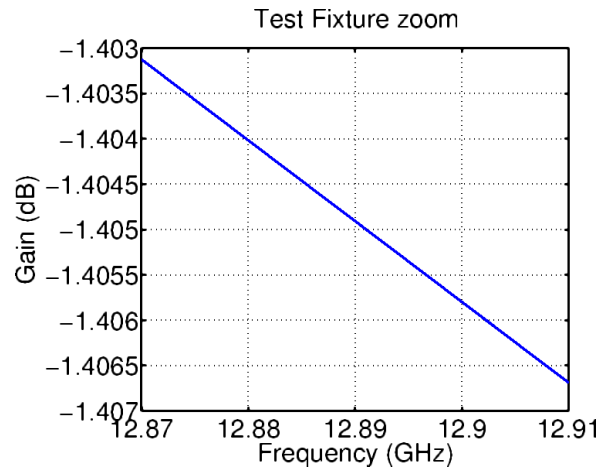
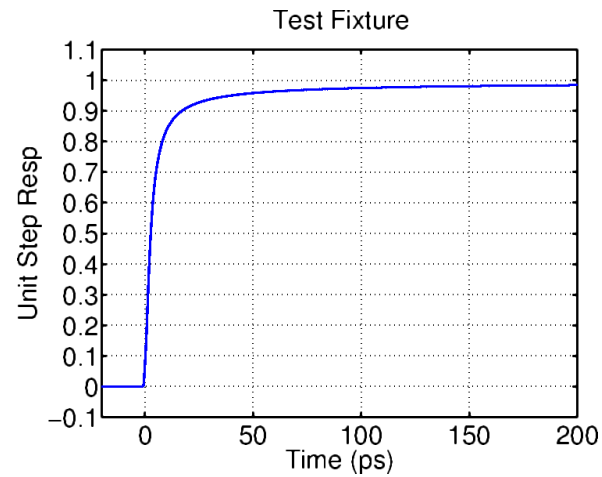
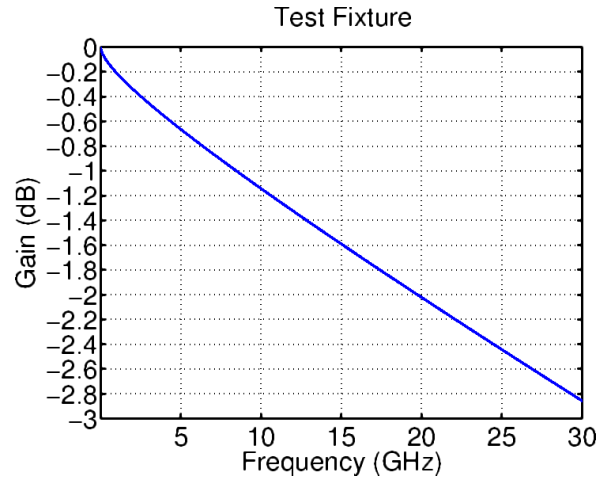
From healey\_3bs\_02\_0916



■ The reference insertion loss of the test fixture is defined by

$$\blacksquare IL_{ref}(f) = -0.0015 + 0.144\sqrt{f} + 0.069f \quad (93-1)$$

- 1.4049dB at 12.89GHz

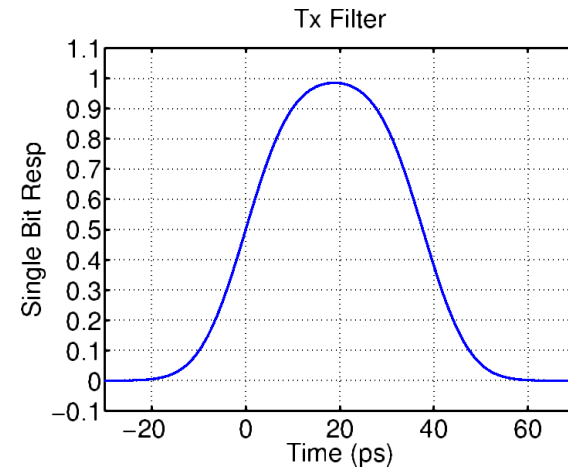
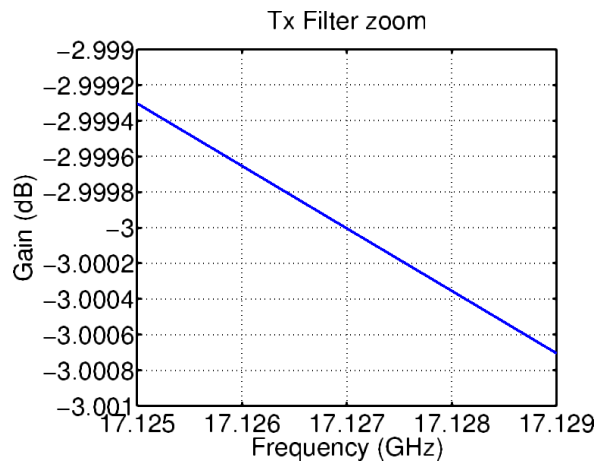
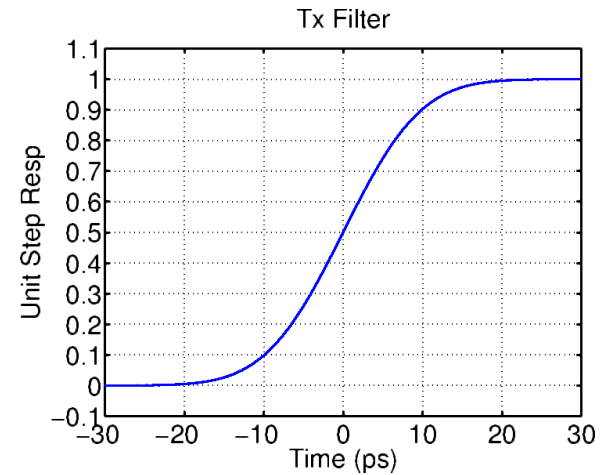
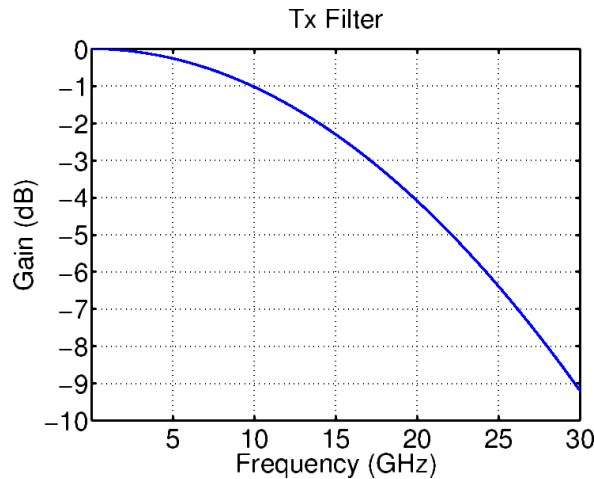


# Tx Transition Time Filter

■ Tx Transition Time Filter (per 802.3by) is defined by

■  $H_t(f) = \exp(-\beta(\pi f T_r / 1.6832)^2)$  (93A-46)

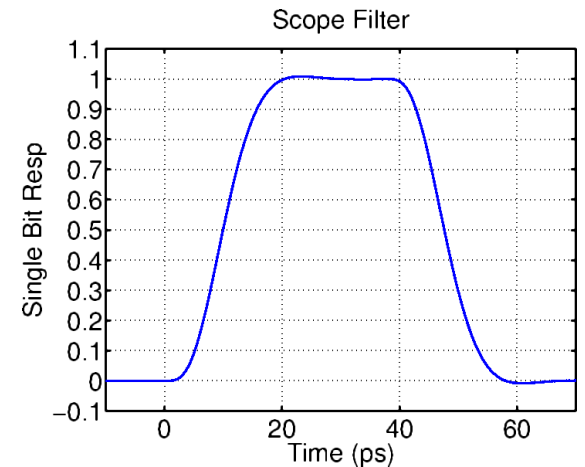
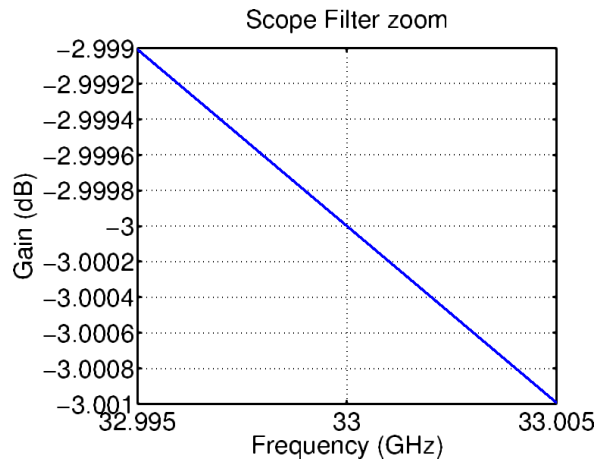
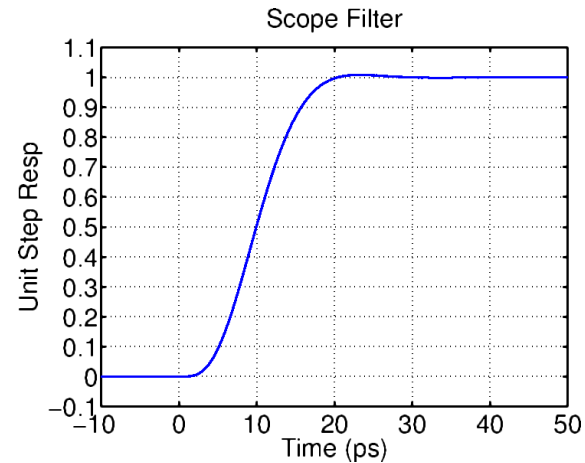
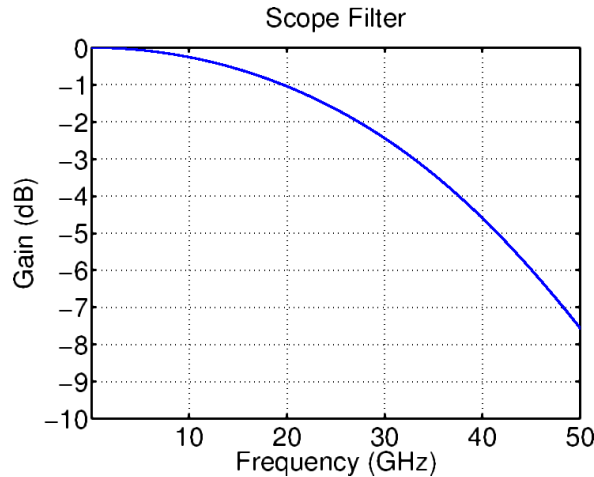
- with  $\beta = 2, T_r = 13ps$



# Scope Filter (4th-order Bessel-Thomson LPF)

■ A 4th-order BT LPF with 33GHz 3dB Bandwidth is defined by

■  $H(s) = \theta_4(0)/\theta_4(s/\omega_0)$  where  $\theta_4(s) = s^4 + 10s^3 + 45s^2 + 105s + 105$  and  $\omega_0 = 98.28967142447435$  G rad/s



# Simulated Package Parameters

- The following 10 combinations of parameters were simulated

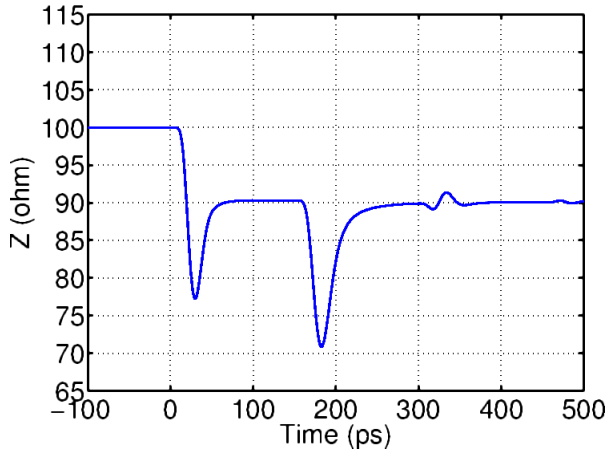
Case	$z_p$ Package trace length	$R_d$ Termination resistance	$Z_c$ Package trace impedance
#1	12 mm	45 $\Omega$	90 $\Omega$
#2			110 $\Omega$
#3		55 $\Omega$	90 $\Omega$
#4			110 $\Omega$
#5	30 mm	45 $\Omega$	90 $\Omega$
#6			110 $\Omega$
#7		55 $\Omega$	90 $\Omega$
#8			110 $\Omega$
#9	12 mm	50 $\Omega$	100 $\Omega$
#10	30 mm		



# TDR of Entire Path from Scope (zp=12mm)

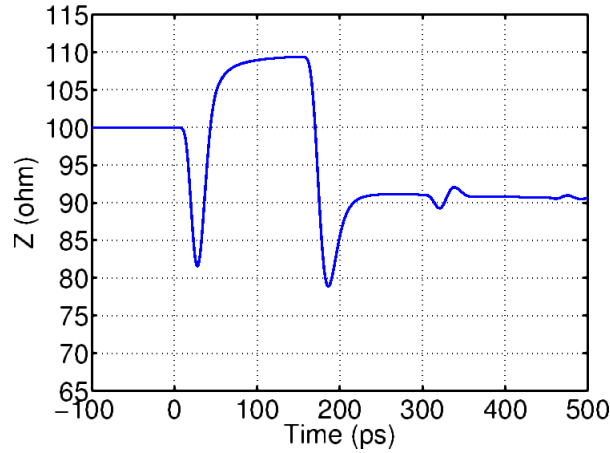
#1:  $R_d=45$ ,  $Z_c=90$

zp12 rd45 zc90



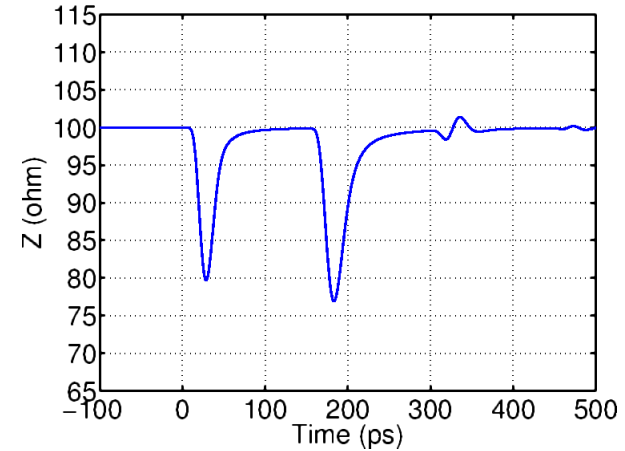
#2:  $R_d=45$ ,  $Z_c=110$

zp12 rd45 zc110



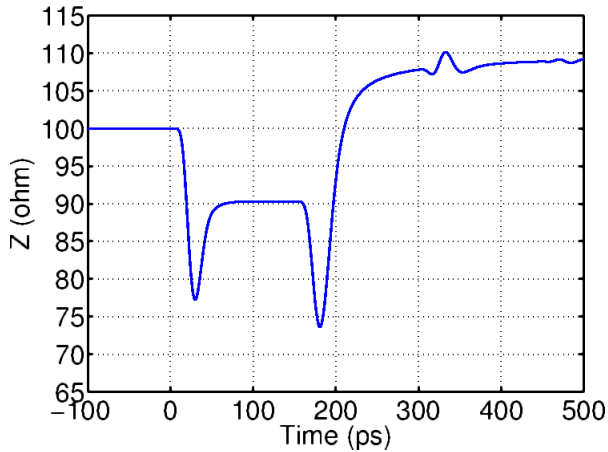
#9:  $R_d=50$ ,  $Z_c=100$

zp12 rd50 zc100



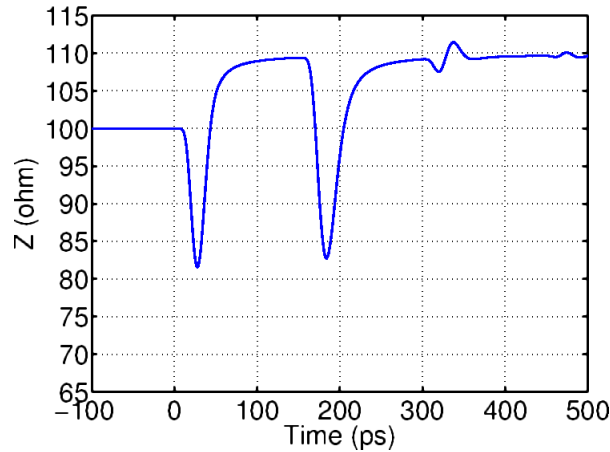
#3:  $R_d=55$ ,  $Z_c=90$

zp12 rd55 zc90



#4:  $R_d=55$ ,  $Z_c=110$

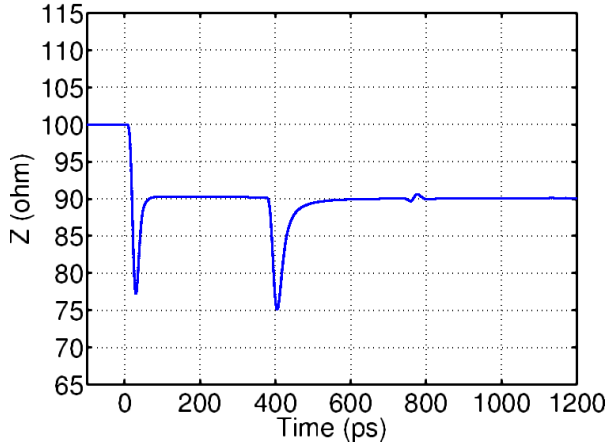
zp12 rd55 zc110



# TDR of Entire Path from Scope (zp=30mm)

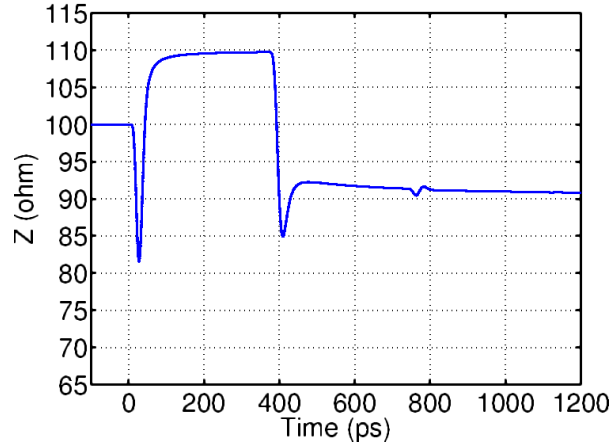
#5: Rd=45, Zc=90

zp30 rd45 zc90



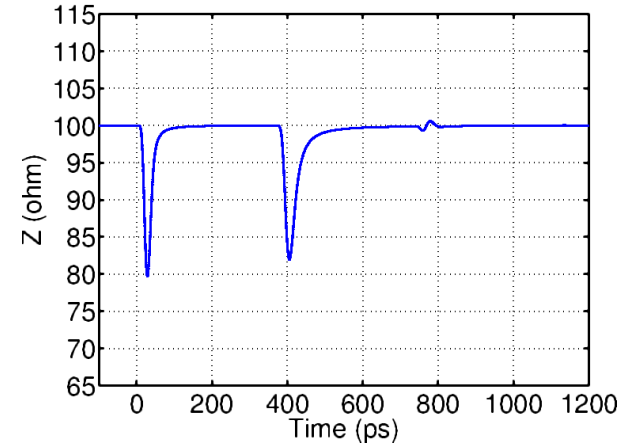
#6: Rd=45, Zc=110

zp30 rd45 zc110



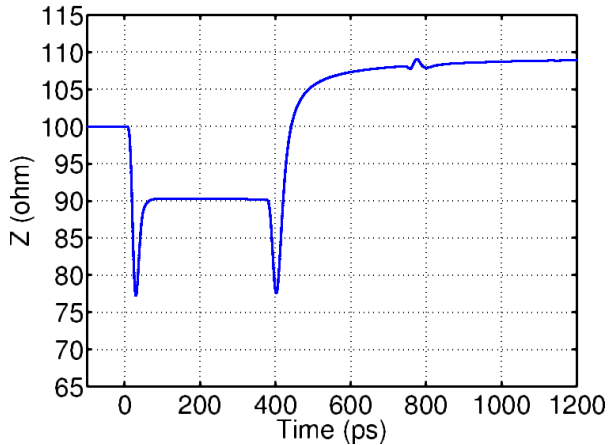
#10: Rd=50, Zc=100

zp30 rd50 zc100



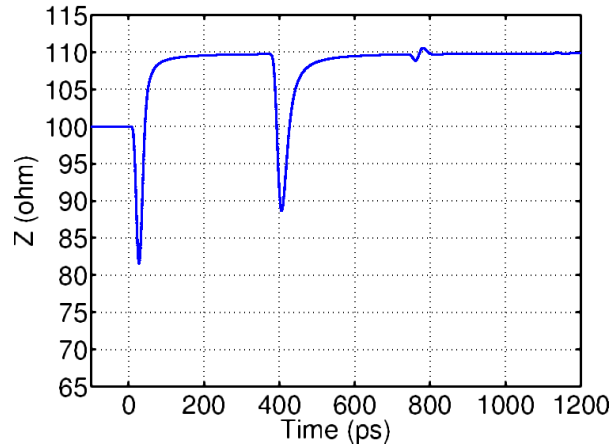
#7: Rd=55, Zc=90

zp30 rd55 zc90



#8: Rd=55, Zc=110

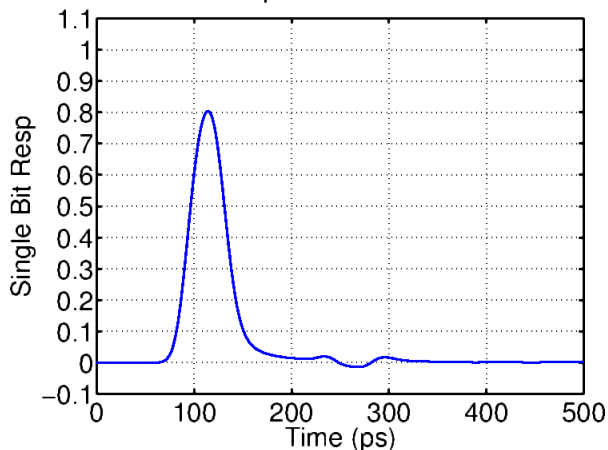
zp30 rd55 zc110



# SBR of Entire Path (zp=12mm)

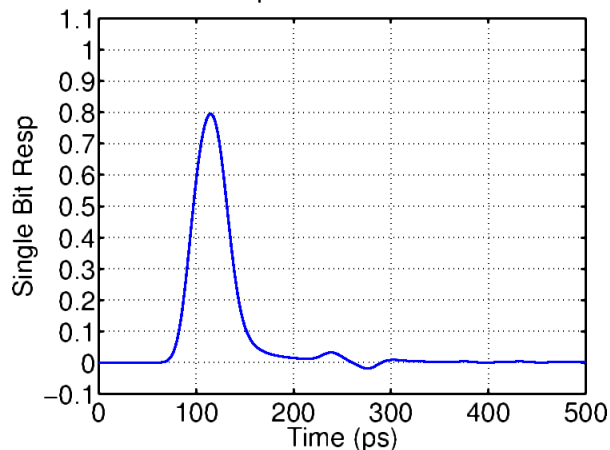
#1: Rd=45, Zc=90

zp12 rd45 zc90



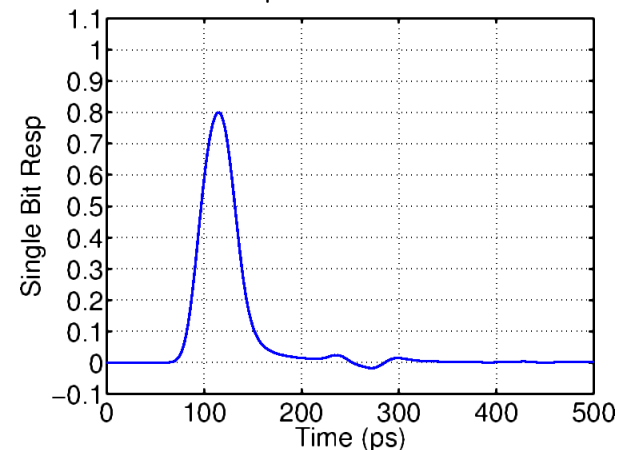
#2: Rd=45, Zc=110

zp12 rd45 zc110



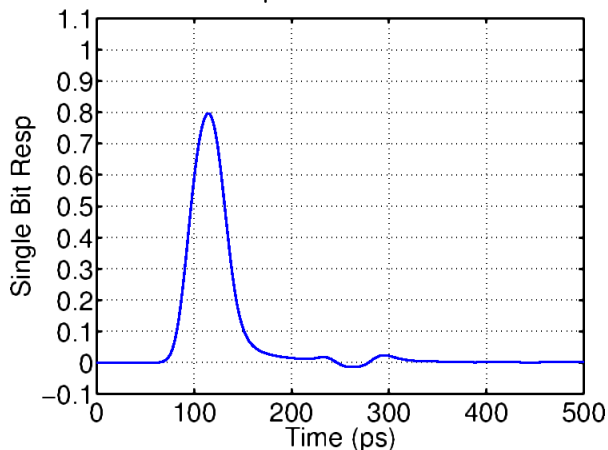
#9: Rd=50, Zc=100

zp12 rd50 zc100



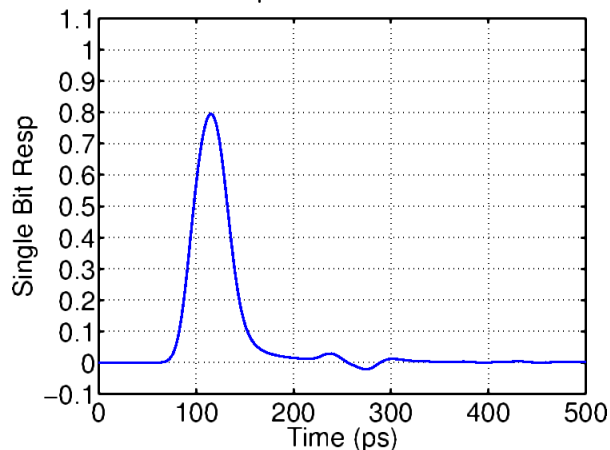
#3: Rd=55, Zc=90

zp12 rd55 zc90



#4: Rd=55, Zc=110

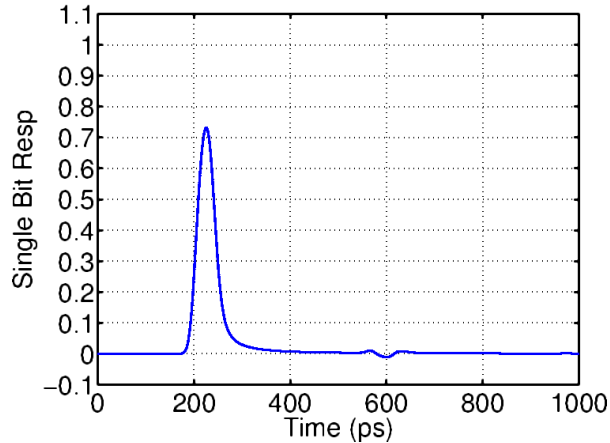
zp12 rd55 zc110



# SBR of Entire Path (zp=30mm)

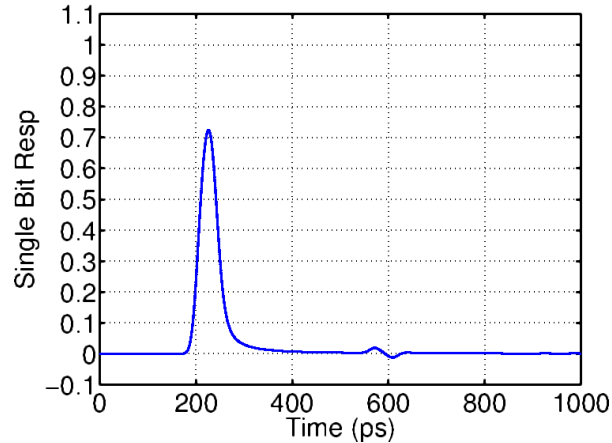
#5: Rd=45, Zc=90

zp30 rd45 zc90



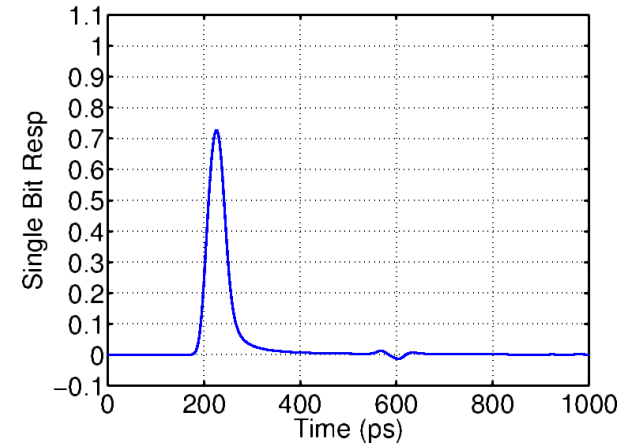
#6: Rd=45, Zc=110

zp30 rd45 zc110



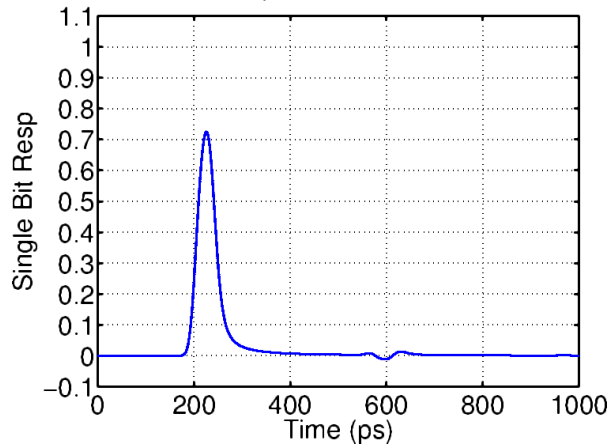
#10: Rd=50, Zc=100

zp30 rd50 zc100



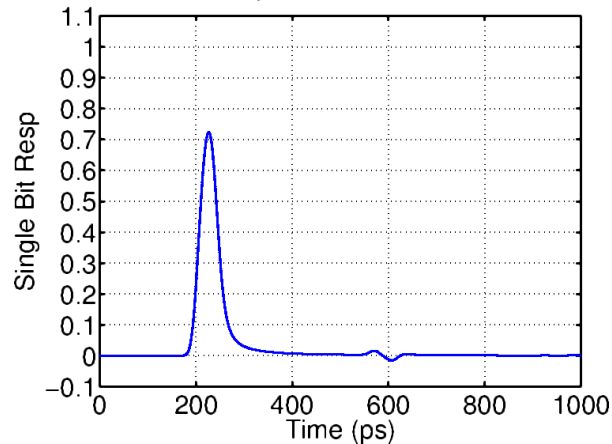
#7: Rd=55, Zc=90

zp30 rd55 zc90



#8: Rd=55, Zc=110

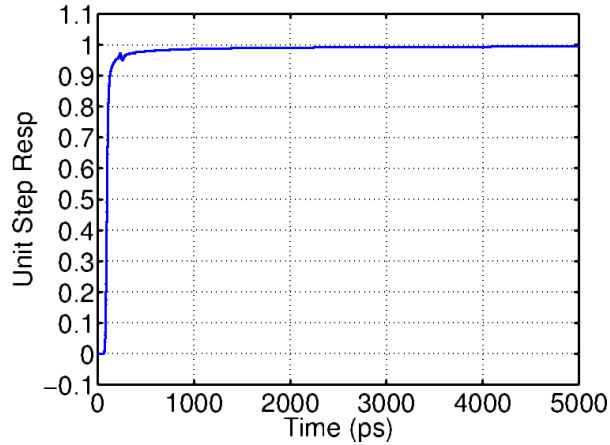
zp30 rd55 zc110



# Step Response of Entire Path (zp=12mm)

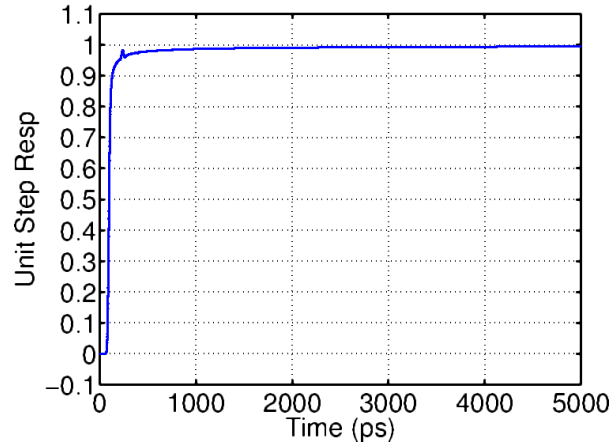
#1:  $R_d=45$ ,  $Z_c=90$

zp12 rd45 zc90



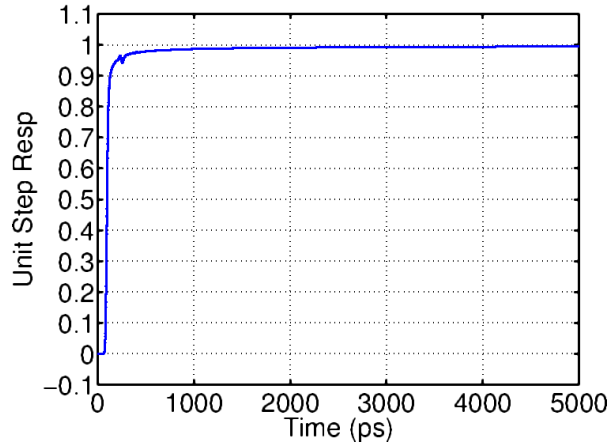
#2:  $R_d=45$ ,  $Z_c=110$

zp12 rd45 zc110



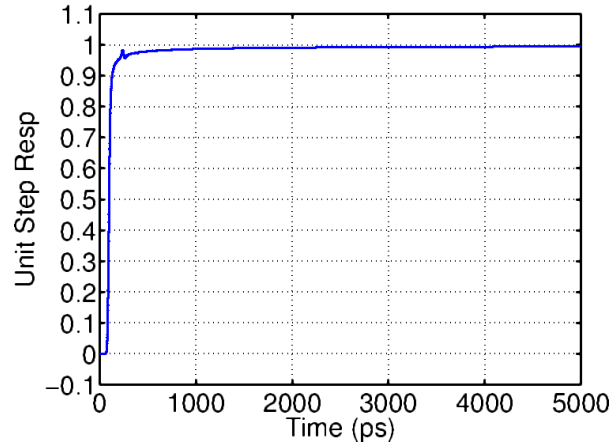
#3:  $R_d=55$ ,  $Z_c=90$

zp12 rd55 zc90



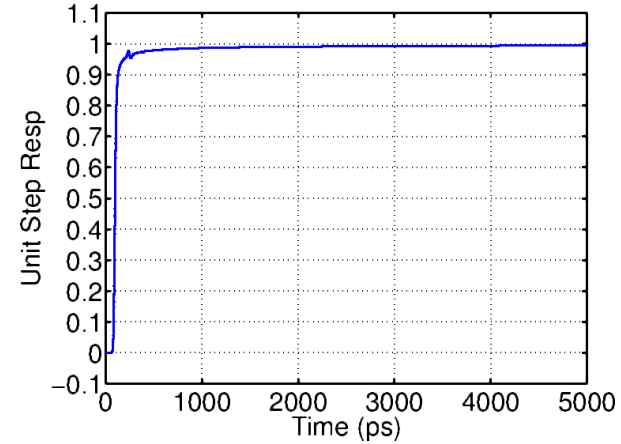
#4:  $R_d=55$ ,  $Z_c=110$

zp12 rd55 zc110



#9:  $R_d=50$ ,  $Z_c=100$

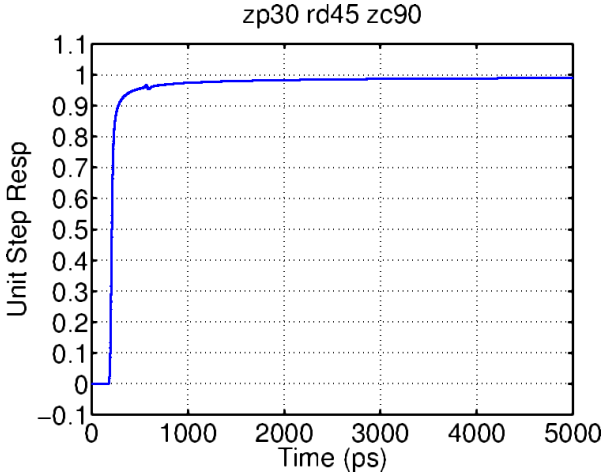
zp12 rd50 zc100



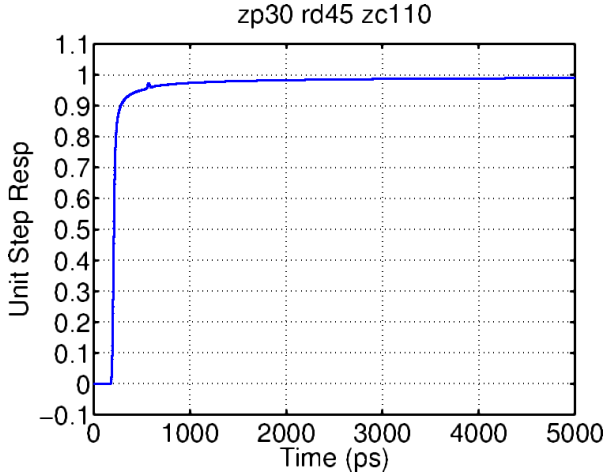
# Step Response of Entire Path (zp=30mm)



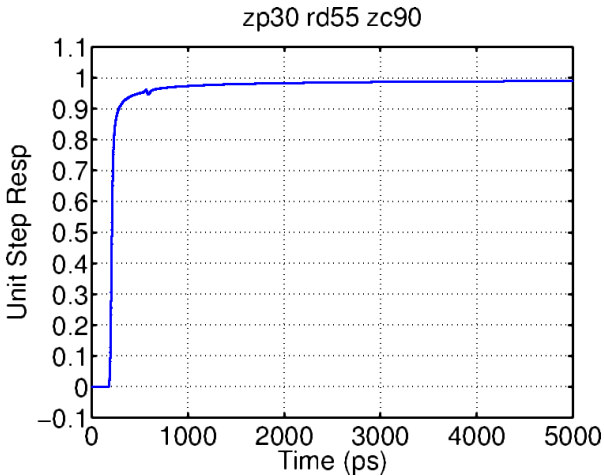
#5: Rd=45, Zc=90



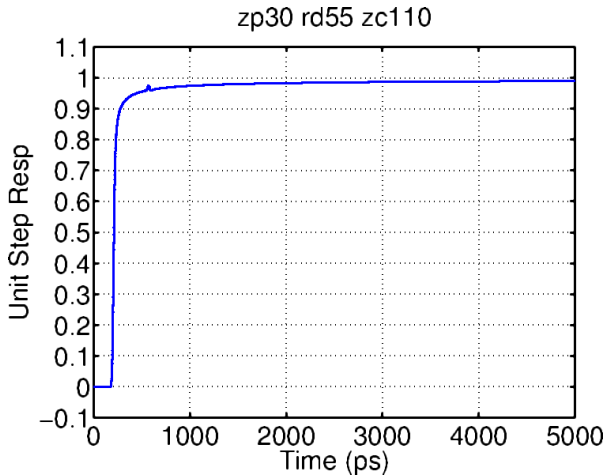
#6: Rd=45, Zc=110



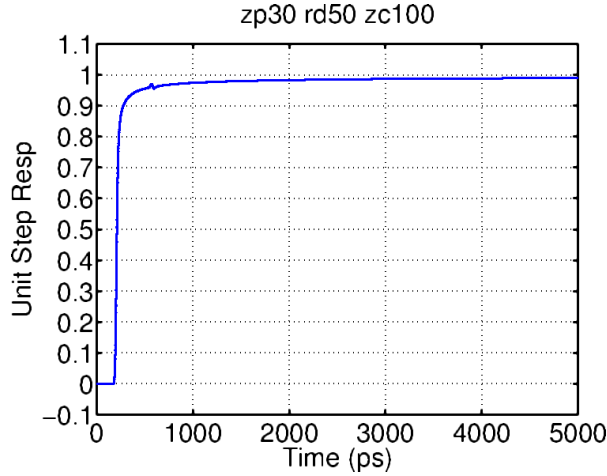
#7: Rd=55, Zc=90



#8: Rd=55, Zc=110



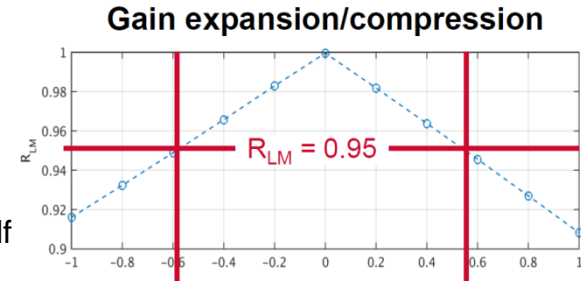
#10: Rd=50, Zc=100



# Level separation mismatch ratio $R_{LM}$

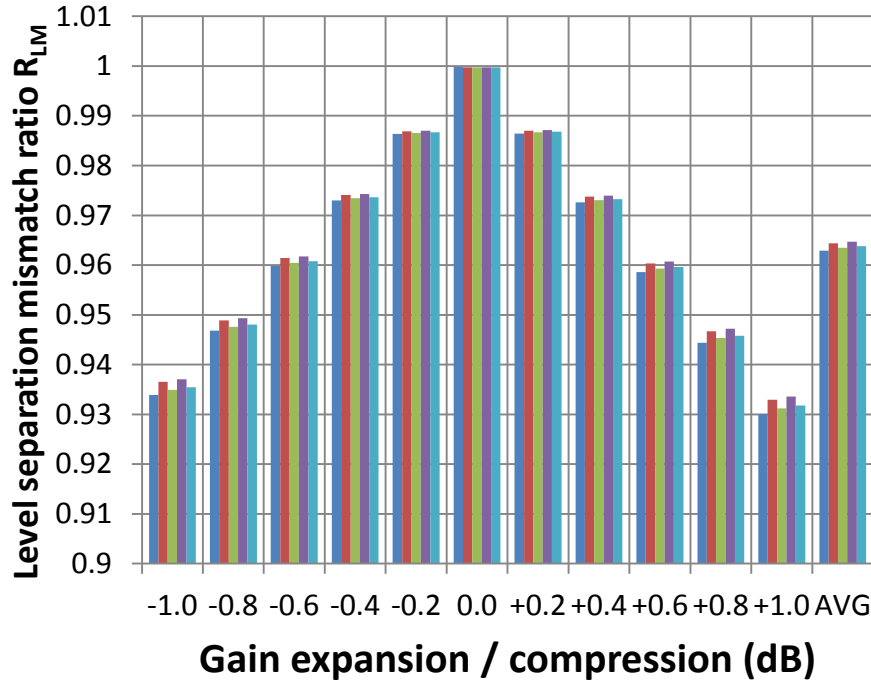
■ Better than healey\_3bs\_02\_0916.pdf

■ Maybe some model difference

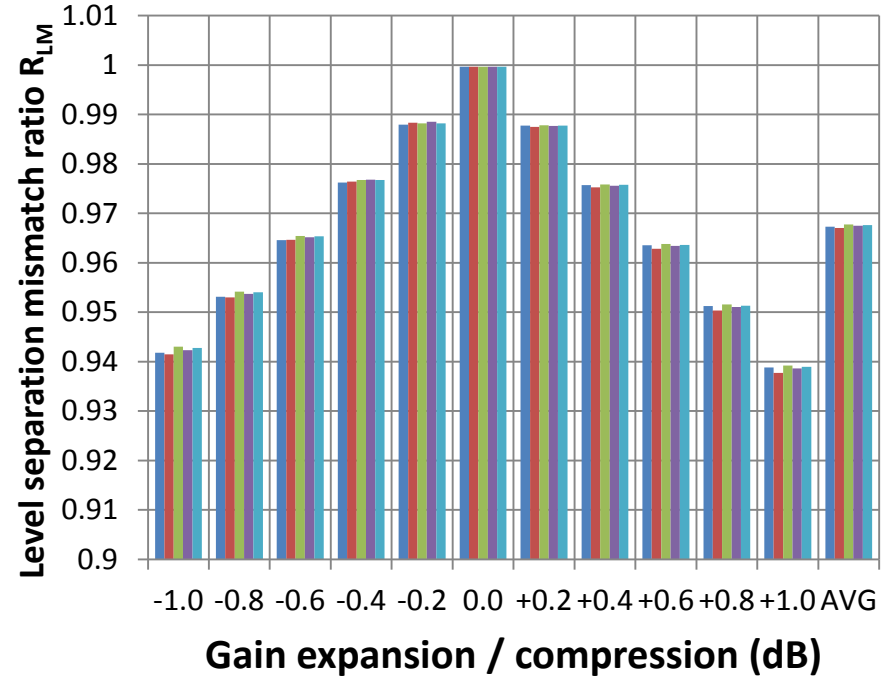


healey\_3bs\_02\_0916.pdf

Level sep. mismatch ratio  $R_{LM}$  (zp=12mm)



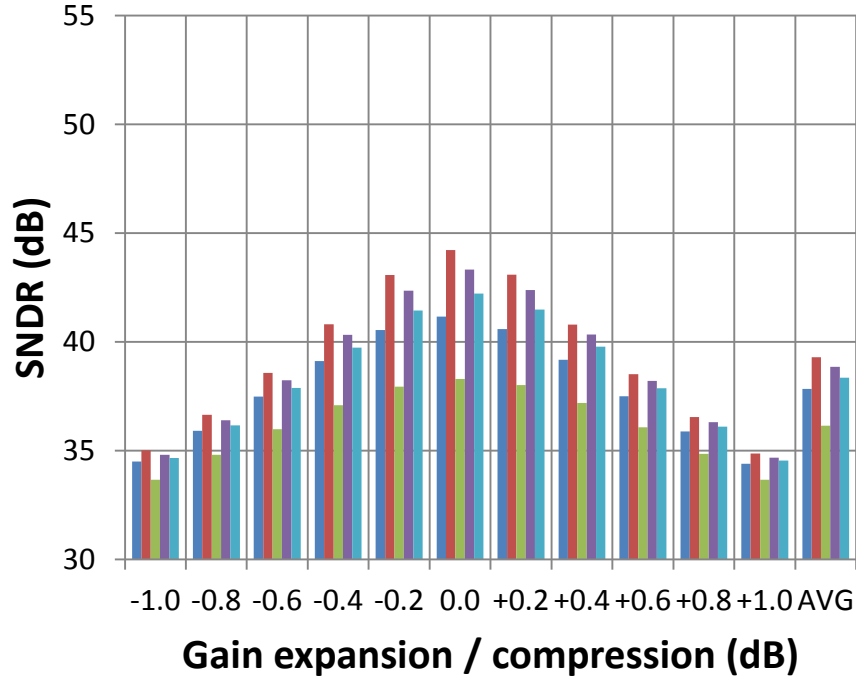
Level sep. mismatch ratio  $R_{LM}$  (zp=30mm)



# SNDR (zp=30mm)

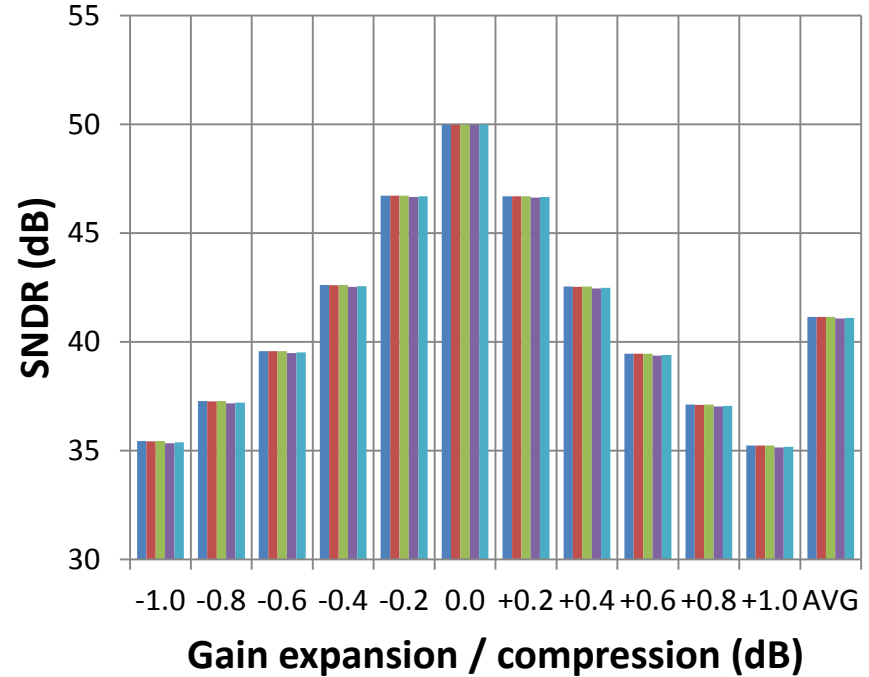
- Less dependent on package parameters as expected
  - For the linear case, we can see the noise floor (50dB in this simulation)

### SNDR (zp=30mm, Np=13)



■ #5 Rd=45 Zc=90   ■ #6 Rd=45 Zc=110   ■ #7 Rd=55 Zc=90  
■ #8 Rd=55 Zc=110   ■ #10 Rd=50 Zc=100

### SNDR (zp=30mm, Np=200)



■ #5 Rd=45 Zc=90   ■ #6 Rd=45 Zc=110   ■ #7 Rd=55 Zc=90  
■ #8 Rd=55 Zc=110   ■ #10 Rd=50 Zc=100

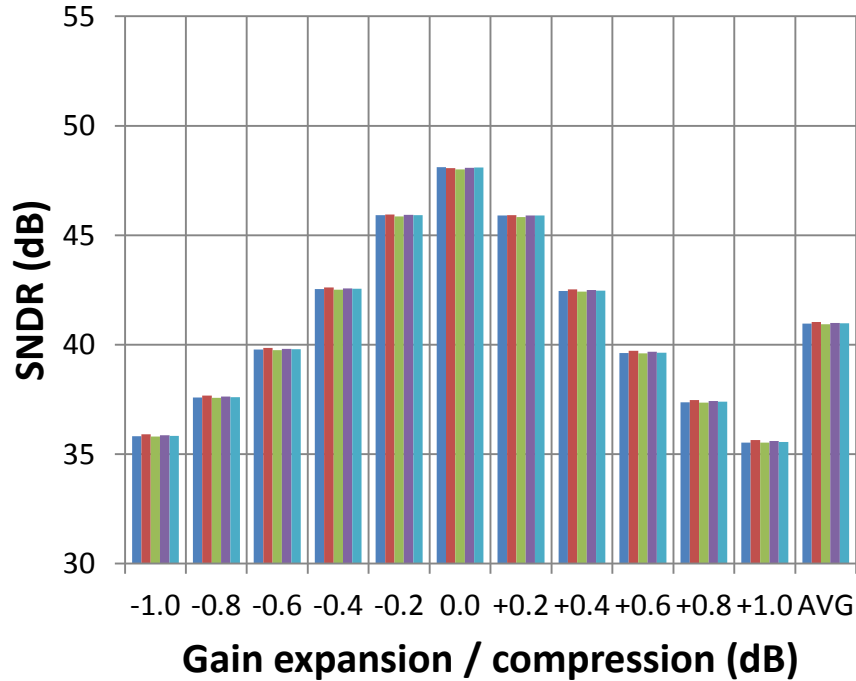


# SNDR (zp=12mm)

■ Improved as expected

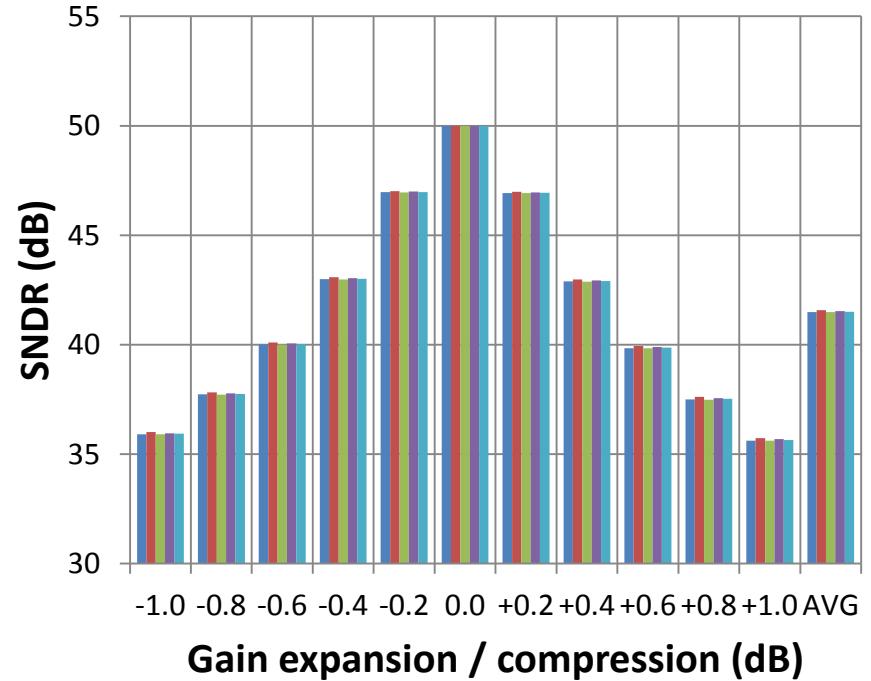
■ For the linear case, we can see the noise floor (50dB in this simulation)

### SNDR (zp=12mm, Np=13)



■ #1 Rd=45 Zc=90 ■ #2 Rd=45 Zc=110 ■ #3 Rd=55 Zc=90  
■ #4 Rd=55 Zc=110 ■ #9 Rd=50 Zc=100

### SNDR (zp=12mm, Np=200)



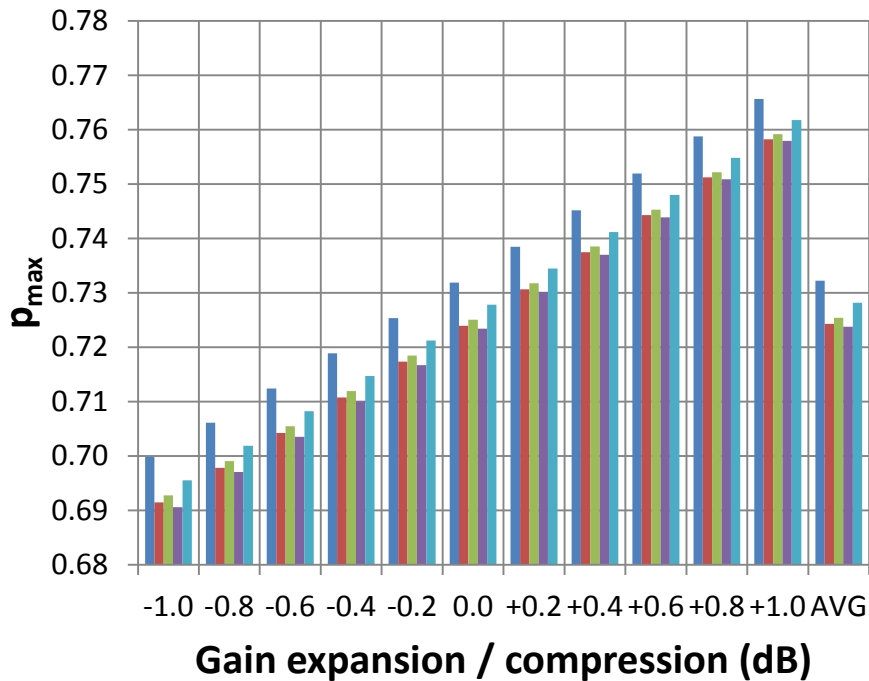
■ #1 Rd=45 Zc=90 ■ #2 Rd=45 Zc=110 ■ #3 Rd=55 Zc=90  
■ #4 Rd=55 Zc=110 ■ #9 Rd=50 Zc=100

# Linear Fit Pulse Peak $p_{\max}$ ( $z_p=30\text{mm}$ )

■ Almost no effect

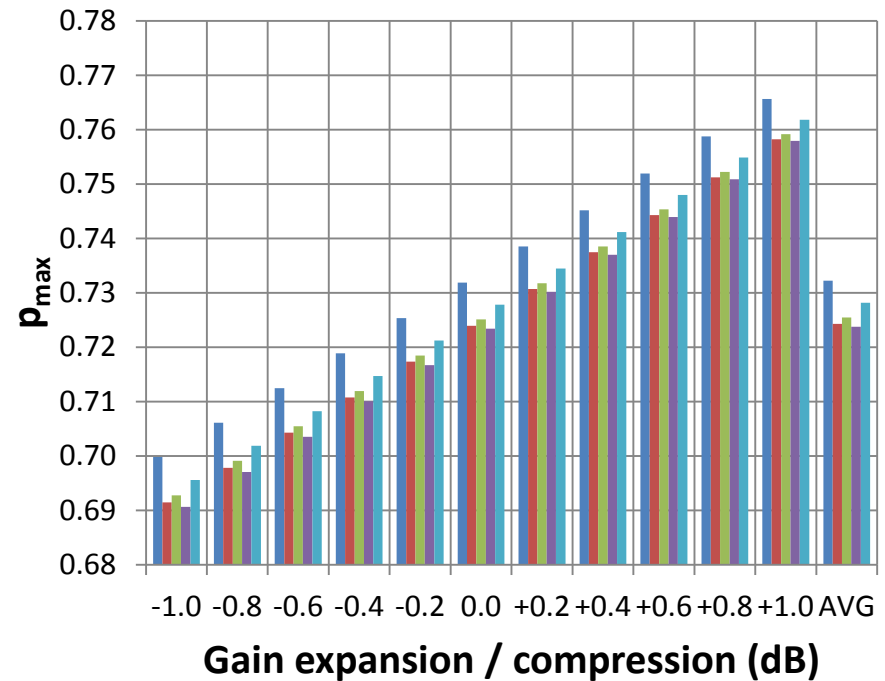
■ The average effect was 0.0011%

### $p_{\max}$ ( $z_p=30\text{mm}$ , $N_p=13$ )



■ #5 Rd=45 Zc=90   ■ #6 Rd=45 Zc=110   ■ #7 Rd=55 Zc=90  
■ #8 Rd=55 Zc=110   ■ #10 Rd=50 Zc=100

### $p_{\max}$ ( $z_p=30\text{mm}$ , $N_p=200$ )



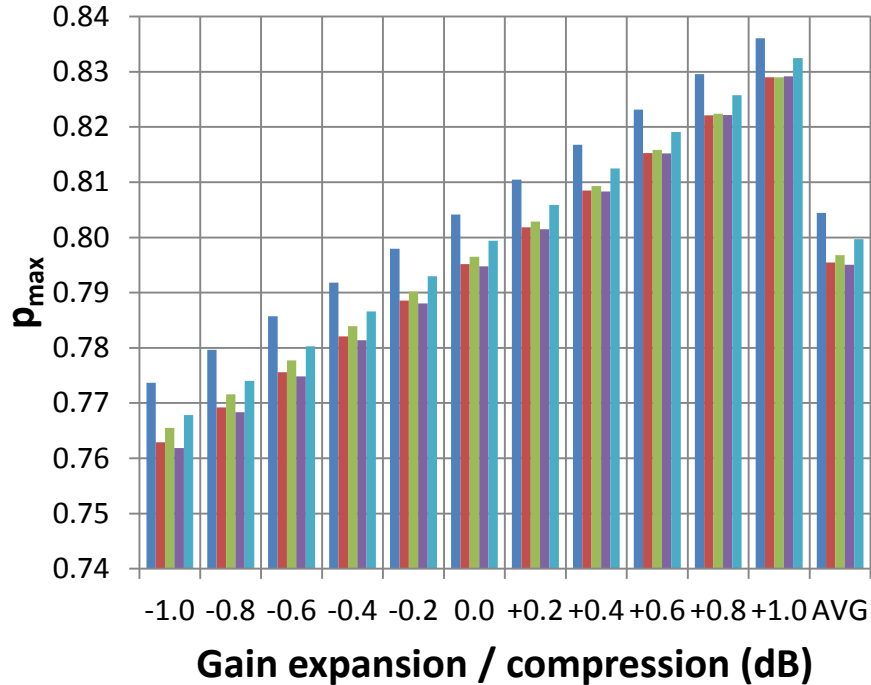
■ #5 Rd=45 Zc=90   ■ #6 Rd=45 Zc=110   ■ #7 Rd=55 Zc=90  
■ #8 Rd=55 Zc=110   ■ #10 Rd=50 Zc=100

# Linear Fit Pulse Peak $p_{\max}$ ( $z_p=12\text{mm}$ )

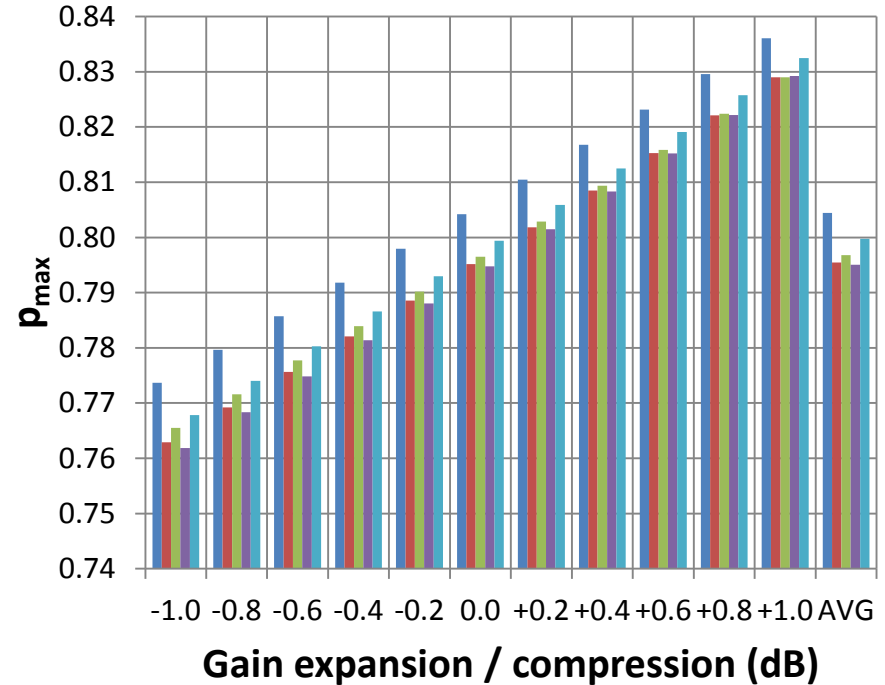
■ Almost no effect

■ The average effect was 0.00047%

$p_{\max}$  ( $z_p=12\text{mm}$ ,  $N_p=13$ )



$p_{\max}$  ( $z_p=12\text{mm}$ ,  $N_p=200$ )

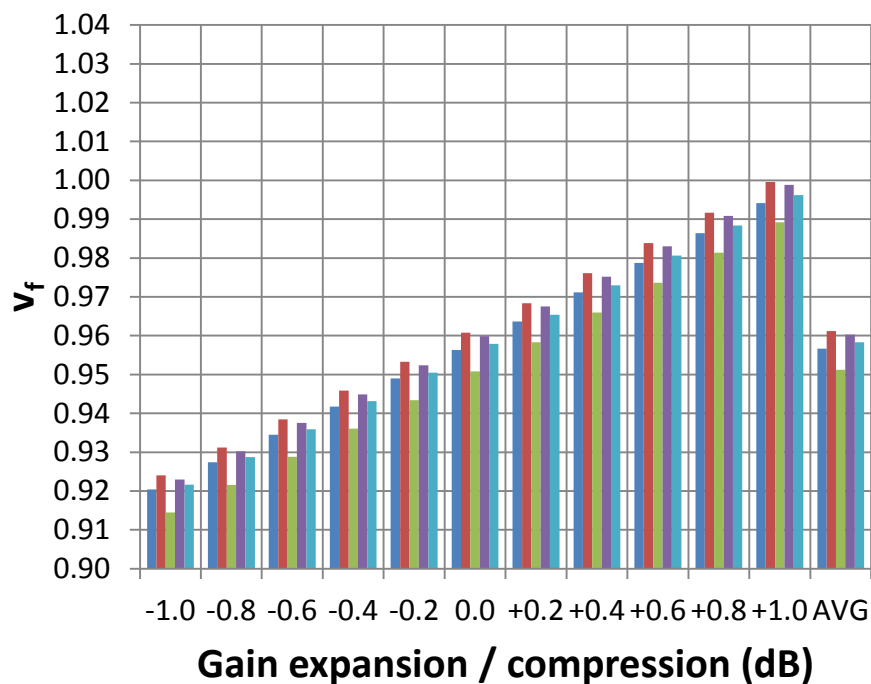


# Steady-State Voltage $v_f$ ( $z_p=30\text{mm}$ )

## ■ Non-negligible increase

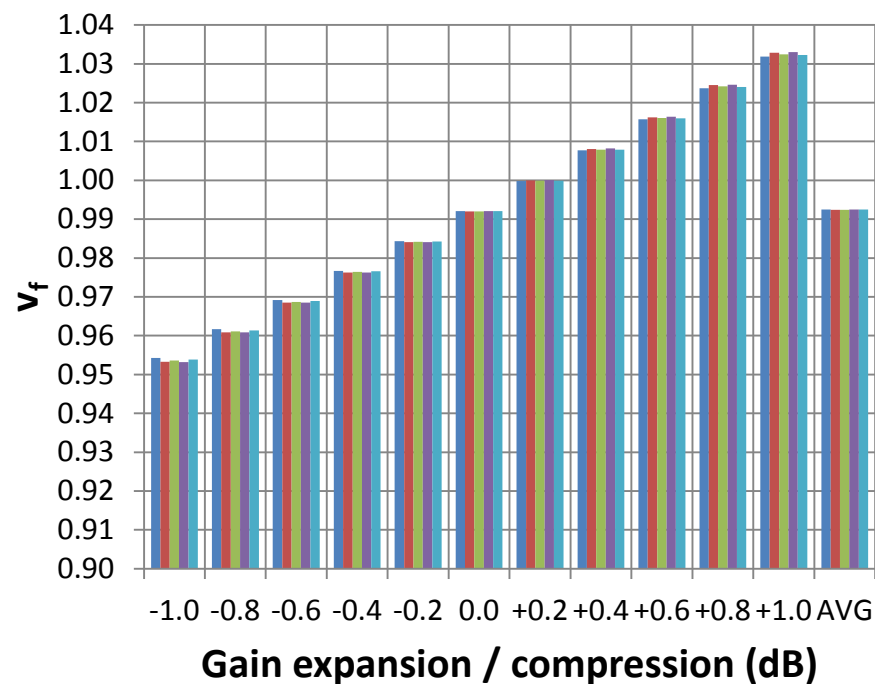
■ Because a longer fitted pulse captures more long-term ISI

$v_f$  ( $z_p=30\text{mm}$ ,  $N_p=13$ )



■ #5 Rd=45 Zc=90   ■ #6 Rd=45 Zc=110   ■ #7 Rd=55 Zc=90  
■ #8 Rd=55 Zc=110   ■ #10 Rd=50 Zc=100

$v_f$  ( $z_p=30\text{mm}$ ,  $N_p=200$ )



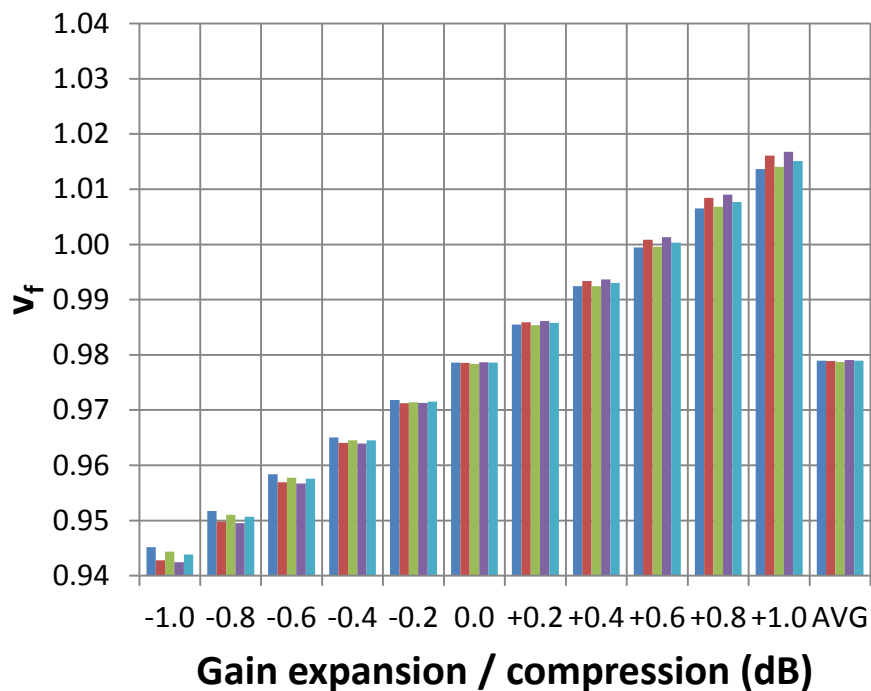
■ #5 Rd=45 Zc=90   ■ #6 Rd=45 Zc=110   ■ #7 Rd=55 Zc=90  
■ #8 Rd=55 Zc=110   ■ #10 Rd=50 Zc=100

# Steady-State Voltage $v_f$ ( $z_p=12\text{mm}$ )

## ■ Non-negligible increase

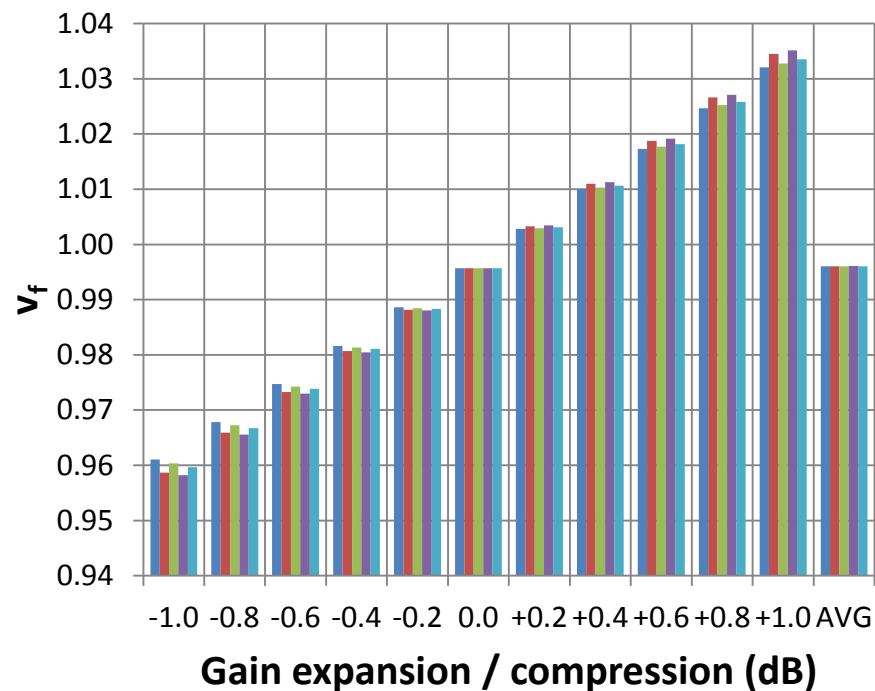
■ Because a longer fitted pulse captures more long-term ISI

### $v_f$ ( $z_p=12\text{mm}$ , $N_p=13$ )



■ #1 Rd=45 Zc=90 ■ #2 Rd=45 Zc=110 ■ #3 Rd=55 Zc=90  
■ #4 Rd=55 Zc=110 ■ #9 Rd=50 Zc=100

### $v_f$ ( $z_p=12\text{mm}$ , $N_p=200$ )



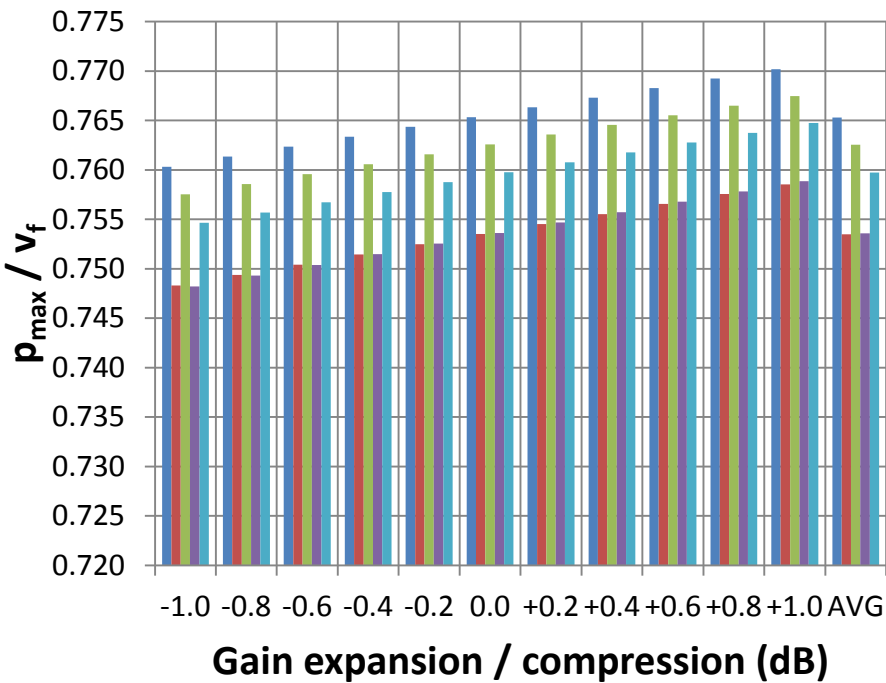
■ #1 Rd=45 Zc=90 ■ #2 Rd=45 Zc=110 ■ #3 Rd=55 Zc=90  
■ #4 Rd=55 Zc=110 ■ #9 Rd=50 Zc=100

# Ratio of $p_{\max}$ to $v_f$ ( $z_p=30\text{mm}$ )

## ■ Reduced

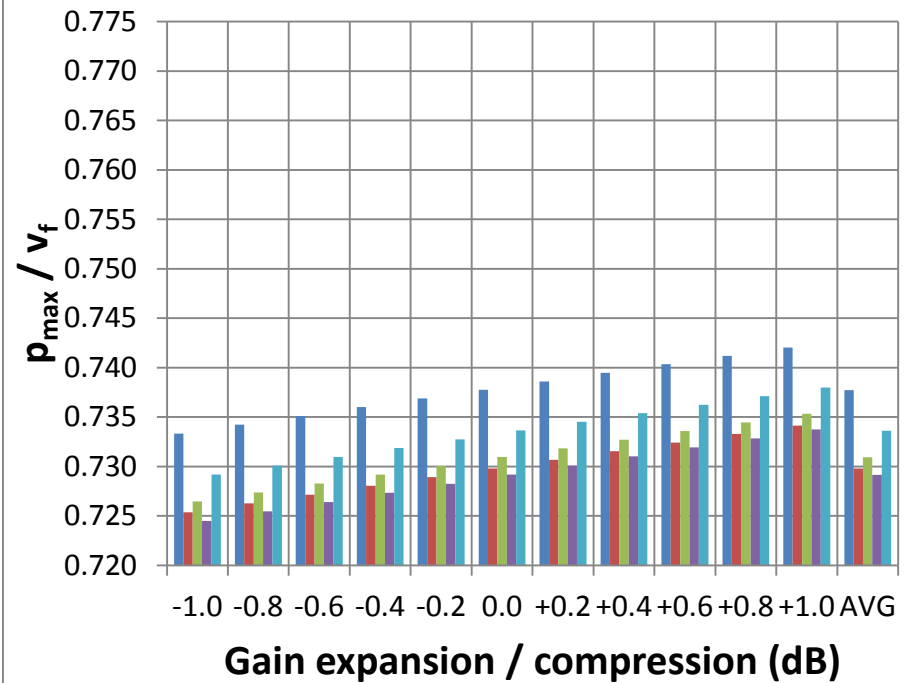
■ Because  $v_f$  increases while  $p_{\max}$  does not change

$p_{\max} / v_f$  ( $z_p=30\text{mm}$ ,  $N_p=13$ )



■ #5 Rd=45 Zc=90   ■ #6 Rd=45 Zc=110   ■ #7 Rd=55 Zc=90  
 ■ #8 Rd=55 Zc=110   ■ #10 Rd=50 Zc=100

$p_{\max} / v_f$  ( $z_p=30\text{mm}$ ,  $N_p=200$ )



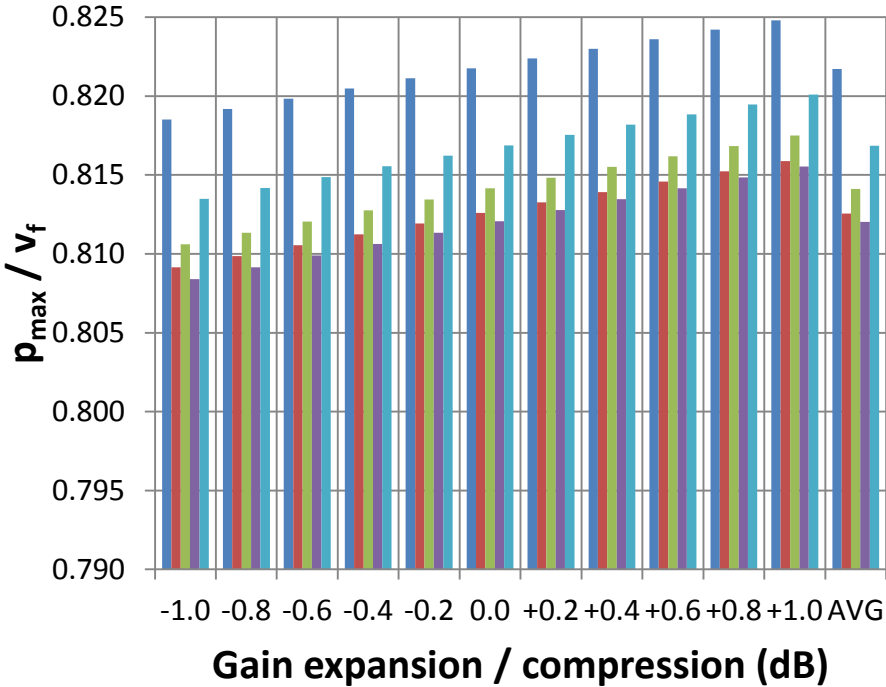
■ #5 Rd=45 Zc=90   ■ #6 Rd=45 Zc=110   ■ #7 Rd=55 Zc=90  
 ■ #8 Rd=55 Zc=110   ■ #10 Rd=50 Zc=100

# Ratio of $p_{\max}$ to $v_f$ ( $z_p=12\text{mm}$ )

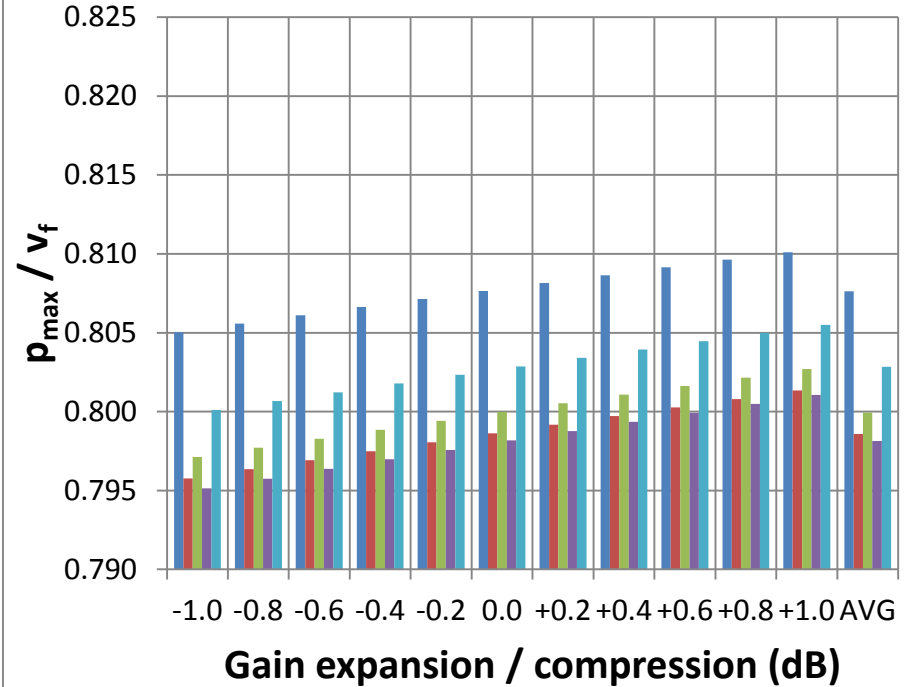
## ■ Reduced

■ Because  $v_f$  increases while  $p_{\max}$  does not change

$p_{\max} / v_f$  ( $z_p=12\text{mm}$ ,  $N_p=13$ )



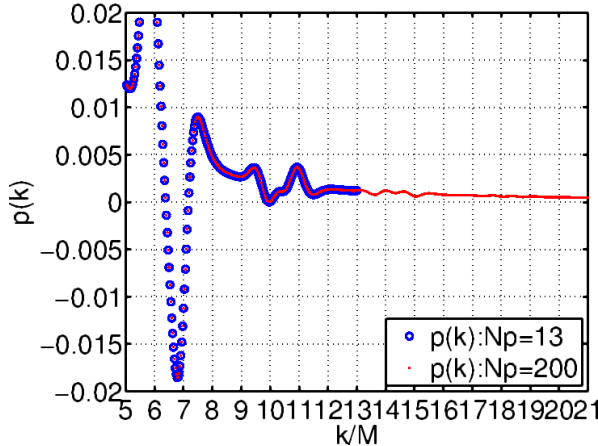
$p_{\max} / v_f$  ( $z_p=12\text{mm}$ ,  $N_p=200$ )



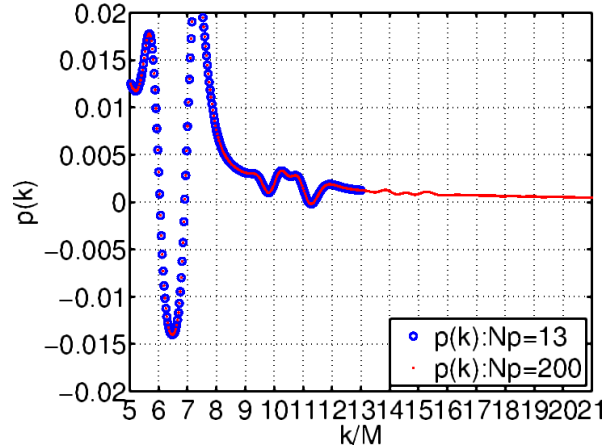
# Linear Fit Pulse $p(k)$

■  $p(k)$  does not change for  $k \leq 13 \cdot M$  between  $N_p=13$  and  $N_p=200$

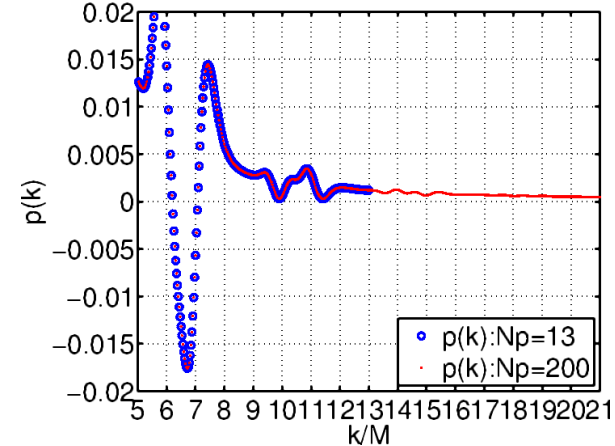
#2:  $Z_p=12, R_d=45, Z_c=110$   
zp12 rd45 zc110 gec0



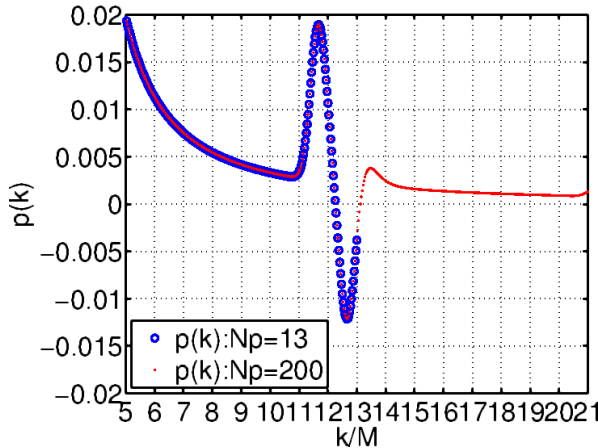
#3:  $Z_p=12, R_d=55, Z_c=90$   
zp12 rd55 zc90 gec0



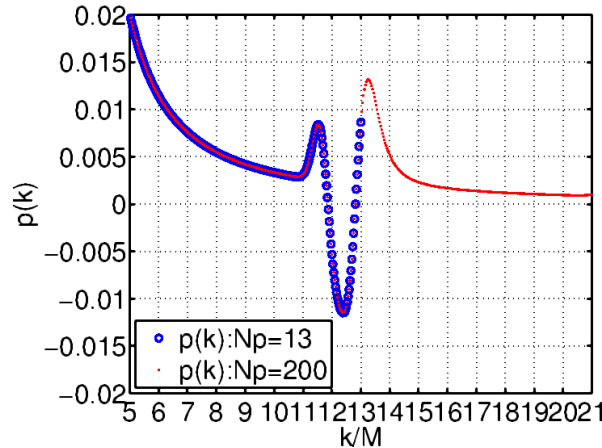
#9:  $Z_p=12, R_d=50, Z_c=100$   
zp12 rd50 zc100 gec0



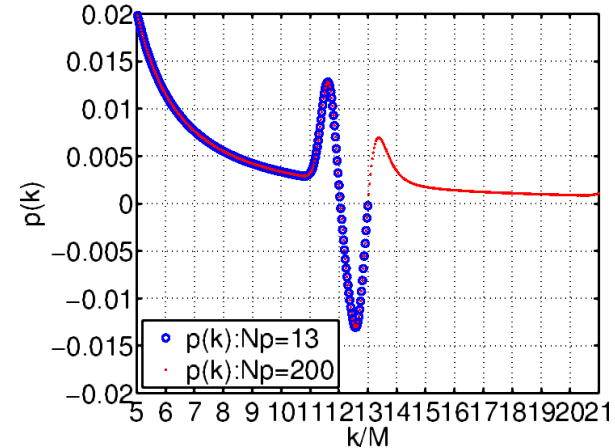
#6:  $Z_p=30, R_d=45, Z_c=110$   
zp30 rd45 zc110 gec0



#7:  $Z_p=30, R_d=55, Z_c=90$   
zp30 rd55 zc90 gec0



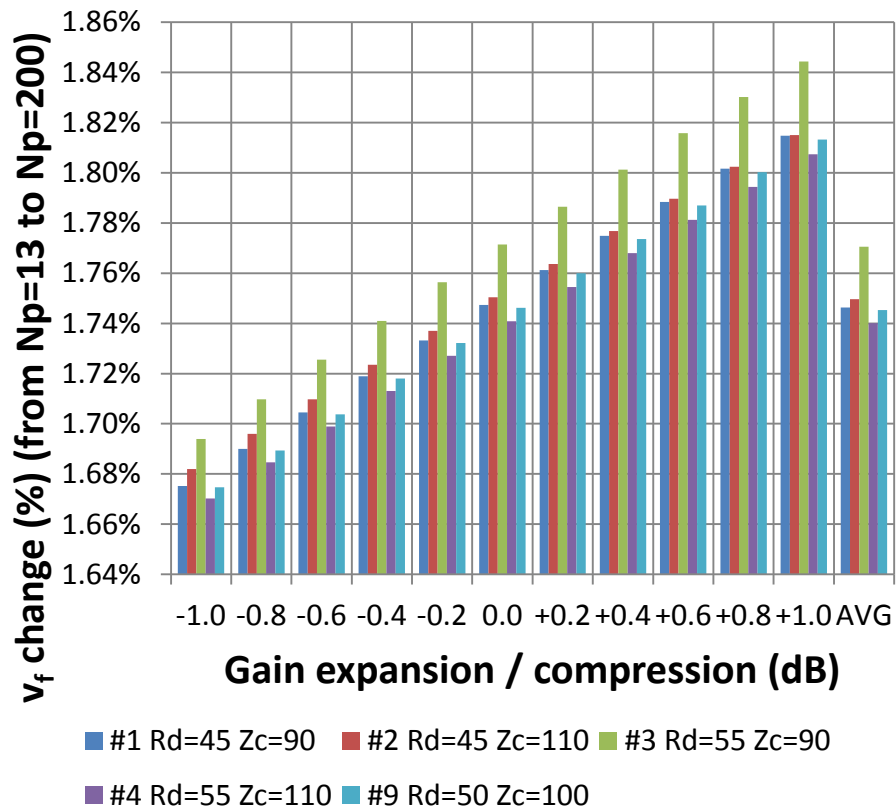
#10:  $Z_p=30, R_d=50, Z_c=100$   
zp30 rd50 zc100 gec0



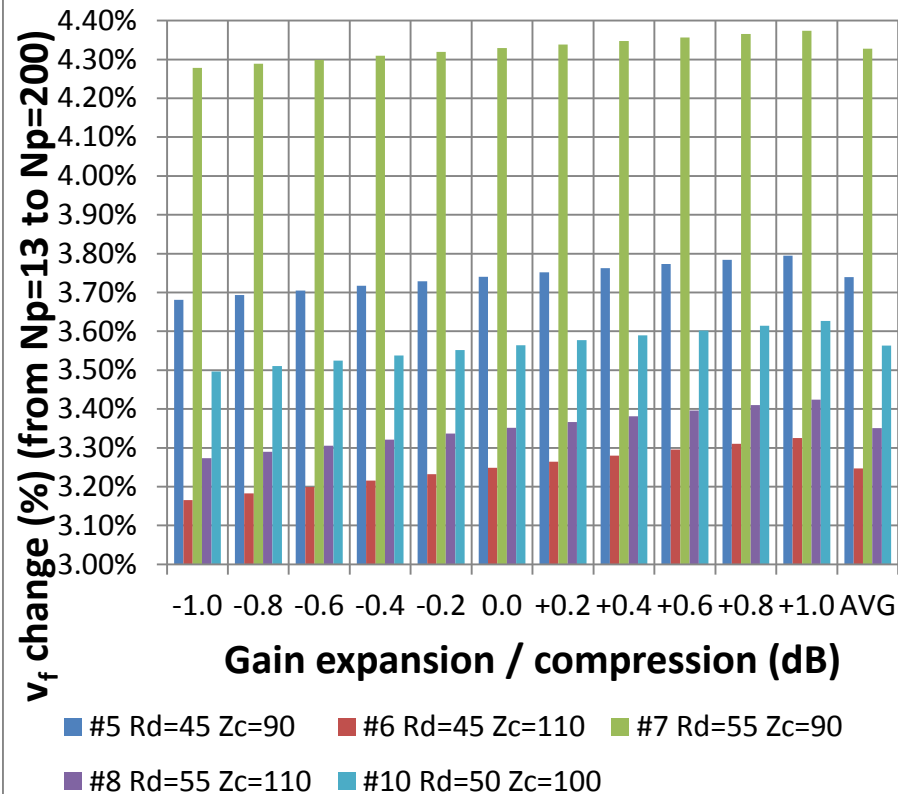


# Change of Steady-State Voltage $v_f$

$v_f$  change (zp=12mm, from Np=13 to Np=200)



$v_f$  change (zp=30mm, from Np=13 to Np=200)

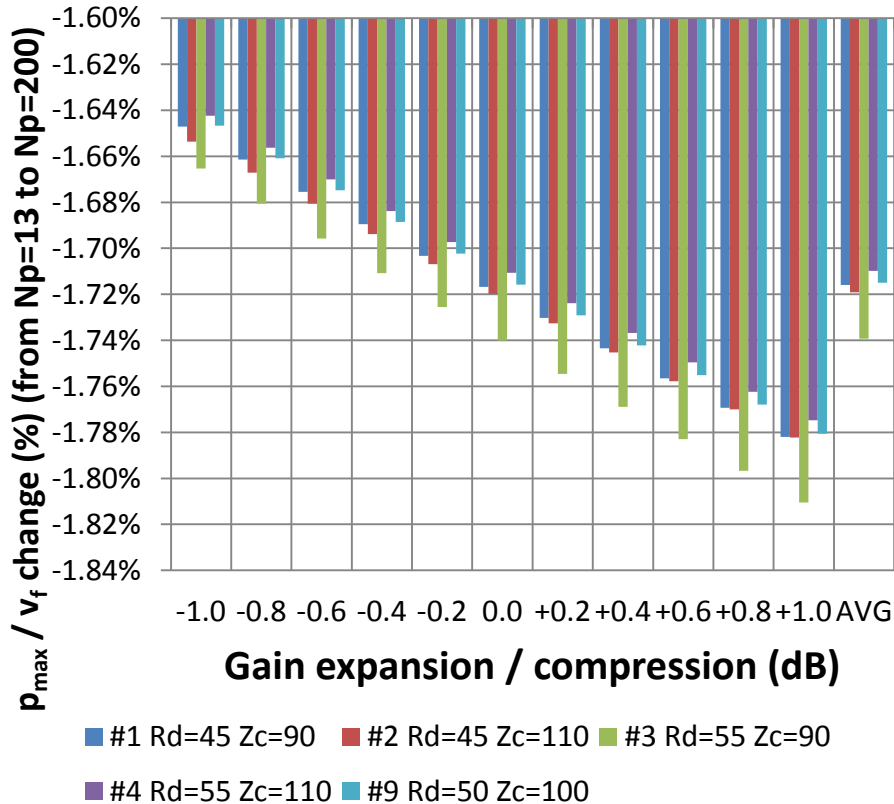


Condition	#3 (Rd=55, Zc=90)	AVG (#1,2,3,4,9)
Change	+1.7706%	+1.7504%
0.6V (max) in D2.1	0.61062	0.61050

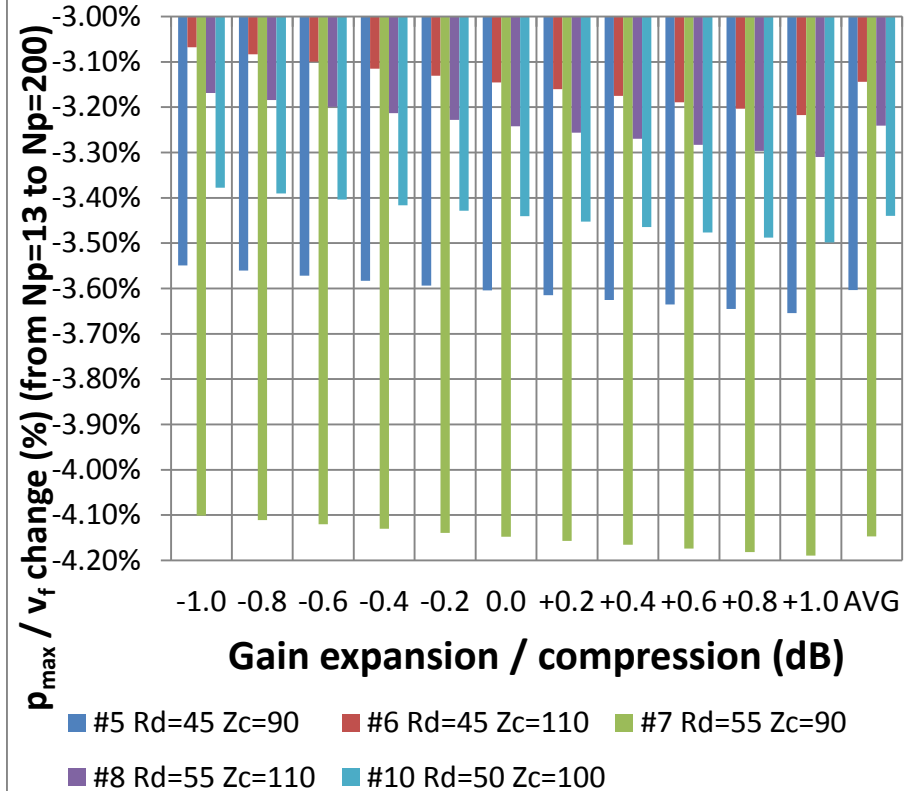
Condition	#7 (Rd=55, Zc=90)	AVG (#5,6,7,8,10)
Change	+4.3279%	+3.6456%
0.4V (max) in D2.1	0.41731	0.41458

# Change of Ratio of $p_{\max}$ to $v_f$

$p_{\max} / v_f$  change (zp=12mm, from Np=13 to Np=200)



$p_{\max} / v_f$  change (zp=30mm, from Np=13 to Np=200)



Condition	#3 (Rd=55, Zc=90)	AVG (#1,2,3,4,9)
Change	-1.7393%	-1.7198%

Condition	#7 (Rd=55, Zc=90)	AVG (#5,6,7,8,10)
Change	-4.1471%	-3.5151%
0.736 (min) in D2.1	0.705477	0.710129

- Recommended changes based on the results for #3 and #7
  - Change the Steady state voltage  $v_f$  (max)
    - from 0.6 V to 0.611 V
  - Change the Steady state voltage  $v_f$  (min)
    - from 0.4 V to 0.417 V
  - Change the Linear fit pulse peak (min)
    - from  $0.736 \times v_f$  to  $0.705 \times v_f$
  
- Or, recommended changes based on the average results
  - Change the Steady state voltage  $v_f$  (max)
    - from 0.6 V to 0.611 V
  - Change the Steady state voltage  $v_f$  (min)
    - from 0.4 V to 0.415 V
  - Change the Linear fit pulse peak (min)
    - from  $0.736 \times v_f$  to  $0.710 \times v_f$

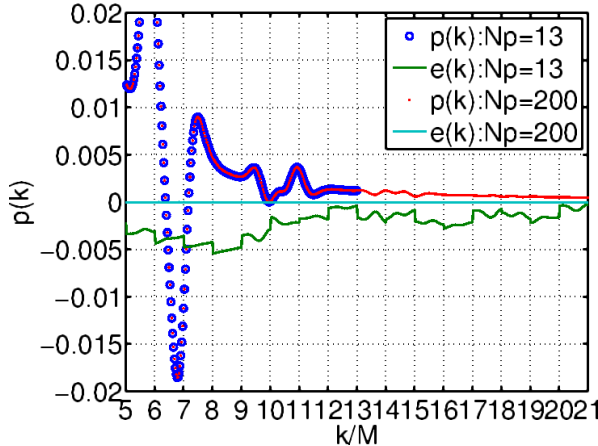
# Back up Slides

- Linear Fit Pulse & Error (Linear)
- Linear Fit Pulse & Error (Non-linear)

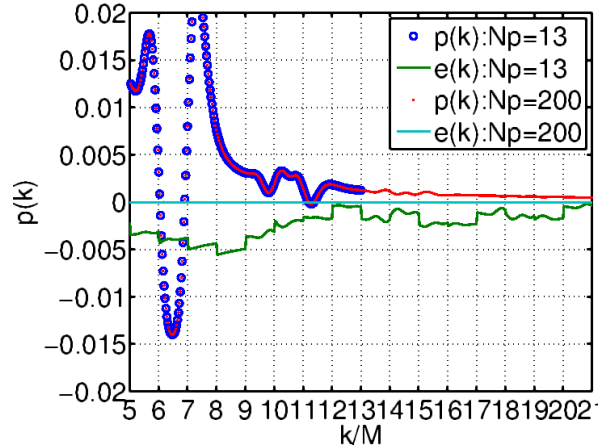
# Linear Fit Pulse & Error (Linear)

■  $p(k)$  after  $N_p$  (i.e.  $k/M > N_p$ ) is translated to  $e(k)$

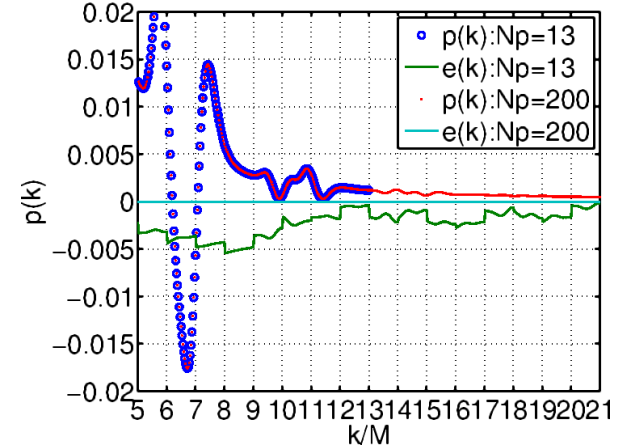
#2:  $Z_p=12, R_d=45, Z_c=110$   
zp12 rd45 zc110 gec0



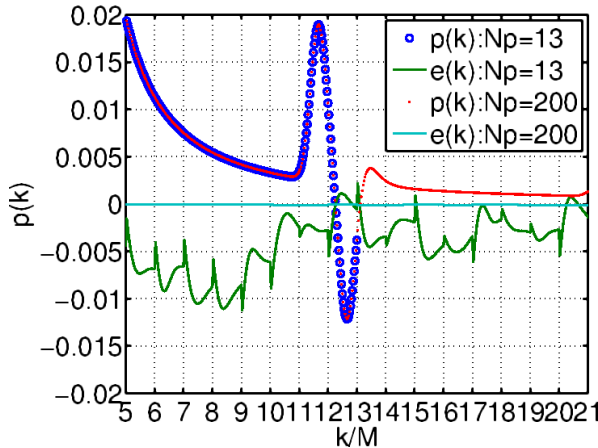
#3:  $Z_p=12, R_d=55, Z_c=90$   
zp12 rd55 zc90 gec0



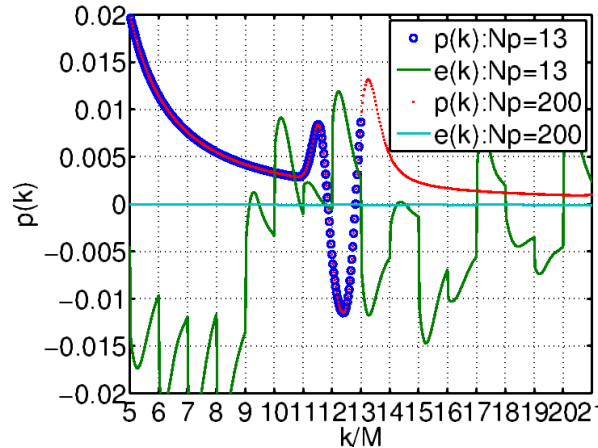
#9:  $Z_p=12, R_d=50, Z_c=100$   
zp12 rd50 zc100 gec0



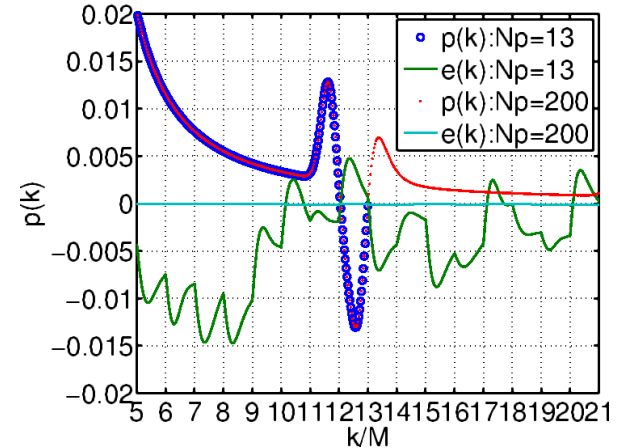
#6:  $Z_p=30, R_d=45, Z_c=110$   
zp30 rd45 zc110 gec0



#7:  $Z_p=30, R_d=55, Z_c=90$   
zp30 rd55 zc90 gec0



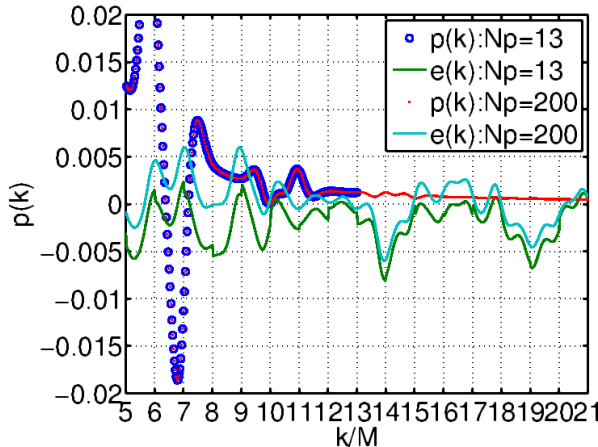
#10:  $Z_p=30, R_d=50, Z_c=100$   
zp30 rd50 zc100 gec0



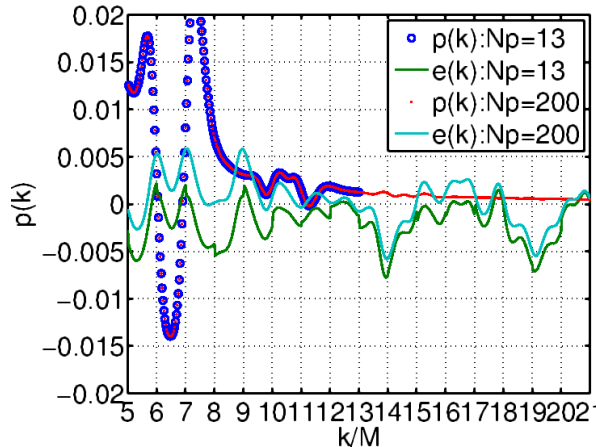
# Linear Fit Pulse & Error (Non-Linear)

■  $e(k)$  represents non-linearity plus  $p(k)$  after  $N_p$

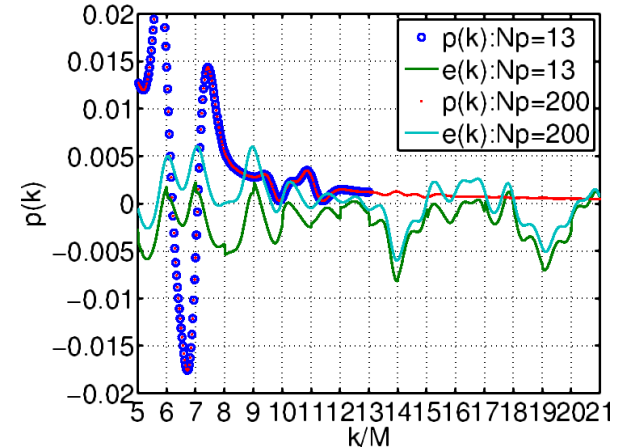
#2:  $Z_p=12, R_d=45, Z_c=110$   
zp12 rd45 zc110 gec0.2



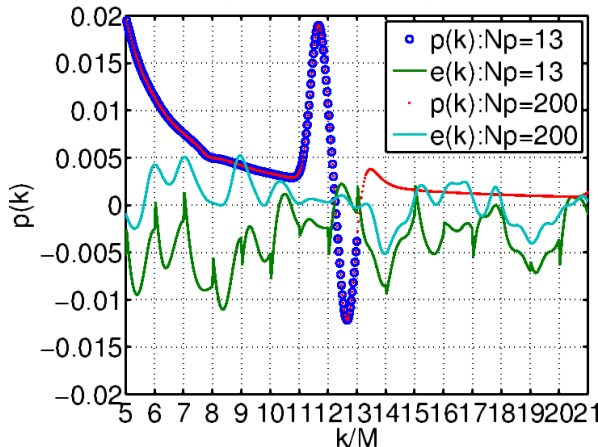
#3:  $Z_p=12, R_d=55, Z_c=90$   
zp12 rd55 zc90 gec0.2



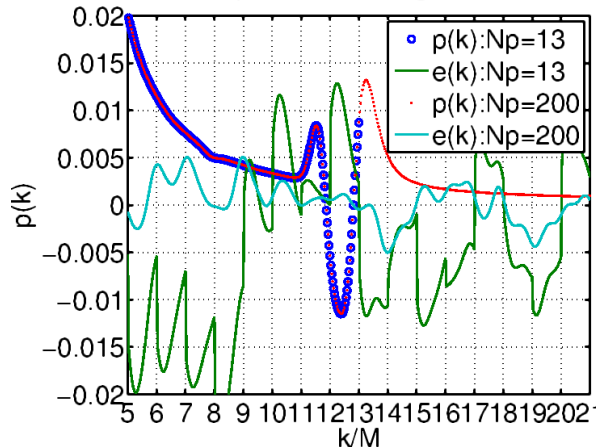
#9:  $Z_p=12, R_d=50, Z_c=100$   
zp12 rd50 zc100 gec0.2



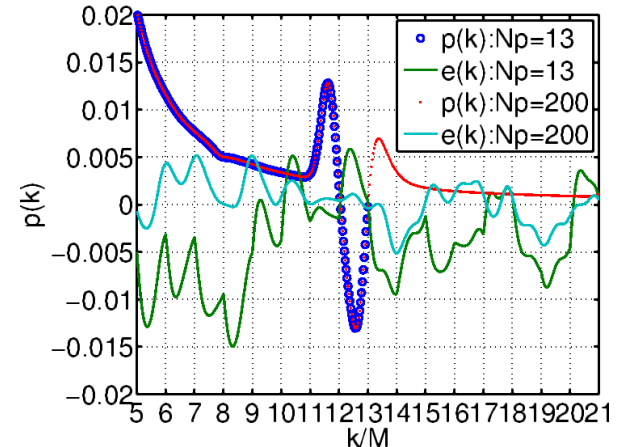
#6:  $Z_p=30, R_d=45, Z_c=110$   
zp30 rd45 zc110 gec0.2



#7:  $Z_p=30, R_d=55, Z_c=90$   
zp30 rd55 zc90 gec0.2



#10:  $Z_p=30, R_d=50, Z_c=100$   
zp30 rd50 zc100 gec0.2



# Thank you