

IEEE P802.3cd 50 Gb/s, 100 Gb/s, 200 Gb/s Ethernet Initial Sponsor ballot comments

Cl 000 SC 000 P L # i-2
Marris, Arthur Cadence Design Syste

Comment Type ER Comment Status A <bucket>

Update the editing instructions throughout the document to reference the new revision to the base standard, due to be published in 2018. Also do this on future drafts of 802.3cd to take into account future changes to the revision project draft standard.

SuggestedRemedy

Update editing instructions in draft 3.0 and future drafts to align with the new base standard.

Response Response Status W

ACCEPT.

Cl 000 SC 000 P L # i-12
Anslow, Peter Ciena Corporation

Comment Type TR Comment Status A editor's notes <cc>

The vote in Sponsor ballot is essentially a response to the question "Do you support sending this draft to RevCom?".

The draft contains five editor's notes:

Clause 136 "Editor's note: The values for SNDR, SNR_ISI, and SNR_TX require confirmation and may change."

Clause 136 "Editor's note: The value for Zc requires confirmation and may change."

Clause 138 "Editor's note: The values for OMAouter, OMAouter minus TDECQ, and TDECQ require confirmation and may change."

Clause 138 "Editor's note: The values for SRS, receiver sensitivity, and SEC require confirmation and may change."

Clause 138 "Editor's note: The values for link budget and allocation for penalties require confirmation and may change."

While any of these editor's notes remain, I do not support sending the draft to RevCom since they would not be likely to recommend approval of the draft.

SuggestedRemedy

Do whatever work is necessary (which may be none) and remove these five editor's notes.

Response Response Status W

ACCEPT IN PRINCIPLE.

The two editor's notes in clause 136 have been addressed by http://www.ieee802.org/3/cd/public/Jan18/dudek_3cd_01_0118.pdf.

Remove all editor's notes in cause 136.

Relating to the editor's notes in Clause 138, measured data has been presented to the task force supporting the current specifications.

See:

http://www.ieee802.org/3/cd/public/Jan18/king_3cd_02_0118.pdf

http://www.ieee802.org/3/cd/public/adhoc/archive/chang_011018_3cd_02_adhoc-v2.pdf

Remove all editor's notes in Clause 138.

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Cl 000 SC 000 P L # i-14
Anslow, Peter Ciena Corporation

Comment Type E Comment Status A <bucket>

Some external cross-references are shown in black text, but should have character tag "External" applied to them.

SuggestedRemedy

Apply character tag "External" to:
"Equation (93A-19)" page 231, line 12
"83A", "83B", "83D", "83E", page 309, lines 25 to 30

Response Response Status C

ACCEPT.

Cl 000 SC 000 P L # i-37
RAN, ADEE Intel Corporation

Comment Type E Comment Status A <bucket>

The convention in most of 802.3 text is that the acronym FEC is preceded by the article "an" rather than "a".

See comment i-19 in
http://www.ieee802.org/3/by/public/comments/8023by_D30_comment_final_responses_by_ID_v2.pdf.

SuggestedRemedy

Change "a FEC" to "an FEC" in the following:

133.5.3
134.5.4.2.3
136.9.4.1

Response Response Status C

ACCEPT.

Cl 000 SC 000 P L # i-9
Anslow, Peter Ciena Corporation

Comment Type E Comment Status A <bucket>

Some cross-references in the draft are in forest green although the target is in the draft.

SuggestedRemedy

Change references to Clause 73 to be cross-references in the following places:
Page 90, line 32 (73.5.1)

Change references to Clause 82 to be cross-references in the following places:
Page 266, line 3 (80.5), line 4 (Figure 80-8), and line 18 (80.5)

Change references to Clause 82 to be cross-references in the following places:
Page 262, line 8

Change references to Clause 91 to be cross-references in the following places:
Page 87, line 48

Page 104, line 36 (91.5.3.1)

Page 105, line 40 (91.5.3.1)

Page 232, line 19 (91.6)

Change references to Clause 120 to be cross-references in the following places:

Page 40, line 36

Page 85, line 41

Page 87, line 8

Page 95, line 54

Page 96, lines 5, 7, and 8

Page 119, lines 8 and 31

Page 198, line 38

Page 246, line 38

Page 262, line 41

Change references to Clause 119 to be cross-references in the following places:

Page 85, line 40

Page 87, lines 8 and 49

Page 199, line 9

Page 245, line 54

Page 262, line 39

Response Response Status C

ACCEPT.

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CI 000 SC 000 P L # i-20
 Anslow, Peter Ciena Corporation

Comment Type E Comment Status A <bucket>

Tables that split across two pages need the bottom ruling on the first page set to "very thin" and the table continuation variable applied to the heading.

SuggestedRemedy

Make the bottom ruling change to all such tables in the draft, including Tables 134-2, 135-2, 135-4, 136-5, 136-6 (2 places), 136-11, 136-15, 137-5, 138-9, 139-6, 140-6, 93A-2, 136C-3, the tables in 134.7.4.1, 134.7.4.2, 136.14.3, 136.14.4.3, 136.14.4.5, 137.12.3, 137.12.4.1, 137.12.4.3, 138.11.4.1, 139.11.4.1, 140.11.4.1, 135E.5.4.1, 135F.6.4.1
 Add the table continuation variable to the heading of Table 93A-2.

Response Response Status C
 ACCEPT.

CI 000 SC 000 P L # i-86
 RAN, ADEE Intel Corporation

Comment Type E Comment Status A

The style manual (Presentation of data and table format, 13.3.2) says: "All numbers should be aligned at the decimal point". This is not always followed (e.g. table 131-4).

It also says "Digits should be separated into groups of three [with space separating], counting from the decimal point toward the left and right". In this draft this is sometimes followed (e.g. table 131-4) and sometimes not (Table 80-5).

The style manual does not require numbers outside of tables to be three-digit-grouped, either left or right of the decimal point. In this draft this is usually done for large integers (left of the decimal point), but not done for fractions (right of the decimal point). The readability of numbers outside of tables is not improved by this grouping.

We should consistently follow the stated table convention, and choose a convention for non-table data.

SuggestedRemedy

Go over all tables and format according to 13.3.2 in the style manual.

Go over numbers in the text and remove the three-digit grouping.

Response Response Status C
 ACCEPT IN PRINCIPLE.

The number formatting in all legacy (amended) clauses and annexes is purposely consistent with the formatting in the base standard. Concerns with this formatting should be addressed against the base standard.

D2.0 comment #2 addressed this topic as follows:

<start of response to D2.0 comment #2>

According to the "2014 IEEE-SA Standards Style Manual", a space for thousand separators are required for numbers in tables. It gives no guidance for numbers outside of tables.

<https://development.standards.ieee.org/myproject/Public/mytools/draft/styleman.pdf>

The "IEEE Editorial Style Manual" provides the following general (not specific to tables) guidance:

"7) Use thin spaces instead of commas between numbers in tens or hundreds of thousands (e.g., 62 000, 100 000, but 4000). "

https://www.ieee.org/documents/style_manual.pdf

P802.3cj (802.3 revision) includes a thousands-separator space in most cases for numbers 10 000 and greater.

Throughout the draft, for all numbers outside of tables less than 10000 in new text remove the thousands-separator space and for number 10000 or greater add a space, if necessary.

<end of response to D2.0 comment #2>

For all new clauses and annexes...

For all numbers in text outside of tables less than 10000 remove the thousands-separator

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space and for numbers 10000 or greater add a space, if necessary; and no spaces will be added to digits to the right of the decimal point.

Within tables, follow the rules in the style guide for space between digits to the left of the decimal point; no spaces will be added to digits to the right of the decimal point; and do not force alignment at the decimal point.

Cl 000 SC 000 P95 L1 # i-113
 Maytum, Michael RETIRED/unemployed

Comment Type E Comment Status A <bucket>
 Energy-Efficient

SuggestedRemedy
 make Energy Efficient to match other 11 occurrences

Response Response Status C
 ACCEPT IN PRINCIPLE.

Replace all instance of "Energy Efficient Ethernet" with "Energy-Efficient Ethernet".

See comments i-111 and i-112.

[Editor's note: References to i-111 and i-112 are intended to point out other comments dealing with the same subject matter.]

Cl 000 SC 000 P97 L13 # i-109
 Maytum, Michael RETIRED/unemployed

Comment Type E Comment Status R <bucket>
 64-bit wide

SuggestedRemedy
 make 64-bit-wide to match other occurrences

Response Response Status C
 REJECT.

The occurrence of "64-bit wide" in Clause 80 is in unchanged text from Clause 80. Any changes to this text are out of scope for this project and must be addressed against the base standard through the revision project or maintenance process.

All other occurrences are in new clauses and are consistently written as "64-bit-wide".

Cl 000 SC 000 P183 L5 # i-110
 Maytum, Michael RETIRED/unemployed

Comment Type E Comment Status A <bucket>
 bit-times

SuggestedRemedy
 make bit times to match other 24 occurrences

Response Response Status C
 ACCEPT IN PRINCIPLE.

On page 183 line 5, change "bit-times" to "bit times".

Cl 000 SC 000 P199 L16 # i-111
 Maytum, Michael RETIRED/unemployed

Comment Type E Comment Status A <bucket>
 Energy-Efficient

SuggestedRemedy
 make Energy Efficient to match other 11 occurrences

Response Response Status C
 ACCEPT IN PRINCIPLE.

Replace all instances of "Energy Efficient Ethernet" with "Energy-Efficient Ethernet".

See comments i-112 and i-113.

[Editor's note: References to i-112 and i-113 are intended to point out other comments dealing with the same subject matter.]

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CI 000 SC 000 P247 L1 # i-112
 Maytum, Michael RETIRED/unemployed
 Comment Type E Comment Status A <bucket>
 Energy-Efficient
 SuggestedRemedy
 make Energy Efficient to match other 11 occurrences
 Response Response Status C
 ACCEPT IN PRINCIPLE.
 Replace all instances of "Energy Efficient Ethernet" with "Energy-Efficient Ethernet".
 See comments i-111 and i-113.
 [Editor's note: References to i-111 and i-113 are intended to point out other comments dealing with the same subject matter.]

CI 000 SC 4.4.2 P41 L8 # i-103
 Healey, Adam Broadcom Ltd.
 Comment Type E Comment Status A
 IEEE P802.3cd will end up being an amendment to IEEE Std 802.3-201x (and not IEEE Std 802.3-2015 as modified by...). It is expected that all amendments except IEEE P802.3bt, IEEE P802.3cb, and IEEE P802.3cd (and, of course, any subsequent amendments) will be part of the base document and should not be called out in the frontmatter and editing instructions. It is also necessary to track relevant changes made to these amendments during the IEEE P802.3 (IEEE 802.3cj) ballot (some such changes have been submitted as separate comments).
 SuggestedRemedy
 At a convenient point in the process, align the draft to the expected base document.
 Response Response Status C
 ACCEPT IN PRINCIPLE.
 [Editor changed Clause from 4 to 000.]
 Align the 802.3cd draft 3.1 with 802.3cj revision.
 Incorporate relevant changes made to the P802.3cb amendment and new base standard during the IEEE P802.3 (IEEE 802.3cj) ballot.

CI 001 SC 1.4 P39 L3 # i-104
 Healey, Adam Broadcom Ltd.
 Comment Type E Comment Status A <bucket>
 The definition sort order used by IEEE 802.3 is defined at <http://www.ieee802.org/3/WG_tools/editorial/requirements/words.html> (search for "Definition sort order"). Based on this order, the specified insertion point for the definition of 100GBASE-CR2 is not correct. Also, IEEE P802.3cd will end up being an amendment to IEEE Std 802.3-201x (currently IEEE P802.3 (IEEE 802.3cj) D3.0 which is in Sponsor ballot). "100GBASE-R encoding" is not 1.4.52 in the expected base document.
 SuggestedRemedy
 Apply the correct definition sort order relative the locations of definitions in the expected base document.
 Response Response Status C
 ACCEPT IN PRINCIPLE.
 To align with the 802.3-201x revision, apply the correct definition sort order according to <http://www.ieee802.org/3/WG_tools/editorial/requirements/words.html> relative the locations of definitions in the 802.3-201x base document.

CI 030 SC 30.3.2.1.2 P42 L11 # i-65
 Marris, Arthur Cadence Design Syste
 Comment Type E Comment Status A <bucket>
 Editorial instruction should say the insertion is after 40GBASE-T rather than 40GBASE-R
 SuggestedRemedy
 Change 40GBASE-R to 40GBASE-T on lines 12 and 21 on page 42
 Response Response Status C
 ACCEPT.

CI 030 SC 30.3.2.1.5 P42 L39 # i-66
 Marris, Arthur Cadence Design Syste
 Comment Type E Comment Status A <bucket>
 The reference should be to Table 81-4 rather than 81-3
 SuggestedRemedy
 Change 81-3 to 81-4
 Response Response Status C
 ACCEPT.

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CI 030 SC 30.5.1.1.2 P42 L51 # i-67
 Marris, Arthur Cadence Design Syste
 Comment Type E Comment Status A <bucket>
 The 50G entries should go after 40GBASE-T rather than 40GBASE-FR
 SuggestedRemedy
 Change 40GBASE-FR to 40GBASE-T
 Response Response Status C
 ACCEPT.

CI 030 SC 30.6.1.1.5 P46 L21 # i-68
 Marris, Arthur Cadence Design Syste
 Comment Type E Comment Status A <bucket>
 The 50GR entry goes after 40GBASE-T rather than 40GBASE-CR4
 SuggestedRemedy
 Change 40GBASE-CR4 to 40GBASE-T
 Response Response Status C
 ACCEPT.

CI 031B SC 31B.4.6 P330 L23 # i-19
 Anslow, Peter Ciena Corporation
 Comment Type E Comment Status A <bucket>
 Comment #15 against D2.0 of the 802.3 revision project changed the format of the table in 31B.4.6. See:
<http://www.ieee802.org/3/cj/comments/P8023-D2p0-Comments-Final-byID.pdf#page=3>
 When the P802.3cd draft is changed to become an amendment to the output of the revision, equivalent changes need to be made to the P802.3cd draft.
 SuggestedRemedy
 When the P802.3cd draft is changed to become an amendment to the output of the revision: in the Value/Comment cell, apply footnote a to "117 pause_quanta" in the Support cell, change "N/A [] M: Yes []" to "Yes [] N/A []"
 Response Response Status C
 ACCEPT.

CI 045 SC 45.2.1.6 P50 L31 # i-1
 Marris, Arthur Cadence Design Syste
 Comment Type ER Comment Status A <bucket>
 The editorial instruction should be simplified to just show the changes to the relevant reserved bit descriptions in the new revision
 SuggestedRemedy
 Simplify Table 45-7 to just show changes to the relevant reserved fields for bits 1.7.6:0
 Response Response Status W
 ACCEPT.

CI 045 SC 45.2.1.116d P60 L35 # i-11
 Anslow, Peter Ciena Corporation
 Comment Type E Comment Status A <bucket>
 Tables that split across two pages need the bottom ruling on the first page set to "very thin" and the table continuation variable applied to the heading.
 SuggestedRemedy
 Make these two changes to tables 45-90ab, 45-90c, 45-90d, 45-90e
 Response Response Status C
 ACCEPT.

CI 045 SC 45.2.1.116d.2 P61 L49 # i-23
 Anslow, Peter Ciena Corporation
 Comment Type E Comment Status A <bucket>
 Generally, text in Clause 45 uses "one" or "zero" when describing the value a bit is set to rather than "1" or "0". However, there are some inconsistencies. There are 188 instances of "to one" and 27 instances of "to 1". There are 175 instances of "to zero" and 5 instances of "to 0". A comment has been submitted against the revision project D3.0 to change these instances of "1" and "0" to "one" and "zero"
 SuggestedRemedy
 Change "to 1" to "to one" on:
 Page 61, line 49
 Page 62, line 5
 Page 64, lines 18 and 26
 Response Response Status C
 ACCEPT.

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Cl **069** SC **69.2.3** P**85** L**49** # **i-7**
 Anslow, Peter Ciena Corporation

Comment Type **E** Comment Status **A** <bucket>

Comment r01-11 against D3.1 of P802.3cb has changed the table inserted by P802.3cb from Table 69-2a to Table 69-1aa. See: http://www.ieee802.org/3/cb/comments/IEEE_P802d3cb_D3p1_Cmt_Resolution_by_ID--20171106_1445.ldb.pdf#page=3
 This change has to be accounted for in the P802.3cb draft.

SuggestedRemedy

Change the base text (before changes) to: "Table 69-1, Table 69-1aa, Table 69-1a, and Table 69-2 specify the correlation..."
 Change the inserted tables to be Table69-2a, Table69-2b, and Table69-2c
 Change the editing instruction on page 86, line 10 to: "Insert Table69-2a, Table69-2b, and Table69-2c after Table69-2 as follows:

Response Response Status **C**

ACCEPT IN PRINCIPLE.

Align the changes with the 802.3-201x revision as modified by IEEE Std 802.3cb-201x.

Cl **073** SC **73.6.4** P**90** L**1** # **i-3**
 Marris, Arthur Cadence Design System

Comment Type **TR** Comment Status **A** <bucket>

Maintenance request 1283 has been implemented by the P802.3cj revision project to the base standard so there is no need for it in 802.3cd

SuggestedRemedy

Remove the text in 802.3cd concerning maintenance request 1283

Response Response Status **W**

ACCEPT.

Cl **073** SC **73.6.4** P**90** L**1** # **i-99**
 Healey, Adam Broadcom Ltd.

Comment Type **TR** Comment Status **A**

IEEE P802.3cd will end up being an amendment to IEEE Std 802.3-201x (currently IEEE P802.3 (IEEE 802.3cj) D3.0 which is in Sponsor ballot). The proposed changes and editing instructions should be aligned with the expected base document. This expected base document incorporates IEEE Std 802.3by-2016, has removed the paragraph shown in strikethrough starting at line 4, and already includes a note similar to the one starting at line 10.

SuggestedRemedy

Change the editing instruction to: "Change the fourth and fifth paragraphs (as modified by IEEE Std 802.3cb-201x) as follows:". Remove the strikethrough paragraph starting at line 4 and the note starting at line 10.

Response Response Status **C**

ACCEPT IN PRINCIPLE.

See also comment i-3.

It is only the last paragraph that has changed so also remove the fourth paragraph at line 12 in addition to removing the strikethrough paragraph starting at line 4 and the note starting at line 10.

Change the editing instruction to:

"Change the last paragraph of 73.6.4 (as modified by IEEE Std 802.3cb-201x) as follows:"

[Editor's note: The reference to comment i-3 is intended to point out another comment dealing with similar subject matter.]

Cl **073** SC **73.11.4.7** P**94** L**26** # **i-8**
 Anslow, Peter Ciena Corporation

Comment Type **E** Comment Status **A** <bucket>

The editing instruction could be improved

SuggestedRemedy

Change "Change Table" to "Change PICS item SD15"

Response Response Status **C**

ACCEPT.

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Cl 078 **SC 78.5** **P96** **L20** # **i-69**
Marris, Arthur Cadence Design Syste
Comment Type **E** **Comment Status** **A** <bucket>
The insertion should be below the row for 40GBASE-T
SuggestedRemedy
Change 40GBASE-KR to 40GBASE-T
Response **Response Status** **C**
ACCEPT.

Cl 080 **SC 80.1.3** **P97** **L47** # **i-70**
Marris, Arthur Cadence Design Syste
Comment Type **E** **Comment Status** **A** <bucket>
40GBASE-T is missing from the list
SuggestedRemedy
Add:
m) The MDI as specified in Clause 113 for 40GBASE-T uses a 4 lane data path.
Response **Response Status** **C**
ACCEPT IN PRINCIPLE.
To align with the 802.3-201x revision implement the suggested remedy.

Cl 080 **SC 80.5** **P105** **L16** # **i-126**
Dawe, Piers J G Mellanox Technologies
Comment Type **TR** **Comment Status** **A** skew variation <cc>
This table 80-7 (Skew Variation) does not agree with e.g. 138.3.2.1, which says "Since the signal at XX represents a serial bit stream, there is no Skew Variation at this point". All 50GBASE-R PMDs are serial.
SuggestedRemedy
Correct the table, at least for SP2-6, by using Table 131-6 (corrected) for 100G serial.
Response **Response Status** **C**
ACCEPT IN PRINCIPLE.

The only 100G interface that uses 53.125 GBd per lane is the 100GBASE-DR which has a single lane. There is therefore no skew variation from lane to lane.
In Table 80-7, remove the column for 53.125 GBd lanes and footnote d.
In 80.5...
The references in Table 80-6 to 140.4 are incorrect.
In Table 80-6, change 140.4 to 140.3 (four instances).
The references in Table 80-7 to 140.4 are not relevant.
In Table 80-7, delete references to 140.4.
[Editor's note: Comment i-124 deals with the same topic for 50GBASE-R.]

Cl 091 **SC 91.5.3.1** **P111** **L5** # **i-4**
Marris, Arthur Cadence Design Syste
Comment Type **TR** **Comment Status** **A** <bucket>
Maintenance request 1299 has been implemented by the P802.3cj revision project to the base standard so there is no need for it in 802.3cd
SuggestedRemedy
Remove the text and figure 91-8 in 802.3cd in Clauses 45 and 91 concerning maintenance request 1299.
Response **Response Status** **W**
ACCEPT.

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Cl 093A SC 93A.1.4.2 P332 L38 # i-166
 Dudek, Michael Cavium

Comment Type T Comment Status A <bucket>

The footnote below table 93A-1 implies that there is more information about what to do with C(-2) for clauses that don't have it in 93A.1.4.2. There isn't any and it should be added.

SuggestedRemedy

Add a paragraph. "Some clauses do not provide information about c(-2). For those clauses c(-2) is always zero.

Response Response Status C

ACCEPT IN PRINCIPLE.

The information for c(-2) when the clause doesn't provide it exists in 93A.1.6 (page 333) rather than 93A.1.4.2.

Change the cross-reference in the footnote of table 93A-1 from 93A.1.4.2 to 93A.1.6.

Cl 120 SC 120.5.7 P122 L11 # i-10
 Anslow, Peter Ciena Corporation

Comment Type E Comment Status A <bucket>

Heading 120.5.7 is being added with an Insert editing instruction, so it should not be underlined

SuggestedRemedy

Remove the underline from the heading 120.5.7

Response Response Status C

ACCEPT.

Cl 131 SC 131.1.2 P126 L15 # i-144
 Nicholl, Gary Cisco Systems, Inc.

Comment Type TR Comment Status A <bucket>

"uses a two-lane data path as specified in Annex 135F or Annex 135G." should be "uses a one-lane data path as specified in Annex 135F or Annex 135G"

SuggestedRemedy

Change "two-lane" to "one-lane"

Response Response Status W

ACCEPT.

Cl 131 SC 131.5 P134 L5 # i-6
 Anslow, Peter Ciena Corporation

Comment Type E Comment Status A <bucket>

In the heading row of Table 131-6, "Gbd" should be "GBd" (2 instances)

SuggestedRemedy

In the heading row of Table 131-6, change "Gbd" to "GBd" (2 instances)

Response Response Status C

ACCEPT.

Cl 131 SC 131.5 P134 L14 # i-124
 Dawe, Piers J G Mellanox Technologies

Comment Type TR Comment Status A skew variation <cc>

This table 131-6 (Skew Variation) does not agree with e.g. 138.3.2.1, which says "Since the signal at XX represents a serial bit stream, there is no Skew Variation at this point". All 50GBASE-R PMDs are serial.

SuggestedRemedy

Correct the table, at least for SP2-6.

Response Response Status C

ACCEPT IN PRINCIPLE.

50GAUI-1 and all 50G PMDs specified in this draft are serial interfaces so there is no skew variation.

The skew variation specifications in Table 131-6 are relevant only for LAUI-2 (25.78125 GBd NRZ) and 50GAUI-2 (26.5625 GBd NRZ) lanes.

In footnote "b", change "50GAUI-n or PMD" to "50GAUI-2".

In rows for SP2, SP3, SP4, and SP5 remove references to 136.6, 137.6, 138.3.2, and 139.3.

[Editor's note: Comment i-126 deals with the same topic for 100GBASE-R.]

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Cl 133 SC 133.1.2 P141 L17 # i-32
 RAN, ADEE Intel Corporation

Comment Type E Comment Status A <bucket>

"The 50GBASE-R PCS is identical to the 40GBASE-R PCS specified in Clause 82 with the following exceptions:"

The list of exceptions here is identical to the list of exceptions in "133.2.1 Functions within the PCS".

The repetition is unnecessary. Whenever I read this text I wonder if there is any difference.

Also, The PCS is not _identical_ with these exceptions; it also has slightly different delay constraints. The wording in 133.2.1 is more appropriate.

SuggestedRemedy

Replace the text from the second paragraph to the end of the subclause with the following:

The 50GBASE-R PCS specifications are based on the 40GBASE-R PCS specifications in Clause 82, with the modifications listed in 133.2 and 133.3.

Response Response Status C

ACCEPT.

Cl 133 SC 133.1.2 P141 L21 # i-145
 Nicholl, Gary Cisco Systems, Inc.

Comment Type E Comment Status R <withdrawn>

Add a reference at the end of the bullet 2 pointing to section 133.2.2.

SuggestedRemedy

Add a reference at the end of the bullet 2 pointing to section 133.2.2.

Response Response Status C

REJECT.

This comment was WITHDRAWN by the commenter.

Cl 133 SC 133.1.2 P141 L24 # i-146
 Nicholl, Gary Cisco Systems, Inc.

Comment Type E Comment Status R <withdrawn>

Add a reference at the end of the bullet 3 pointing to section 133.2.4.

SuggestedRemedy

Add a reference at the end of the bullet 3 pointing to section 133.2.4.

Response Response Status C

REJECT.

This comment was WITHDRAWN by the commenter.

Cl 133 SC 133.1.4 P141 L50 # i-16
 Anslow, Peter Ciena Corporation

Comment Type E Comment Status A <bucket>

Space missing between number and unit

SuggestedRemedy

Change 50Gb/s to 50 Gb/s using a non-breaking space (Ctrl space)

Response Response Status C

ACCEPT.

Cl 134 SC 134.1.1 P151 L13 # i-147
 Nicholl, Gary Cisco Systems, Inc.

Comment Type E Comment Status A <bucket>

In bullet (1) shouldn't we also mention that the nominal rate for the PCS lanes is different than the noimnal rate for 100G PCS lanes. We have a similar statement at the beginning of Clause 133.

SuggestedRemedy

Add some text to include the nominal rate of the PCS lanes, and note that the nominal rate is different from the 100G PCS lanes. Also add reference to 134.2.

Response Response Status C

ACCEPT.

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Cl 134 SC 134.1.1 P151 L15 # i-148
 Nicholl, Gary Cisco Systems, Inc.
 Comment Type E Comment Status A <bucket>
 Add a reference at the end of the bullet 3 pointing to section 134.5.2.7
 SuggestedRemedy
 Add a reference at the end of the bullet 3 pointing to section 134.5.2.7
 Response Response Status C
 ACCEPT.

Cl 134 SC 134.1.1 P151 L18 # i-149
 Nicholl, Gary Cisco Systems, Inc.
 Comment Type E Comment Status A <bucket>
 Add a reference at the end of the bullet 4 pointing to section 134.5.2.6.
 SuggestedRemedy
 Add a reference at the end of the bullet 4 pointing to section 134.5.2.6.
 Response Response Status C
 ACCEPT.

Cl 134 SC 134.1.1 P151 L22 # i-150
 Nicholl, Gary Cisco Systems, Inc.
 Comment Type E Comment Status A <bucket>
 Add a reference at the end of the bullet 5 pointing to section 134.5.4.
 SuggestedRemedy
 Add a reference at the end of the bullet 5 pointing to section 134.5.4.
 Response Response Status C
 ACCEPT.

Cl 134 SC 134.5.2.4 P153 L50 # i-33
 RAN, ADEE Intel Corporation
 Comment Type T Comment Status R
 "The incoming bit error ratio can be estimated by dividing the BIP block error ratio by a factor of 1 351 680"
 This sentence is misleading; within this subclause, it is not the _incoming bit error ratio_ that most readers would think it is, but rather the bit error ratio in the data stream from the local PCS to the RS-FEC input. This data path is not described, but in some applications it may create errors.

Unlike errors in the incoming data (from the link partner), any errors in this data stream are neither detected nor corrected. This is not obvious from reading the text.
 A similar comment against clause 91 was submitted to 802.3cj.
 SuggestedRemedy
 Change the quoted text to the following and add an informative note:
 The bit error ratio in the data received from the local PCS can be estimated by dividing the BIP block error ratio by a factor of 1 351 680.

NOTE--The data received from the local PCS is processed by the RS-FEC transmit function without error correction.
 Response Response Status C
 REJECT.
 The text is technically correct as written. The term "incoming" is clear in the context of the subclause (i.e., the transmit function of the RS-FEC sub-layer) and when looking at the functional block diagram in Figure 134-2.
 However, a similar comment is being addressed in the 802.3cj revision project. The 802.3cd task force would prefer to address this comment in the same way as 802.3cj.
 If the revision project adopts a change, the commenter is encouraged to resubmit.

IEEE P802.3cd 50 Gb/s, 100 Gb/s, 200 Gb/s Ethernet Initial Sponsor ballot comments

Cl 134 SC 134.5.2.6 P156 L20 # i-62
 Trowbridge, Stephen Nokia

Comment Type E Comment Status A <bucket>

Figure 134-3 has some sloppy drawing elements. The line above amp_tx_0 is either a different width than the line above amp_tx_2 or is two lines slightly offset. The line to the right of amp_tx_3(56:57) doesn't quite line up with the line between RS index 12 and 13 on the row above at every level of magnification on the PDF

SuggestedRemedy

Tidy up the figure. Zoom in close and nudge the items to line up. Use continuous lines where things are supposed to line up

Response Response Status C

ACCEPT.

Cl 134 SC 134.5.2.8 P156 L40 # i-42
 RAN, ADEE Intel Corporation

Comment Type E Comment Status A <bucket>

"in a round robin distribution from the lowest to the highest numbered FEC lane"

This can be simplified, since there are only two FEC lanes.

Also in 134.5.3.6 and in the corresponding PICS.

SuggestedRemedy

Change the quoted text to

"alternating between FEC lanes 0 and 1".

Update PICS items TF10 and RF11 accordingly.

Response Response Status C

ACCEPT IN PRINCIPLE.

Change the identified text in 134.5.2.8:

from: "one 10-bit symbol at a time in a round robin distribution from the lowest to the highest numbered FEC lane "

to: "one 10-bit symbol at a time alternating between FEC lanes 0 and 1"

Change the value/comment text for PICS TF10 in 134.7.4.1:

from: "Distributed to 2 FEC lanes, one 10-bit symbol at a time in a round robin distribution from the lowest to the highest numbered FEC lane"

to: "Distributed to 2 FEC lanes, one 10-bit symbol at a time alternating between FEC lanes 0 and 1"

Note, the same change is not applicable for 134.5.3.6 and the associated PICS RF11, as in this case the data is distributed to four PCS lanes and the text cannot be simplified as suggested by the commenter.

IEEE P802.3cd 50 Gb/s, 100 Gb/s, 200 Gb/s Ethernet Initial Sponsor ballot comments

Cl 134 SC 134.5.3.1 P157 L4 # i-63
 Trowbridge, Stephen Nokia
 Comment Type E Comment Status A <bucket>
 Several of the bit numbers in Figure 134-4 are touching the lines on the right side of the box:
 Four instances of "65" on line 4 and 256 on line 12.
 SuggestedRemedy
 Adjust the position of these numbers to be the same distance from the right edge of the box
 as the "0" is from the left edge of the corresponding box. The digits 0 and 9 should be
 centered in the C543, C542 boxes. Some similar adjustments (although fewer problems)
 should be made to Figure 134-5
 Response Response Status C
 ACCEPT.

Cl 134 SC 134.5.3.3 P158 L23 # i-34
 RAN, ADEE Intel Corporation
 Comment Type T Comment Status A
 "The probability that the decoder fails to indicate a codeword with t+1 errors as uncorrected
 is not expected to exceed 10⁻⁶"
 With RS(544,514) the probability is much lower; 802.3bs (119.2.5.3) states 10⁻¹⁶ for the
 same code.
 See the response to comment #74 in
http://www.ieee802.org/3/bs/comments/P802d3bs_D1p2_comments_final_ID.pdf.
 SuggestedRemedy
 Change "10⁻⁶" to "10⁻¹⁶".
 Response Response Status C
 ACCEPT.

Cl 134 SC 134.5.3.7 P160 L26 # i-43
 RAN, ADEE Intel Corporation
 Comment Type E Comment Status A <bucket>
 Missing period after "am_rxmapped".
 SuggestedRemedy
 Add a period.
 Response Response Status C
 ACCEPT.

Cl 134 SC 134.5.4 P160 L32 # i-35
 RAN, ADEE Intel Corporation
 Comment Type E Comment Status A <bucket>
 Superfluous period after "diagrams".
 SuggestedRemedy
 Remove it.
 Response Response Status C
 ACCEPT.

Cl 134 SC 134.5.4.2.3 P162 L52 # i-36
 RAN, ADEE Intel Corporation
 Comment Type E Comment Status A <bucket>
 Missing period after "FEC lane".
 SuggestedRemedy
 Add a period.
 Response Response Status C
 ACCEPT.

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Cl 134 SC 134.6 P164 L36 # i-39
 RAN, ADEE Intel Corporation

Comment Type E Comment Status R <withdrawn>

This clause has no state diagrams but it does define variables. The conventional text "The following subclauses define variables that are not otherwise defined, e.g., for use by state diagrams" creates a long list of 21 subclauses.

Unlike the common variable definition lists, these subclauses are not sorted by a meaningful order, and there is no separation to variables and counters.

It may be friendlier for readers to have the usual structure of variables and counters, sorted alphabetically.

SuggestedRemedy

Create a new subclause 134.7 titled "Variable definitions" (renumbering the PICS to 134.8).

Create two subclauses, 134.7.1 "Variables" and 134.7.2 "Counters".

Move the variable definitions in 136.6.1 through 136.6.21 to these subclauses, sorted alphabetically, with the usual variable-list format.

Response Response Status C

REJECT.

This comment was WITHDRAWN by the commenter.

Cl 134 SC 134.6.11 P165 L49 # i-40
 RAN, ADEE Intel Corporation

Comment Type E Comment Status A <bucket>

Superfluous period after "91.5.4.3".

SuggestedRemedy

Delete it.

Response Response Status C

ACCEPT IN PRINCIPLE.

Replace period with space.

Cl 134 SC 134.6.17 P166 L36 # i-38
 RAN, ADEE Intel Corporation

Comment Type E Comment Status A <bucket>

Missing period after "(see 134.5.2.2)".

SuggestedRemedy

Add a period.

Response Response Status C

ACCEPT.

Cl 134 SC 134.7.4.1 P170 L3 # i-41
 RAN, ADEE Intel Corporation

Comment Type T Comment Status A <bucket>

Item TF8 "feature" text "Alignment marker insertion point" is incorrect.

It resembles item TF7 "Alignment marker insertion", but the requirement it refers to in 134.5.2.6 is stated differently: the 257-bit block _following_ the AM corresponds to the PCS blocks 0, 1, 2 and 3 following the alignment marker. (P156 L4)

SuggestedRemedy

Change "feature" text from "Alignment marker insertion point" to "First 257-bit block inserted after am_txmapped".

Change "value/comment" by deleting the aforementioned words.

Response Response Status C

ACCEPT IN PRINCIPLE.

Change the "feature" text for PICS TF8 in 134.7.4.1:
 from: "Alignment marker insertion point"
 to: "First 257-bit block inserted after am_txmapped"

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Cl 135 SC 135 P176 L52 # i-45
 RAN, ADEE Intel Corporation

Comment Type E Comment Status A <bucket>

The identifiers p, q, i, j, and k are not consistently italicized throughout this clause.

There are also identifiers m, n, and z, denoting number of lanes, which are never italicized; so it's unclear whether p and q (which also denote the number of lanes) should be italicized.

Since p usually is italicized, I assume that all instances of p and q should be italicized. It may be decided otherwise. But for a specific identifier it should be consistent.

SuggestedRemedy

Search through clause 135 for isolated p/q/i/j/k and for UNITDATA_k and UNITDATA_i, and italicize the p/q/i/j/k identifiers.

Response Response Status C

ACCEPT.

Cl 135 SC 135.1 P172 L6 # i-128
 Dawe, Piers J G Mellanox Technologies

Comment Type E Comment Status R

Missing text: compare 136.1.

SuggestedRemedy

Mention all seven annexes briefly, in the style of 136.1.

e.g. Add some text in for the overview explaining what this clause is about - take text from 135.1.1 if appropriate:

"The Physical Medium Attachment sublayer (PMA) allows the PCS (see Clause 133 and Clause 82) and FEC (see Clause 134 and Clause 91) to connect in a media-independent way with a range of physical media. This clause has seven associated annexes ..."

Response Response Status C

REJECT.

Clause 136 specifies a PMD. It is common style to define the components of the PMD in the first subclause of a PMD clause.

Clause 135 specifies a pair of PMAs and no PMDs. Consistency with a PMD clause is not directly relevant.

The six Annexes relating to 50GAUI-n and 100GAUI-n are introduced in the third paragraph of 135.1.1.

Annex 135A, which gives examples of PHY layering when a 50GAUI-n or 100GAUI-n is used, is referenced in the first paragraph of 135.1.4.

This is consistent with the style of Clause 83 (40G/100G PMA) in 802.3-2015 and Clause 120 (200G/400G PMA) in 802.3bs-2018.

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Cl 135 SC 135.1.3 P172 L46 # i-129
 Dawe, Piers J G Mellanox Technologies

Comment Type E Comment Status A

We have added another function, precoding. This isn't the same as Gray mapping, which is part of PAM4 coding - a PMA with PAM4 input and output might do precoding but not PAM4 coding (because that's already done). Another PMA might do PAM4 coding but not precoding.

SuggestedRemedy

add item k, In some circumstances, perform precoding for PAM4.
 Add full stop to item j.

Response Response Status C

ACCEPT IN PRINCIPLE.

Precoding is part of the processing required for PAM4 modulated signals. It is never required for NRZ modulated signals.

Note that under the subclause 135.5.7 "PAM4 Encoding" includes subclauses 135.5.7.1 "Gray mapping for PAM4 encoded lanes" and 135.5.7.2 "Precoding for PAM4 encoded lanes".

However, for clarification, change item j to the following:
 "Perform PAM4 encoding and decoding, including Gray mapping and optional precoding, when required."

Cl 135 SC 135.1.4 P175 L18 # i-151
 Dudek, Michael Cavium

Comment Type E Comment Status A <bucket>

poor grammar.

SuggestedRemedy

add word "in" after specified

Response Response Status C

ACCEPT.

Cl 135 SC 135.3 P176 L44 # i-44
 RAN, ADEE Intel Corporation

Comment Type E Comment Status A <bucket>

Superfluous ")" after "indication".

SuggestedRemedy

Delete it.

Response Response Status C

ACCEPT.

Cl 135 SC 135.3 P177 L22 # i-64
 Trowbridge, Stephen Nokia

Comment Type TR Comment Status A <bucket>

It is not correct that the PMA passes symbols from the input lanes to the output lanes unless the symbols are bits. According to Figure 135-5, PAM4 symbols are decoded (converted to pairs of bits), passed through a bit mux, and encoded to PAM4 symbols at the output.

SuggestedRemedy

Change "the PMA passes symbols from the input lanes to the output lanes" to "the PMA passes the bits represented by the symbols from the input lanes into encoded symbols on the output lanes". Same issue Page 178 line 5 in the reverse direction.

Response Response Status W

ACCEPT.

IEEE P802.3cd 50 Gb/s, 100 Gb/s, 200 Gb/s Ethernet Initial Sponsor ballot comments

CI 135 SC 135.5.7.2 P184 L12 # i-130
 Dawe, Piers J G Mellanox Technologies

Comment Type T Comment Status A

Because a lane can run through PMAs or PMDs, this text is ambiguous: does an indirect connection count? In the first paragraph we have "PMA lanes connected to" and in the last two paragraphs we have "PMA lanes adjacent to".
 Also, per 120D.1, "The... C2C link is described in terms of a ... C2C transmitter, a ... C2C channel, and a ... C2C receiver." So a PMA lane connected to a C2C link (not part of the link) might be further up or down the chain.

The remedy is a corrected version of the November proposal; further improvements may be appropriate.

SuggestedRemedy

Change "For PMA lanes connected to a 50GAUI-1 C2C or 100GAUI-2 C2C link, or to the PMD service interface of a 50GBASE-CR, 50GBASE-KR, 100GBASE-CR2, or 100GBASE-KR2 PMD, the PMA shall provide 1/(1+D) mod 4 precoding capability on each output lane and may optionally provide 1/(1+D) mod 4 decoding capability on each input lane."

to "A PMA shall provide 1/(1+D) mod 4 precoding capability on each output lane that is part of a 50GAUI-1 C2C or 100GAUI-2 C2C transmitter, or is adjacent to the PMD service interface of a 50GBASE-CR, 50GBASE-KR, 100GBASE-CR2, or 100GBASE-KR2 PMD. A PMA may optionally provide 1/(1+D) mod 4 decoding capability on each input lane that is part of a 50GAUI-1 C2C or 100GAUI-2 C2C receiver, or is adjacent to the PMD service interface of a 50GBASE-CR, 50GBASE-KR, 100GBASE-CR2, or 100GBASE-KR2 PMD." In the penultimate paragraph, change "For PMA lanes adjacent to a 50GBASE-CR PMD" to "For PMA inputs and outputs adjacent to a 50GBASE-CR PMD".

In the last paragraph, change "For PMA lanes adjacent to a 50GAUI-1 C2C" to "For PMA inputs and outputs that are part of a 50GAUI-1 C2C".

Response Response Status C

ACCEPT IN PRINCIPLE.

Some clean-up of the wording would be helpful to the reader. However, the language should be kept consistent throughout the subclause.

Change: "For PMA lanes connected to a 50GAUI-1 C2C or 100GAUI-2 C2C link, or to the PMD service interface of a 50GBASE-CR, 50GBASE-KR, 100GBASE-CR2, or 100GBASE-KR2 PMD, the PMA shall provide 1/(1+D) mod 4 precoding capability on each output lane and may optionally provide 1/(1+D) mod 4 decoding capability on each input lane."

To: "A PMA shall provide 1/(1+D) mod 4 precoding capability on each output lane that is part of a 50GAUI-1 C2C or 100GAUI-2 C2C link, or connected to the PMD service interface of a 50GBASE-CR, 50GBASE-KR, 100GBASE-CR2, or 100GBASE-KR2 PMD. A PMA may optionally provide 1/(1+D) mod 4 decoding capability on each input lane that is part of a 50GAUI-1 C2C or 100GAUI-2 C2C link, or connected to the PMD service interface of a 50GBASE-CR, 50GBASE-KR, 100GBASE-CR2, or 100GBASE-KR2 PMD."

In the penultimate paragraph...

Change: "For PMA lanes adjacent to a 50GBASE-CR PMD"

To: "For PMA input and output lanes connected to the PMD service interface of a 50GBASE-

CR PMD".

In the last paragraph...

Change "For PMA lanes adjacent to a 50GAUI-1 C2C or a 100GAUI-2 C2C"

To: "For PMA input and output lanes that are part of a 50GAUI-1 C2C or 100GAUI-2 C2C link".

CI 135 SC 135.5.10 P186 L17 # i-152
 Dudek, Michael Cavium

Comment Type E Comment Status A <bucket>

poor grammar.

SuggestedRemedy

add word "it" after not

Response Response Status C

ACCEPT.

CI 135 SC 135.5.10.1 P186 L24 # i-153
 Dudek, Michael Cavium

Comment Type E Comment Status A <bucket>

The intent here is to differentiate between NRZ test patterns and PAM4 test patterns (if it isn't this sentence has little value). Using "clause" here includes both.

SuggestedRemedy

Change "clause" to "sub-clause". Also on line 46

Response Response Status C

ACCEPT IN PRINCIPLE.

On page 185 lines 24 and 46 change "clause" to "subclause".

CI 135 SC 135.5.10.2.2 P187 L7 # i-154
 Dudek, Michael Cavium

Comment Type T Comment Status A

A PRBS31Q checker is also optionally needed, (and is already included in the PICs).

SuggestedRemedy

Change the sentence and add an extra paragraph to be equivalent to the NRZ section.

Change to "A PMA may optionally include a PRBS31Q test-pattern generator on output lanes in either direction as specified in 120.5.11.2.2. Add a sentence. "A PMA may optionally include a PRBS31Q test-pattern checker on input lanes in either direction as specified in 120.5.11.2.2."

Response Response Status C

ACCEPT.

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Cl 135 SC 135.7.4.2 P193 L19 # i-46
 RAN, ADEE Intel Corporation
 Comment Type T Comment Status A <bucket>
 I can't find the definitions of conditional features "PIU", "PID", and "PIP" which appear in the status column..
 SuggestedRemedy
 Add the definitions for these features, or change the conditions of items using them to something else.
 Response Response Status C
 ACCEPT.

Cl 135 SC 135.7.4.3 P194 L19 # i-47
 RAN, ADEE Intel Corporation
 Comment Type E Comment Status A <bucket>
 It doesn't make sense that all items in this table have status "M". They should be conditional on data rate and number of lanes.
 In addition, item E8 requires 53.125 GBd for a one-lane interface; does this rule out a one-lane 50GBASE-*R PMD?
 SuggestedRemedy
 Add necessary conditions for each case.
 Response Response Status C
 ACCEPT.

Cl 135 SC 135.7.4.3 P194 L20 # i-155
 Dudek, Michael Cavium
 Comment Type E Comment Status A <bucket>
 Subclause references are missing
 SuggestedRemedy
 Add them
 Response Response Status C
 ACCEPT.

Cl 135B SC 135B.5.4.2 P345 L12 # i-167
 Dudek, Michael Cavium
 Comment Type T Comment Status A <bucket>
 There are no exceptions to Table 83D-5 in 135B.3.2
 SuggestedRemedy
 Delete "with the exceptions in 135B.3.2"
 Response Response Status C
 ACCEPT.

Cl 135C SC 135C.1 P347 L22 # i-168
 Dudek, Michael Cavium
 Comment Type E Comment Status A <bucket>
 poor English
 SuggestedRemedy
 Change "using" to "uses"
 Response Response Status C
 ACCEPT.

Cl 135D SC 135D.5.4.2 P357 L12 # i-169
 Dudek, Michael Cavium
 Comment Type E Comment Status A
 The exceptions are listed in 120B.3.2 and 135D.3.2 only contains a reference to 120B.3.2
 SuggestedRemedy
 Change to "with the exceptions in 120B.3.2" but keep the subclause reference as 135D.3.2
 Response Response Status C
 ACCEPT.

IEEE P802.3cd 50 Gb/s, 100 Gb/s, 200 Gb/s Ethernet Initial Sponsor ballot comments

Cl 135F SC 135F.1 P367 L7 # i-142
 Dawe, Piers J G Mellanox Technologies

Comment Type T Comment Status A precoding

This annex does not refer to Clause 135 at all, nor does it mention precoding for the data path.

SuggestedRemedy

Make reference to 135.

Here, add sentence saying that a receiver may request precoding and a transmitter should? shall? follow the request.

In 135F.3.1, say that in addition the C2C transmitter provides a precoding function that can be switched on and off.

In 135F.3.2, say that in addition the C2C receiver may provide an inverse precoding function.

Response Response Status C

ACCEPT IN PRINCIPLE.

In 135F.1 expand the first sentence of the second paragraphs as follows:

"50GAUI-1 C2C and 100GAUI-2 C2C are physical instantiations of the PMA service interface between the FEC and the PMD, as described in 135.1.4."

Make similar changes in 135B.1, 135C.1, 135D.1, 135E.1, and 135G.1.

Add a new paragraph at the end of 135F.1 as follows:

"The 50GAUI-1 C2C or 100GAUI-2 C2C transmitter and receiver processing may include precoding as specified in 135F.3.1 and 135F.3.2, respectively. Precoding may be enabled and disabled using the precoder request mechanism specified in 135F.3.2.1."

Add a new paragraph in 135F.3.1 as follows:

"In addition, the 50GAUI-1 C2C or 100GAUI-2 C2C transmitter shall support $1/(1+D) \bmod 4$ precoding as specified in 135.5.7.2 that may be enabled or disabled as required."

Replace the content of 135F.3.2 with the following:

"The 50GAUI-1 C2C or 100GAUI-2 C2C receiver may optionally support $1/(1+D) \bmod 4$ decoding as specified in 135.5.7.2 that may be enabled or disabled as required. A 50GAUI-1 C2C or a 100GAUI-2 C2C receiver shall meet all specifications in 120D.3.2, with precoding enabled on the test transmitter if required by the receiver."

Cl 135F SC 135F.3 P367 L18 # i-98
 Rysin, Alexander Mellanox Technologies

Comment Type TR Comment Status R ERL

Transmitter output residual ISI SNR_ISI (min) 34.8 dB (Clause 120D) is too high - can barely measure the IC through the test fixture. The warning NOTE in 120D.3.1.7 shows the issue, but doesn't solve it. D2.0 comment 140, D2.1 comment 49, D2.2 comment 22.

Since both SNR_ISI and Effective Return Loss (ERL) represent uncompensated reflections from the transmitter and the test fixtures, measurements of ERL can replace SNR_ISI.

Also, frequency domain return loss mask does not truly represent digital signaling at a given bit error ratio. There is no real proof that violating return loss masks is directly tied to failures and a number of false negatives have been shown. D2.0 comment 141, D2.1 comments 26, 27 and 28.

SuggestedRemedy

Change 135F.3.1 from "A 50GAUI-1 C2C or a 100GAUI-2 C2C transmitter shall meet all specifications in 120D.3.1" to

"A 50GAUI-1 C2C or a 100GAUI-2 C2C transmitter shall meet all specifications in 120D.3.1 with the following exceptions:

Effective Return Loss (ERL) is calculated with Nb set to 10 (see Annex New). ERL shall be at least 16.2 dB. The Transmitter Output residual ISI SNR_ISI and the return loss specifications in Table in Table 120D-1 do not apply."

Change 135F.3.2 from "A 50GAUI-1 C2C or a 100GAUI-2 C2C receiver shall meet all specifications in 120D.3.1" to

"A 50GAUI-1 C2C or a 100GAUI-2 C2C transmitter shall meet all specifications in 120D.3.2 with the following exceptions:

Effective Return Loss (ERL) is calculated with Nb set to 10 (see Annex New). ERL shall be at least 16.2 dB. There is no frequency domain return loss mask."

Response Response Status U

REJECT.

Although ERL was adopted for clauses 137 and 136, it is not clear whether it should be adopted for Annex 135F, since its electrical characteristics were intended to be essentially identical to 120D.

There is no consensus to implement the suggested remedy.

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CI 135F SC 135F.3.2 P367 L25 # i-170
 Dudek, Michael Cavium

Comment Type T Comment Status A

The Receiver should be allowed to use the Transmitter precoding to meet the FEC symbol error ratio requirements.

SuggestedRemedy

Add the following "with the optional use of Transmitter pre-coding to achieve the required FEC symbol error ratio."

Response Response Status C

ACCEPT IN PRINCIPLE.

Resolve with the response to i-142.

[Editor's note: For reference, the response to comment i-142 is copied here:

ACCEPT IN PRINCIPLE.

In 135F.1 expand the first sentence of the second paragraphs as follows:
 "50GAUI-1 C2C and 100GAUI-2 C2C are physical instantiations of the PMA service interface between the FEC and the PMD, as described in 135.1.4."

Make similar changes in 135B.1, 135C.1, 135D.1, 135E.1, and 135G.1.

Add a new paragraph at the end of 135F.1 as follows:
 "The 50GAUI-1 C2C or 100GAUI-2 C2C transmitter and receiver processing may include precoding as specified in 135F.3.1 and 135F.3.2, respectively. Precoding may be enabled and disabled using the precoder request mechanism specified in 135F.3.2.1."

Add a new paragraph in 135F.3.1 as follows:
 "In addition, the 50GAUI-1 C2C or 100GAUI-2 C2C transmitter shall support $1/(1+D) \bmod 4$ precoding as specified in 135.5.7.2 that may be enabled or disabled as required."

Replace the content of 135F.3.2 with the following:
 "The 50GAUI-1 C2C or 100GAUI-2 C2C receiver may optionally support $1/(1+D) \bmod 4$ decoding as specified in 135.5.7.2 that may be enabled or disabled as required. A 50GAUI-1 C2C or a 100GAUI-2 C2C receiver shall meet all specifications in 120D.3.2, with precoding enabled on the test transmitter if required by the receiver."

]

CI 135F SC 135F.6.4.1 P371 L38 # i-171
 Dudek, Michael Cavium

Comment Type T Comment Status A <bucket>

The 12mV is incorrect. It is 30mV in the specifications in 120D.3.1 and was corrected in the 802.3bs PICs from 12mV to 30mV in the last revision

SuggestedRemedy

Change 12mV to 30mV.

Response Response Status C

ACCEPT.

CI 135F SC 135F.6.4.3 P372 L36 # i-172
 Dudek, Michael Cavium

Comment Type T Comment Status A <bucket>

The Pics for the Channel Return loss is missing

SuggestedRemedy

Add the equivalent Pics to CC2 in 120D.5.4.3

Response Response Status C

ACCEPT.

IEEE P802.3cd 50 Gb/s, 100 Gb/s, 200 Gb/s Ethernet Initial Sponsor ballot comments

Cl **135G** SC **135G.3.1** P**375** L**21** # **i-115**
 Dawe, Piers J G Mellanox Technologies

Comment Type **TR** Comment Status **R** jitter mismatch <cc>

As pointed out in both 802.3bs and this project, a host output with 50 Gb/s lanes is allowed to make twice as much low frequency jitter at very low frequencies as a receiver with 100 Gb/s lane(s) is required to receive. A jitter buffer does not fix this unless it is infinite. To assure interoperability, there must be industry-wide agreement that tightens 50G/lane host low frequency jitter generation, increases 100G/lane receiver low frequency jitter tolerance, or a combination. The proposed remedy is as simple as any of the options considered. Also it is likely to be compatible with 100G electrical lanes. This remedy must be applied to 100GAUI-2 C2M host outputs (unless another remedy is chosen), but may be applied to 50GAUI-1 host outputs and/or the corresponding module inputs for consistency. As any 50G/lane E/O conversions basically pass the low frequency jitter along for something else to tolerate, we can leave their specs alone.

SuggestedRemedy

Add to the end of the sentence "with the exception that the clock recovery unit's corner frequency (see 120E.4.2) is 2 MHz not 4 MHz".

If desired, change 135G.3.4: add "with the exceptions that the sinusoidal jitter (see 120E.3.4.1.1 and Table 120E-8) is defined by Table 135G-New, and that the reference CRU's corner frequency (see 120E.3.4.1.1of 4 MHz) is 2 MHz not 4 MHz".

Table 135G-New--Applied sinusoidal jitter

Parameter	Case A	Case B	Case C	Case D	Case E	Case F	Units
Jitter frequency	0.02	0.667	2	6	20	60	MHz
Jitter amplitude	5	0.15	0.05	0.05	0.05	0.05	UI

Response Response Status **W**

REJECT.

Resolve using the response to comment i-61.

[Editor's note: For reference, the response to comment i-61 is copied here:

REJECT.

Reviewed http://www.ieee802.org/3/cd/public/Jan18/ghiasi_3cd_01_0118.pdf.

Straw poll #1 indicated lack of consensus to make any technical changes to the jitter specification.

Straw poll #1:

I would support making a technical change to the jitter specification.

Y: 4

N: 21

There is no support to make any changes to the jitter specifications.

]

Cl **135G** SC **135G.3.1** P**375** L**21** # **i-61**
 RAN, ADEE Intel Corporation

Comment Type **TR** Comment Status **R** jitter mismatch <cc>

100GAUI-2 C2M host output is specified by reference to 120E.3.1. This means jitter is measured with a CRU with corner frequency of 4 MHz (per 120E.4.2).

Low-frequency jitter will be attenuated by the CRU - that means it is assumed to be tracked by the module's CDR.

This creates a problem if the module is a 100GBASE-DR PMD; the tracked jitter will be forwarded to the optical transmitter with the same time values, so doubled magnitude in UI terms.

This means that the link partner's optical receiver, with assumed CDR BW of 4 MHz too (per 140.7.9 and 121.8.9.4 SRS definitions), will see low frequency jitter that can be twice of what it is tested to tolerate.

The CDRs used in practice are second-order, so at very low frequencies this higher jitter level will likely be acceptable; but there is no specification for the integral gain of the CDR, so at medium frequencies the jitter tolerance is implementation dependent (even for fully compliant PMDs).

Having excessive untracked low-frequency jitter may be detrimental for BER even with FEC; the SNR will vary over time, and even if the average is good, uncorrectable codewords may be more frequent than what could be expected. This can cause unexpected deployment problems.

This issue was not resolved in 802.3bs although there have been comments about having the same CDR bandwidth for 50 and 100 Gb/s per lane interfaces. The least painful way to solve it at this point seems to be a recommendation for the host output jitter. This will leave all optical specs unmodified.

SuggestedRemedy

Add the following text after the single paragraph in 135G.3.1:

To limit the jitter at frequencies which a 100GBASE-DR PMD's optical receiver may not track well, it is recommended that in addition to the specifications in 120E.3.1, the Host output eye width and eye height specifications (120E.3.1.6) be met when measured using a clock recovery unit with a corner frequency of 2 MHz.

Response Response Status **U**

REJECT.

Reviewed http://www.ieee802.org/3/cd/public/Jan18/ghiasi_3cd_01_0118.pdf.

Straw poll #1 indicated lack of consensus to make any technical changes to the jitter specification.

Straw poll #1:

IEEE P802.3cd 50 Gb/s, 100 Gb/s, 200 Gb/s Ethernet Initial Sponsor ballot comments

I would support making a technical change to the jitter specification.
Y: 4
N: 21

There is no support to make any changes to the jitter specifications.

Cl **135G** SC **135G.3.1** P**375** L**22** # **i-114**
Dawe, Piers J G Mellanox Technologies

Comment Type **TR** Comment Status **A**

As shown in
http://iee802.org/3/bs/public/adhoc/elect/05Oct_17/dawe_01b_100517_elect.pdf and
http://www.ieee802.org/3/cd/public/Nov17/dawe_3cd_01_1117.pdf there is a need for an additional spec to protect the module from e.g. very noisy hosts, and a max VEC spec provides worthwhile protection.
This was agreed in principle (D2.2 comment 30) but not implemented at that time. Now is the time.

SuggestedRemedy

Here, add a requirement for VEC, max 12 dB. In a new 135G3.1.1 or 135G.4.1, add definition of VEC, based on the definition in P802.3bs D2.0 120E.4.2.1: see daw_3cd_01_1117 slide 13 (or successor) for proposed text. Add new PICS for 135G.5.1.

Response Response Status **C**

ACCEPT IN PRINCIPLE.

A presentation and proposal on this subject was considered at the previous task force meeting. The response included the following:
"Viewed daw_3cd_01_1117. There was general agreement with the proposal.
A presentation providing detailed implementation is encouraged.
The commenter is encouraged to resubmit this comment at Sponsor ballot."

Create new subclause 135G.4.1 specifying methodology for VEC measurement using the definition on slide 13 of http://www.ieee802.org/3/cd/public/Jan18/dawe_3cd_01_0118.pdf.

Change the text 135G.3.1 to the following:
"A 50GAUI-1 C2M or 100GAUI-2 C2M host output shall meet all specifications in 120E.3.1 and VEC as specified in 135G.4.1 shall be less than 12 dB."

Add the following the end of the sentence in 135G.3.4:
"with the exception that for the module stressed input test in 120E.3.1 the input VEC as specified in 135G.4.1 is less than 12 dB".

Implement all with editorial license.

Cl **135G** SC **135G.3.1** P**375** L**33** # **i-87**
Wertheim, Oded Mellanox Technologies

Comment Type **TR** Comment Status **R** jitter mismatch <cc>

The jitter specification for the 100G per lane 100GBASE-DR1 receiver uses the same frequency corner as the 50G per lane 100GAUI-2 with the same jitter but with half the peak-to-peak jitter as the jitter mask is defined in Uls. This requires the 100GBASE-DR transceiver PMA to implement a de-jitterizer, which requires to add a PLL to handle the low frequency jitter and a large jitter buffer (which may be unbounded when attempting to reduce also the very low frequencies jitter). This adds unnecessary complexity, cost and power to the transceiver.

SuggestedRemedy

Scale the corner frequency for 100GAUI-2 to 2MHz (half the corner frequency of 100GBASE-DR). The proposed resolution doesn't introduce constraints on future 100G per lane interfaces and provides simpler solution than alternative solutions that were investigated, with no change to the optical specs.

1. Add an exception to 135G.4 50GAUI-1 C2M and 100GAUI-2 C2M measurement methodology with an exception that:
a. The reference CRU for the Eye width and eye height measurement method has a corner frequency of 2MHz for the host output and module input tests.

2. Add an exception to 135G.3.4 50GAUI-1 C2M and 100GAUI-2 C2M module input characteristics:
With an exception that:
a. The reference CRU for the Module stressed input test has a corner frequency of 2MHz
b. The applied sinusoidal jitter values for 100GAUI-2 Module stressed input test shall be: {Jitter frequency, Jitter amplitude}
Case A: {0.02, 5}
Case B: {0.66, 0.15}
Case C: {2, 0.05}
Case D: {6, 0.05}
Case E: {20, 0.05}

Response Response Status **W**

REJECT.

Resolve using the response to comment i-61.

[Editor's note: For reference, the response to comment i-61 is copied here:

REJECT.

Reviewed http://www.ieee802.org/3/cd/public/Jan18/ghiasi_3cd_01_0118.pdf.

Straw poll #1 indicated lack of consensus to make any technical changes to the jitter specification.

Straw poll #1:

IEEE P802.3cd 50 Gb/s, 100 Gb/s, 200 Gb/s Ethernet Initial Sponsor ballot comments

I would support making a technical change to the jitter specification.
 Y: 4
 N: 21

There is no support to make any changes to the jitter specifications.
]

Cl 136 SC 136 P207 L20 # i-158
 Dudek, Michael Cavium

Comment Type T Comment Status A <bucket>
 There are two cable assembly test fixtures in the cable assembly specifications.

SuggestedRemedy
 Change "the cable assembly test fixture" to "two cable assembly test fixtures"

Response Response Status C
 ACCEPT IN PRINCIPLE.

The comment correctly points out that two test fixtures are included in the specifications.
 However, the test fixtures and the cable assembly include the mated connectors; there is no need to list the mated connector pairs separately.
 Change from "Two mated connector pairs and the cable assembly test fixture"
 To "Two cable assembly test fixtures".

Cl 136 SC 136.1 P198 L10 # i-156
 Dudek, Michael Cavium

Comment Type E Comment Status R <cc>
 In the stack Clause 91 FEC will always be below the Clause 83 annexes. It would read better if Table 136-2 were in the same order.

SuggestedRemedy
 In table 136-2 Move the row for clause 91 immediately below the row for Annex 83D. Make the same change in Table 137-2.

Response Response Status C
 REJECT.

The ordering of Clauses in this table is not intended to define the sublayer stack order.
 There is consensus to leave the tables as they are currently written.
 Straw poll:
 Do you support making the proposed changes to the table?
 Y: 3
 N: 20

Cl 136 SC 136.3 P200 L45 # i-157
 Dudek, Michael Cavium

Comment Type E Comment Status R <bucket>
 With just two possible values of I the use of "or" instead of "to" is better.

SuggestedRemedy
 Change "to" to "or"

Response Response Status C
 REJECT.

This is consistent with other definitions with multiple lanes, e.g, 0 to 3. Also, it is not incorrect as written.

Cl 136 SC 136.3 P234 L30 # i-77
 Mellitz, Richard Samtec, Inc.

Comment Type TR Comment Status A ERL
 Return loss has not been demonstrated to limit sufficiently limit COM variability. There is no clear relation between the DFE in the reference signaling architecture and portions of reflections which are re-reflected. Apparently, there is no clear tie-in between the host input/output return loss and cable assembly return loss. ERL addresses these reflections directly and provided a linkage to input/output return loss.

SuggestedRemedy
 Rename clause 136.11.3 from "Cable Assembly Differential Return Loss" to ""Cable Assembly Effective Return Loss". Remove all the content of 136.11.3. Replace with: "The minimum effective return loss of the cable assembly shall be greater than 11.2 dB only when COM is less than 4 dB computed using beta_x=10.7e9, rho_x=0.15, PTDR Tr=18.9ps, and N_b is set by this clause."

Response Response Status C
 ACCEPT IN PRINCIPLE.

Implement the changes according to
http://www.ieee802.org/3/cd/public/Jan18/ran_3cd_01_0118.pdf.

IEEE P802.3cd 50 Gb/s, 100 Gb/s, 200 Gb/s Ethernet Initial Sponsor ballot comments

Cl 136 SC 136.6.1 P202 L19 # i-123
 Dawe, Piers J G Mellanox Technologies

Comment Type TR Comment Status R skew <cc>

The Skew at SP4 (the receiver MDI) has to be the same as the Skew at SP3 (the transmitter MDI) for these serial PMDs.

SuggestedRemedy

Correct the numbers at SP4 and SP5. Correct Table 131-5, Summary of Skew constraints - all 50GBASE-R PMDs are serial so it's simple to do. Also 137.6.1 138.3.2.1 139.3.2.

Response Response Status U

REJECT.

The skew constraints for 100G in Table 80-5 and for 50G in Table 131-5 are consistent with the budget and methodology adopted by 802.3ba and 802.3bg and used in subsequent projects (e.g., 802.3bm, 802.3bs).

The skew constraints are established to ensure that the FEC/PCS skew tolerance is sufficient to support the worst case skew for any currently specified or potential (within reason) future PHY (e.g., 2-lane PMD for reach longer than 40 km). This is accomplished by having the same skew constraint at SP5 regardless of the PMD type.

The skew constraint at SP5 includes allocation for skew accumulated through the TX PMD (SP2 to SP3), the medium (SP3 to SP4), and the RX PMD (SP4 to SP5). Rather than specifying unique values for SP3, SP4, and SP5 based on PMD type, the adopted approach was to use the same numbers for all PMD types for consistency.

The approach described above is consistent for all PHY types defined by 802.3ba and subsequent projects. For instance, the medium skew accumulation (SP3 to SP4) of 80 ns was based on an 80 km multi-lane optical PMD. Nevertheless, the same value is used for other PMDs where the skew would be considerably lower (e.g., 100GBASE-SR4, 100GBASE-KR4, 100GBASE-CR4, etc.).

This specification methodology does not preclude an engineered implementation that optimizes the FEC/PCS skew buffering based on assumed lower PMD and medium skew accumulation. However, it should be noted that this implementation would not be compliant to 802.3cd.

Cl 136 SC 136.8.1 P207 L15 # i-24
 Lusted, Kent Intel Corporation

Comment Type ER Comment Status A <bucket>

Incorrect cross reference. this should reference 136.10 (Channel characteristics), not 136.9 (PMD electrical characteristics)

SuggestedRemedy

Change reference to 136.10

Response Response Status W

ACCEPT.

IEEE P802.3cd 50 Gb/s, 100 Gb/s, 200 Gb/s Ethernet Initial Sponsor ballot comments

CI 136 SC 136.8.2 P208 L1 # i-25
Lusted, Kent Intel Corporation

Comment Type TR Comment Status A PAM4 levels <cc>

there is no explicit mapping of the differential output voltage to tx_symbol = two and tx_symbol = one.

SuggestedRemedy

Add the explicit mapping of the differential output voltage to tx_symbol = two and tx_symbol = one.

Response Response Status C

ACCEPT IN PRINCIPLE.

In the second paragraph, change FROM

"The highest differential output voltage (SLi<p> minus SLi<n>) shall correspond to tx_symbol = three and the lowest differential output voltage shall correspond to tx_symbol = zero"

TO

"The differential output voltage (SLi<p> minus SLi<n>) meets the specifications in 136.9.3.1.1 where the PAM4 symbol values 0, 1, 2, and 3 correspond to the tx_symbol values zero, one, two, and three, respectively, with the highest differential output voltage corresponding to tx_symbol = three and the lowest differential output voltage corresponding to tx_symbol = zero".

In the third paragraph, change FROM

"The highest differential output voltage (SLi<p> minus SLi<n>) shall correspond to the symbol 3 and the lowest differential output voltage shall correspond to the symbol 0"

TO

"The differential output voltage (SLi<p> minus SLi<n>) meets the specifications in 136.9.3.1.1, with the highest differential output voltage corresponding to the PAM4 symbol 3 and the lowest differential output voltage corresponding to the PAM4 symbol 0".

A similar clarification should be provided for the optical PMDs.

In 138.5.2, 139.5.2, and 140.5.2 ...

change: "The highest optical power level in the signal stream shall correspond to tx_symbol = three and the lowest shall correspond to tx_symbol = zero."

to: "The four optical power levels in the signal stream in order from lowest to highest shall correspond to tx_symbols zero, one, two, and three, respectively."

In 138.5.3, 139.5.3, and 140.5.3 ...

change: "The highest optical power level in each signal shall correspond to rx_symbol = three and the lowest shall correspond to rx_symbol = zero."

to: "The four optical power levels in each signal in order from lowest to highest shall correspond to rx_symbols zero, one, two, and three, respectively."

Update PICS as required.

CI 136 SC 136.8.2 P208 L6 # i-26
Lusted, Kent Intel Corporation

Comment Type ER Comment Status R <bucket>

The second paragraph in 136.8.2 reference the tx_symbol values as "three" and "zero". The first paragraph in 136.8.3 reference the rx_symbol values as "three" and "zero".

however, the 3rd paragraph of 136.8.2 does not use "three" and "zero" but "3" and "0".

SuggestedRemedy

In the 3rd paragraph of 136.8.2, change to "three" and "zero"

Response Response Status W

REJECT.

The 3rd paragraph uses "3" and "0" because in TRAINING mode the input to the PMD transmit function comes from the PMD control function, which is specified using the numbers 0 to 3 (the numbers are mapped to tx_symbol values, see 136.8.11.1).

CI 136 SC 136.8.11.1 P210 L4 # i-27
Lusted, Kent Intel Corporation

Comment Type TR Comment Status A <bucket>

the term "the symbol values..." in the parenthesis is a bit confusing. The first sentence of the paragraph references PAM4 symbols as well as tx_symbol and rx_symbol.

SuggestedRemedy

change "the symbol values" to "the PAM4 symbol values"

Response Response Status W

ACCEPT.

IEEE P802.3cd 50 Gb/s, 100 Gb/s, 200 Gb/s Ethernet Initial Sponsor ballot comments

Cl 136 SC 136.8.11.4.1 P215 L47 # i-89
 Slavick, Jeff Broadcom Limited

Comment Type E Comment Status A <bucket>

This sub-section has 2 chunks of information, the first part describes how to Request an Initial Condition and the second part how to respond to a Request. It would be cleaner if these were split into two sections.

SuggestedRemedy

Change title of 136.8.4.11.1 to be "Initial condition setting request process"
 Insert new sub-heading 136.8.4.11.2 titled "Initial condition setting response process" before the paragraph starting with "The handling of"
 Update 136.8.11.7.2 UPDATE_IC reference to the new sub-section

Response Response Status C

ACCEPT IN PRINCIPLE.

This response is the same as the suggested remedy, except with subclause number corrected.

Change title of 136.8.11.4.1 to be "Initial condition setting request process".

Insert new subclause heading 136.8.11.4.2 titled "Initial condition setting response process" before the paragraph starting with "The handling of".

Update 136.8.11.7.2 UPDATE_IC reference to the new subclause 136.8.11.4.2.

Cl 136 SC 136.8.11.4.2 P216 L28 # i-90
 Slavick, Jeff Broadcom Limited

Comment Type E Comment Status A <bucket>

This sub-section has 2 chunks of information, the first part describes how to Request a Coefficient update and the second part how to respond to a Request. It would be cleaner if these were split into two sections.

SuggestedRemedy

Change title of 136.8.4.11.2 to be "136.8.4.2.11.3 Coefficient update request process"
 Insert new sub-heading 136.8.4.11.4 titled "Coefficient update response process" before the paragraph starting with "The handling of"
 Update 136.8.11.7.2 UPDATE_C(k) reference to the new sub-section

Response Response Status C

ACCEPT IN PRINCIPLE.

Resolve with comment i-89 using appropriate updated subclause numbers.

[Editor's note: For reference, the response to comment i-89 is copied here:
 ACCEPT IN PRINCIPLE.

This response is the same as the suggested remedy, except with subclause number corrected.

Change title of 136.8.11.4.1 to be "Initial condition setting request process".

Insert new subclause heading 136.8.11.4.2 titled "Initial condition setting response process" before the paragraph starting with "The handling of".

Update 136.8.11.7.2 UPDATE_IC reference to the new subclause 136.8.11.4.2.
]

IEEE P802.3cd 50 Gb/s, 100 Gb/s, 200 Gb/s Ethernet Initial Sponsor ballot comments

CI 136 SC 136.8.11.6 P218 L15 # i-159
 Dudek, Michael Cavium

Comment Type E Comment Status A <bucket>

It would read better if the order of the sentence were changed.

SuggestedRemedy

Change "The time from the receipt of a new request to the time that request is acknowledged shall be less than 2 ms when the receiver frame lock bit in the status field of transmitted training frames is set to 1." to "When the receiver frame lock bit in the status field of transmitted training frames is set to 1 the time from the receipt of a new request to the time that request is acknowledged shall be less than 2 ms."

Response Response Status C

ACCEPT IN PRINCIPLE.

Change FROM

"The time from the receipt of a new request to the time that request is acknowledged shall be less than 2 ms when the receiver frame lock bit in the status field of transmitted training frames is set to 1."

TO

"When the receiver frame lock bit in the status field of transmitted training frames is set to 1, the time from the receipt of a new request to the acknowledgment of that request shall be less than 2 ms."

CI 136 SC 136.8.11.7.3 P221 L27 # i-91
 Slavick, Jeff Broadcom Limited

Comment Type TR Comment Status A training

The initial suggested maximum link train duration provided during baseline adoptions was 1.5s which was made without significant operation of the newly proposed training protocol. With the benefit of additional experience gained over the last 18 months it has become clear that additional time would be beneficial. Some of the reasons the new protocol is taking longer are

- 1) Additional equalization tap provided (pre2)
- 2) Protocol serializes the coefficient updates
- 3) Additional Preset condition to test
- 4) Additional transmission modes (ie. precode)
- 5) PAM4 is more sensitive to mis-equalization

SuggestedRemedy

Change the max_wait_timer in 136.8.11.7.3 to be 3s
 Change the link_inhibit_fail_timer in Table 73-7 to range from 3.1 to 3.2 seconds for the PAM4 PHYs

Response Response Status W

ACCEPT.

CI 136 SC 136.9 P225 L39 # i-96
 Rysin, Alexander Mellanox Technologies

Comment Type TR Comment Status A ERL

Frequency domain return loss mask does not truly represent digital signaling at a given bit error ratio. There is no real proof that violating return loss masks is directly tied to failures and a number of false negatives have been shown. D2.0 comment 141, D2.1 comments 26, 27 and 28.

SuggestedRemedy

- * Add annex describing ERL measurement and computation. See prior presentations for description.
- * Remove the requirement for Differential return loss in Table 136-11.
- * Add a requirement for Effective Return Loss (ERL) to be greater than 18.2 dB in Table 136-11.
- * In 136.9.4 change "The receiver shall meet the return loss requirements specified in 92.8.4.2 and 92.8.4.3." to "The receiver shall meet the effective return loss requirement in 136.9.3."
- * Add a paragraph in 137.9.2 and to 137.9.3 - "Effective Return Loss (ERL, min) is 16.2 dB. There is no frequency domain return loss mask."

Response Response Status U

ACCEPT IN PRINCIPLE.

Implement the changes according to
http://www.ieee802.org/3/cd/public/Jan18/ran_3cd_01_0118.pdf.

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Cl 136 SC 136.9 P226 L8 # i-97
 Rysin, Alexander Mellanox Technologies

Comment Type TR Comment Status A ERL

Transmitter output residual ISI SNR_ISI (min) 36.8 dB (Clause 136) and 43 dB (Clause 137) is too high - can barely measure the IC through the test fixture. The warning NOTE in 120D.3.1.7 shows the issue, but doesn't solve it. The limits for SNR_ISI in Clause 136 and Clause 137 are even more stringent than in 120D. D2.0 comment 140, D2.1 comment 49, D2.2 comment 22.
 Since both SNR_ISI and Effective Return Loss (ERL) represent uncompensated reflections from the transmitter and the test fixtures, measurements of ERL can replace SNR_ISI.

SuggestedRemedy

- * Remove reference to SNR_ISI in Table 136-11 --Summary of transmitter specifications at TP2.
- * Add a requirement for Effective Return Loss (ERL) to be greater than 18.2 dB in Table 136-11.
- * Change paragraph 3 in 137.9.2 from "SNR_ISI is computed with Nb set to 12 and Dp set to 3. The value of SNR_ISI (min) is 43 dB." to "Effective Return Loss (ERL) is calculated with Nb set to 12 (see Annex New). ERL shall be at least 16.2 dB. The Transmitter Output residual ISI SNR_ISI specification in Table in Table 120D-1 does not apply."

Response Response Status U

ACCEPT IN PRINCIPLE.

Implement the changes according to
http://www.ieee802.org/3/cd/public/Jan18/ran_3cd_01_0118.pdf.

Cl 136 SC 136.9.3 P225 L23 # i-21
 RAN, ADEE Intel Corporation

Comment Type TR Comment Status R AC-coupling

Scope connection through AC coupling is not specified in this clause. Transmitter tests should be done through AC coupling (except for common mode tests).

See http://www.ieee802.org/3/cd/public/adhoc/archive/ran_112717_3cd_adhoc.pdf

SuggestedRemedy

In the first paragraph:

"Unless specified otherwise, all transmitter measurements are made for each lane separately, at TP2, utilizing the test fixtures specified in Annex 136B, using a test system with a fourth-order Bessel-Thomson low-pass response with 33 GHz 3 dB bandwidth"

Append: "connected as shown in Figure 92-15".

Response Response Status U

REJECT.

[Editor changed CommentType from GR to TR]

A similar issue is being addressed in the comment resolution in the 802.3cj revision project. The task force prefers to close this issue based on the resolution of comments in 802.3cj.

Cl 136 SC 136.9.3 P225 L37 # i-50
 RAN, ADEE Intel Corporation

Comment Type E Comment Status A <bucket>

"1 200"

According to the style guide (13.3.2), "In numbers of four digits, the space is not necessary, unless four-digit numbers are grouped in a column with numbers of five digits or more".

SuggestedRemedy

Remove the space here and in all other occurrences of four-digit numbers.

Consider removing spaces from all numbers within normal text (excluding tables).

Response Response Status C

ACCEPT IN PRINCIPLE.

Change "1 200" to "1200".

See also comment i-86.

[Editor's note: The reference to comment i-86 points another comment that deals with a similar topic.]

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Cl 136 SC 136.9.3 P225 L39 # i-74
 Mellitz, Richard Samtec, Inc.

Comment Type TR Comment Status A ERL

Comments and supporting presentations in prior drafts reported difficulty making SNDR and SNR_ISI measurements. SNR_ISI is a small difference of large numbers. Thus, is somewhat problematic. SNR_ISI is related to return loss. Clause 136.9.3 specifies return loss pointing to 92.8.3.2. Return loss is a measurement of reflections. However, return loss does not comprehend a DFE and impact of cable assembly return loss which is a component of host return loss as well as SNR_ISI. Re-reflection was also not considered in SNR_ISI.

SuggestedRemedy

ERL is a direct measure of pertinent reflections in the context of host loss and a DFE, plus allowing for a specific budgeted amount of cable assembly reflection derived from channel ERL. In table 136-11 remove row for "SNRISI (min.)". Replacing row for "differential output return loss (min)" in Table 136-11 with ERL (min) which shall be greater than 12.9 dB using $\beta_x=10.7e9$, and $\rho_x=0.28$, PTDR $T_r=18.9$ ps, and N_b is set by this clause. Also add annex 137A describing ERL computation. See presentation on implementation.

Response Response Status C

ACCEPT IN PRINCIPLE.

Implement the changes according to http://www.ieee802.org/3/cd/public/Jan18/ran_3cd_01_0118.pdf.

Cl 136 SC 136.9.3 P225 L46 # i-161
 Dudek, Michael Cavium

Comment Type TR Comment Status A Tx electrical

The value of linear fit pulse peak needs to correlate with the value expected with the transmitter and host board used in COM to specify the cable. The existing value for this parameter is the same as 802.3by which have larger die and package capacitance. It is expected therefore that the value of this parameter should be larger than 0.49

SuggestedRemedy

Complete the simulation and change the value. A presentation is expected. Make the change on page 228 line 23 as well.

Response Response Status C

ACCEPT IN PRINCIPLE.

http://www.ieee802.org/3/cd/public/Jan18/dudek_3cd_01_0118.pdf was reviewed.

Straw poll ET-2:

For 3rd bullet in slide 10 of [dudek_3cd_01_0118](#)

- A. Accept as is
- B. Accept changing sndr to 32.2 dB
- C. Do not accept the changes

Chicago rules:

A: 13
 B: 19
 C: 0

Straw poll ET-3

For "COM parameters" and "COM pass/fail criteria" in slide 10 of [dudek_3cd_01_0118](#)

- A. Accept all changes in both
- B. Accept only the changes in "COM parameters"
- C. Accept only the first four sub-bullets in "COM parameters" (Rd, Zc of package, Av/Afe, Ane), do not change the Zc for the PCB
- D. Do not accept any of the changes

Chicago rules

A: 4, B: 14, C: 17, D: 3

Straw poll ET-4

For "COM parameters" in slide 10 of [dudek_3cd_01_0118](#)

- A. Accept all sub-bullets
- B. Accept only the first four sub-bullets (Rd, Zc of package, Av/Afe, Ane), do not change the Zc for the PCB

Choose one

A: 12, B: 12

Second count

A: 12, B: 10

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Straw poll ET-5

For COM pass/fail criterion of cable test in slide 10 of dudek_01

A. Change from 3.0 dB to 3.3 dB

B. Change from 3.0 dB to 3.2 dB

C. Change from 3.0 dB to 3.1 dB

D. No change

Chicago rules

A: 7, B: 8, C: 9, D: 13

Implement the changes in slide 10 of dudek_3cd_01_0118 except for:

1. No change to "COM pass/fail criterion"

2. SNDR=32.2 dB instead of 32 dB

Cl 136 SC 136.9.3 P226 L7 # i-48
 RAN, ADEE Intel Corporation

Comment Type TR Comment Status A ERL

The SNR_ISI requirement in this clause (36.8 dB) is very demanding and may be impossible to meet with a test setup that includes imperfectly-matched test fixture and scope, and low-loss instrument-grade cables.

This specification is based on budgeting the residual ISI and the measured SNDR as the SNR_ISI COM parameter. But counting all measured ISI beyond the DFE range as residual ISI may be too stringent.

For instance: in reality, only a fraction of the transmitted energy will be returned from the remote end of the cable and bounce back (triple transit), due to the insertion loss of the cable (so this effect gets weaker with increased cable loss). But in a lab setup, the triple-transit reflection through a short, low-loss instrument-grade cable may be much stronger and cause degradation in the measured SNR_ISI.

Adding a directional coupler in the measurement may help reduce the latter effect.

The comment also applies to the similar specification in 137.9.2 (43 dB, which is impossible to measure in practice).

SuggestedRemedy

Add a recommendation for using a directional coupler in the measurement setup.

Consider replacing the SNR_ISI specification with an alternative method such as ERL.

Response Response Status C

ACCEPT IN PRINCIPLE.

Implement the changes according to
http://www.ieee802.org/3/cd/public/Jan18/ran_3cd_01_0118.pdf.

Cl 136 SC 136.9.3 P226 L7 # i-75
 Mellitz, Richard Samtec, Inc.

Comment Type TR Comment Status R <bucket>
 see previous

SuggestedRemedy
 see previous

Response Response Status W
 REJECT.

Comment and remedy do not provide sufficient detail to make any change in the draft.

Cl 136 SC 136.9.3 P226 L7 # i-49
 RAN, ADEE Intel Corporation

Comment Type TR Comment Status A Tx electrical

The SNR_ISI specification in 120D.3.1.7 uses N_b from Table 120D-8, which is 10; but in this clause the reference receiver has N_b=12. This should be an exception to the procedure.

SuggestedRemedy

Add to footnote b: Calculation of SNR_ISI is done with N_b given in Table 136-15 replacing the value in Table 120D-8.

Response Response Status C
 ACCEPT IN PRINCIPLE.

Add to footnote b: Calculation of SNR_ISI is done with N_b given in Table 136-15.

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CI 136 SC 136.9.3 P226 L10 # i-131
 Dawe, Piers J G Mellanox Technologies

Comment Type TR Comment Status A Tx electrical

As noted in D2.0 comment 143 and 144, and D2.1 comment 43, these TP2 Jrms and J4u limits, which are copies of the ones in Table 120D-1 (different BER, different test point) should be replaced with Jrms and J3u limits that are consistent (not the same) as the TP0a limits. Crosstalk at the connector combined with the slower edges increases J3u from TP0a to TP2.

SuggestedRemedy

Change J4u to J3u, here and in 137. Choose the limits at TP2 considering the jitter limit at TP0a, the mated compliance board crosstalk specs, and the slower edges at TP2. In 136.9.4.2.3 step e, change J4u to J3u (3 places).

Response Response Status C

ACCEPT IN PRINCIPLE.

Resolve using the responses to comments i-106 and i-140.

In addition, in 136.9.4.2.3 step e, change J4u to J3u (3 places).

[Editor's note: For reference, the responses to comments i-106 and i-140 are copied here:

Comment i-106:

ACCEPT IN PRINCIPLE.

Based on the comment, we are assuming that the commenter was referring to 136.9.3, not 137.9.2.

http://www.ieee802.org/3/cd/public/Jan18/healey_3cd_01_0118.pdf was reviewed.

Per comment i-140, J4u was changed to J3u with a value of 0.106 at TP0a, therefore the suggested remedy has to be modified accordingly

The increase in J3u from TP0a to TP2 based on the analysis in the presentation is 0.009 UI.

In Table 136-11, change from J4u with value 0.118 to J3u with value 0.115, and add a reference to the new subclause added by comment i-140. Add a footnote to the output jitter row with the text:

"J4u, JRMS, and Even-odd jitter measurements are made with a single transmit equalizer setting selected to compensate for the loss of the host channel".

Comment i-140:

ACCEPT IN PRINCIPLE.

The informative note in the suggested remedy is correct only in case the jitter distribution matches the dual-Dirac model exactly (with A_DD=0.02 UI and Sigma_RJ=0.01 UI). It is not

true in general, and real transmitters may meet one specification and fail another.

In 137.9.2, add exception 5: the J4u limit in Table 120E-1 does not apply but the maximum J3u is 0.106 UI.

In Eq 136-7 and 136-8 and the NOTE, change J4u to J3u, Q4=3.8906 to Q3=3.2905, Q(Q3) = 5 x 10⁻⁴.

Jrms and it value don't change.

Add a new subclause:

136.9.3.n J3u Jitter

J3u is defined similarly to J4u (see 120D.3.1.8). J3u is defined as the time interval that includes all but 10⁻³ of fJ(t), from the 0.05th to the 99.95th percentile of fJ(t).

The informative note in the suggested remedy is correct only in case the jitter distribution matches the dual-Dirac model exactly (with A_DD=0.02 UI and Sigma_RJ=0.01 UI). It is not true in general, and real transmitters may meet one specification and fail another. Therefore it will not be added.

Implement with editorial license.

]

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Cl 136 SC 136.9.3 P226 L22 # i-88
 Szczepanek, Andre HSZ Consulting Ltd

Comment Type TR Comment Status A editor's notes <cc>

The editors note "The values for SNDR, SNR_ISI, and SNR_TX require confirmation and may change." indicates that values in Table 136-11 are not ready for standardisation.

Like-wise the editors notes on pages: 236, 271, 272, & 273 which all relate to table values that "require confirmation and may change".

SuggestedRemedy

Gain the required confirmation of the values and then remove the editors note(s).

Response Response Status C

ACCEPT IN PRINCIPLE.

Resolve using the response to comment i-12.

[Editor's note: For reference, the response to comment i-12 is copied here:

ACCEPT IN PRINCIPLE.

The two editor's notes in clause 136 have been addressed by
http://www.ieee802.org/3/cd/public/Jan18/dudek_3cd_01_0118.pdf.

Remove all editor's notes in cause 136.

Relating to the editor's notes in Clause 138, measured data has been presented to the task force supporting the current specifications.

See:
http://www.ieee802.org/3/cd/public/Jan18/king_3cd_02_0118.pdf
http://www.ieee802.org/3/cd/public/adhoc/archive/chang_011018_3cd_02_adhoc-v2.pdf

Remove all editor's notes in Clause 138.

]

Cl 136 SC 136.9.4 P259 L40 # i-76
 Mellitz, Richard Samtec, Inc.

Comment Type TR Comment Status A ERL

Clause 136.9.4 specifies return loss pointing to 92.8.4.2. Return loss is a measurement of reflections. However, return loss does not comprehend a DFE and impact of cable assembly return loss.

SuggestedRemedy

ERL is a direct measure of pertinent reflections in the context of package loss and a DFE, plus allowing for a specific budgeted amount of cable assemble reflection derived from channel ERL. Remove the reference to 92.9.4.2. Add text indicating that ERL (min) for the host input shall be greater than 12.9 dB using $\beta_x=10.7e9$, and $\rho_x=0.28$, PTDR $T_r=18.9ps$, and N_b is set by this clause. Also add annex 137A describing ERL computation. See presentation on implementation.

Response Response Status C

ACCEPT IN PRINCIPLE.

Implement the changes according to
http://www.ieee802.org/3/cd/public/Jan18/ran_3cd_01_0118.pdf.

IEEE P802.3cd 50 Gb/s, 100 Gb/s, 200 Gb/s Ethernet Initial Sponsor ballot comments

Cl 136 SC 136.9.4.2 P230 L26 # i-101
 Healey, Adam Broadcom Ltd.

Comment Type TR Comment Status A Rx electrical

The responses to comments #135 and #136 against IEEE P802.3 (IEEE 802.3cj) D2.0 clarified that the COM value for interference tolerance testing is a "target" and not a "max" value. Table 136-13 would also benefit from this clarification.

SuggestedRemedy

Straddle the "min" and "max" columns for the COM row (keeping the same COM value). Add a note to the COM value similar to note c) of Table 110-6 in IEEE P802.3 (IEEE 802.3cj)/D3.0 i.e. "The COM value is the target value for the SNR_TX calibration defined in 136.9.4.2.3 item f). The SNR_TX value measured at the Tx test reference should be as close as practical to the value needed to produce the target COM. If lower SNR_TX values are used, this would demonstrate margin to the specification but this is not required for compliance."

Response Response Status C

ACCEPT IN PRINCIPLE.

Resolve using the response to comment i-132.

[Editor's note:

For reference, the response to i-132 is "ACCEPT" and the suggested remedy is copied here: "In Table 136-13, straddle the "Min" and "Max" columns for the "COM" row and place the contents of the "Max" column into the straddled column. Add the following table footnote to the "COM" parameter label.

"The COM value is the target value for the SNR_TX calibration defined in 136.9.4.2.3 item f). The SNR_TX value measured at the Tx test reference should be as close as practical to the value needed to produce the target COM. If lower SNR_TX values are used, this would demonstrate margin to the specification but this is not required for compliance.""

]

Cl 136 SC 136.9.4.2 P230 L26 # i-132
 Dawe, Piers J G Mellanox Technologies

Comment Type TR Comment Status A Rx electrical

The COM value in the receiver interference tolerance isn't a maximum, it's the reference value that defines what we mean by receiver interference tolerance, and it is used as a target when adjusting the injected noise. See maintenance D2.0 comments 135 and 136.

SuggestedRemedy

In Table 136-13, straddle the "Min" and "Max" columns for the "COM" row and place the contents of the "Max" column into the straddled column. Add the following table footnote to the "COM" parameter label.

"The COM value is the target value for the SNR_TX calibration defined in 136.9.4.2.3 item f). The SNR_TX value measured at the Tx test reference should be as close as practical to the value needed to produce the target COM. If lower SNR_TX values are used, this would demonstrate margin to the specification but this is not required for compliance."

Response Response Status C

ACCEPT.

IEEE P802.3cd 50 Gb/s, 100 Gb/s, 200 Gb/s Ethernet Initial Sponsor ballot comments

Cl 136 SC 136.9.4.2 P230 L26 # i-52
 RAN, ADEE Intel Corporation

Comment Type T Comment Status A Rx electrical

COM is specified as maximum here.

As of D3.0 of 802.3cj, the COM in receiver tolerance tests was changed to be a target (or both minimum and maximum), with a clarifying comment. The same should be done here.

SuggestedRemedy

Straddle the COM value across all columns.

Add a footnote with the following text:

The COM value is the target for the injected noise calibration defined in 136.9.4.2.3 step f). The noise level should be as close as practical to the value needed to produce the target COM. If higher noise levels are used, it would demonstrate margin to the specification but this is not required for compliance.

Response Response Status C

ACCEPT IN PRINCIPLE.

Resolve using the response to comment i-132.

[Editor's note:

For reference, the response to i-132 is "ACCEPT" and the suggested remedy is copied here: "In Table 136-13, straddle the "Min" and "Max" columns for the "COM" row and place the contents of the "Max" column into the straddled column. Add the following table footnote to the "COM" parameter label.

"The COM value is the target value for the SNR_TX calibration defined in 136.9.4.2.3 item f). The SNR_TX value measured at the Tx test reference should be as close as practical to the value needed to produce the target COM. If lower SNR_TX values are used, this would demonstrate margin to the specification but this is not required for compliance.""

]

Cl 136 SC 136.9.4.2 P230 L27 # i-51
 RAN, ADEE Intel Corporation

Comment Type T Comment Status A Rx electrical

b_max(1) and DER_0 values specified here are the same as the values for the cable assembly specification (Table 136-15) so they need not be listed.

SuggestedRemedy

Delete the bottom two rows from Table 136-13.

Response Response Status C

ACCEPT.

Cl 136 SC 136.9.4.2.2 P230 L42 # i-133
 Dawe, Piers J G Mellanox Technologies

Comment Type T Comment Status R Rx electrical

As pointed out in hidaka_3cd_01a_0517.pdf and hidaka_060717_3cd_adhoc-v2.pdf, and D2.0 comment 72, we need a spec for the test channel RL (Rx end) that's better than the regular cable RL spec given by 92.10.3, eq 92-27: 16.5-2rt.f to 4.1 GHz then 10.66-14log10(f/5.5). The comment proposed the mated test fixtures return loss limit, eq 92-38, 20-f to 4 GHz then 18-0.5f. Adopting a limit about half way between these two would be much better than doing nothing. See hidaka_3cd_01a_0517 slides 17/18 to end.

SuggestedRemedy

Insert new requirement into 136.9.4.2.2:

The test channel is the same as the one defined in 110.8.4.2.2, except that the cable assembly meets the requirements of 136.11, the differential return loss of the test channel measured at the Rx test reference (see Figure 110-3b) meets Equation (136-new)."

Eq 136-new: 18-f to 4 GHz then 16-0.5f (about half way between eq 92-27 and eq 92-38).

Response Response Status C

REJECT.

Comment #72 against D2.0 was rejected due to lack of consensus.

A straw poll was taken.

Straw poll ET-1:

A. I support accepting the suggested remedy or applying a similar change.

B. I support retaining the current text, equations and values.

Result: A: 5, B: 8

There is no consensus for making the suggested change.

Cl 136 SC 136.9.4.2.3 P231 L12 # i-28
 RAN, ADEE Intel Corporation

Comment Type E Comment Status A Rx electrical

"Equation (93A-19)" is an external cross reference.

SuggestedRemedy

Unless overtaken by another comment, apply external format.

Response Response Status C

ACCEPT IN PRINCIPLE.

Apply "external" format to the text "Equation (93A-19)".

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Cl 136 SC 136.9.4.2.3 P231 L12 # i-29
 RAN, ADEE Intel Corporation

Comment Type T Comment Status A beta

Following the updates in the revision project (as of 802.3cj D3.0), the correction term beta is not needed any more.

The definition of Equation (93A-19) encompasses Equation (93A-46), so only the value of T_r is needed.

SuggestedRemedy

Change FROM

"The filtered voltage transfer function $H(k)(f)$ calculated in Equation (93A-19) uses the filter $H_t(f)$ defined by Equation (93A-46), where β is 2 and T_r is the 20% to 80% transition time at the Tx test reference"

TO

"The filtered voltage transfer function $H(k)(f)$ calculated in Equation (93A-19) uses T_r equal to the 20% to 80% transition time at the Tx test reference."

Response Response Status C

ACCEPT.

Cl 136 SC 136.9.4.2.3 P231 L13 # i-18
 Anslow, Peter Ciena Corporation

Comment Type T Comment Status A beta

Comment #116 against D2.0 of the 802.3 revision project changed "<beta>" to "2" in Equation (93A-46). See: <http://www.ieee802.org/3/cj/comments/P8023-D2p0-Comments-Final-byID.pdf#page=30>
 When the P802.3cd draft is changed to become an amendment to the output of the revision, equivalent changes need to be made to the P802.3cd draft.

SuggestedRemedy

When the P802.3cd draft is changed to become an amendment to the output of the revision:
 In 136.9.4.2.3, remove the phrase "<beta> is 2 and" from the second sentence of item d).
 In 136.11.7, remove the phrase "and <beta> is 2" from the second sentence.
 In 137.10, remove the phrase "and <beta> is 2" from the first sentence.

Response Response Status C

ACCEPT IN PRINCIPLE.

Resolve using the responses to comments i-29 and i-100.

[Editor's note:

For reference the response to i-29 is ACCEPT and the suggested remedy is copied here:

"Change FROM

"The filtered voltage transfer function $H(k)(f)$ calculated in Equation (93A-19) uses the filter $H_t(f)$ defined by Equation (93A-46), where β is 2 and T_r is the 20% to 80% transition time at the Tx test reference"

TO

"The filtered voltage transfer function $H(k)(f)$ calculated in Equation (93A-19) uses T_r equal to the 20% to 80% transition time at the Tx test reference."

"

For reference, the response to comment i-100 is "ACCEPT" and the suggested remedy is copied here:

"Remove the phrase "and <beta> is 2" at line 50 here and in 137.10 (p251, 149)."

]

IEEE P802.3cd 50 Gb/s, 100 Gb/s, 200 Gb/s Ethernet Initial Sponsor ballot comments

Cl 136 SC 136.9.4.2.3 P231 L25 # i-139
 Dawe, Piers J G Mellanox Technologies

Comment Type T Comment Status R Rx electrical

SNDR should be measured in the right bandwidth, or at least sigma_e and sigma_n should, because it's used in COM without further filtering: eq 93A-30. And see another comment.

SuggestedRemedy

Add another exception that sigma_e and sigma_n are found from signals observed with a fourth-order Bessel-Thomson low-pass response with 19.34 GHz 3 dB bandwidth.

Response Response Status C

REJECT.

Per Equation (93A-19) the voltage transfer function includes the receiver filter, which is a fourth-order Butterworth filter (with a cutoff frequency f_r, 19.9219 GHz for this clause).

The noise corresponding to SNDR is affected by h(0), which is the integral of that voltage transfer function, so it is affected by the receiver filter.

Note that the SNDR is calibrated by injecting "Broadband noise". Typical test equipment generate noise in a limited bandwidth, so there is little practical concern.

[Editor's note: comment i-138 deals with a similar topic for the transmitter SNDR.]

Cl 136 SC 136.9.4.2.3 P231 L36 # i-53
 RAN, ADEE Intel Corporation

Comment Type TR Comment Status A Rx electrical

In equation (136-7), if J4u is too large compared to J_RMS, then the discriminant may be negative and the resulting A_DD may become complex.

This may happen in practice, if the transmitter in the test does not have a dual-Dirac jitter distribution; for example, a low jitter most of the time with large but not too frequent excursions (such as sinusoidal jitter) may cause large J4 and small J_RMS.

Assuming we allow such a transmitter in a test setup (to enable injecting sinusoidal jitter in the JTT), it should be considered to have a large but purely "deterministic" jitter; A_DD=J4/2 and sigma_RJ=0.

As a sanity check, a Dual-dirac distribution with these values would yield the original J4u but its J_RMS would be higher than what was measured. This means COM would be "too pessimistic" and it may somewhat relax the test's stress; I think we can live with it.

SuggestedRemedy

Change equation (136-7) to consist of two cases:

When $(Q^4+1)*J_RMS^2 \geq (J4u/2)^2$: the current equation holds.

Otherwise: J4u/2.

Response Response Status C

ACCEPT IN PRINCIPLE.

Add a note stating that if the discriminant is negative, a different transmitter should be used.

Implement with editorial license.

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Cl 136 SC 136.9.4.4 P233 L11 # i-92
Kirkland, William

Comment Type T Comment Status A Rx electrical

I take issue with the use of the word "approximately" where using more than 1 or two significant figures. e.g. approximately 37.64706 ps is hardly approximate, it is quite exact.

SuggestedRemedy

Remedy: use a judicious choice of significant digitals when saying approximately, e.g. 1/Baud Rate or approximately 37.6 ps

Response Response Status C

ACCEPT IN PRINCIPLE.

[Editor changed CommentType from G to T.]

Using language from similar clauses (e.g., Clause 85, Annex 120E, Annex 83E) change the sentence to:

This translates to a nominal unit interval of 37.64706 ps.

Cl 136 SC 136.11 P233 L42 # i-54
RAN, ADEE Intel Corporation

Comment Type T Comment Status A AC-coupling

The important requirement that cable assemblies are AC coupled does not appear in the Cable assembly characteristics as it should.

The requirement does exist in the MDI annex 136C, but that annex mainly deals with mechanical parameters and pin-outs; other than AC coupling (in the overview) it contains no electrical parameters. Readers interested in AC coupling specifications may have a hard time finding it.

It is suggested to move the AC coupling requirement to the Cable assembly characteristics subclause, with the following considerations:

1. AC coupling is between corresponding contacts in two connectors at each end (may be obvious but is not currently stated).
2. The current text in the MDI annex specifies AC coupling "within the plug connector"; This goes without saying if AC coupling requirement is part of the cable assembly specification (and if anyone implements AC coupling in the middle of the cable, we shouldn't care - it is not observable).
3. The text also includes the sentence "The capacitor limits the inrush charge and baseline wander". This is not a specification, and it's arguably even informative, so it doesn't seem to be required.

SuggestedRemedy

Insert the following paragraph after the paragraph starting with "50GBASE-CR, 100GBASE-CR2, and 200GBASE-CR4":

"The path between corresponding contacts in the connectors at each end of a cable assembly shall include AC-coupling. It should be noted that there may be various methods for AC-coupling in actual implementations. The low-frequency 3 dB cutoff of the AC-coupling shall be less than 50 kHz. It is recommended that the value of the coupling capacitors be 100 nF."

Delete the fourth paragraph in annex 136C (which deals with AC coupling).

Change the reference of PICS item CA9 from 136.12 to 136.11, and change value comment to "Between corresponding contacts, 3 dB cutoff frequency less than 50 kHz".

Response Response Status C

ACCEPT IN PRINCIPLE.

Resolve using the response to comment i-160.

[Editor's note: For reference, the response to comment i-160 is copied here:

ACCEPT IN PRINCIPLE.

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Delete paragraph P387, L41.

Insert paragraph in 136.11, at P233, L42:

"For 50GBASE-CR, 100GBASE-CR2, and 200GBASE-CR4, the lanes are AC-coupled. The AC-coupling shall be within the cable assembly. It is recommended that it is within the plug connectors. It should be noted that there may be various methods for AC-coupling in actual implementations. The low-frequency 3 dB cutoff of the AC-coupling shall be less than 50 kHz. It is recommended that the value of the coupling capacitors be 100 nF. The capacitor limits the inrush charge and baseline wander."

In the sentence Page 225 line 5 and 6, change the reference to 136.11 and delete "plug connectors" .

In PICS item CA9, change the reference from 136.12 to 136.11.

]

Cl 136	SC 136.11.7	P234	L50	# i-30
RAN, ADEE		Intel Corporation		
Comment Type	T	Comment Status A		
Following the updates in the revision project (as of 802.3cj D3.0), the correction term beta is not needed any more.				
Also in 136.9.4.2.3.				
SuggestedRemedy				
Delete "and \beta is 2" here.				
Delete "\beta is 2 and" in 136.9.4.2.3.				
Response		Response Status C		
ACCEPT IN PRINCIPLE.				
Resolve using the responses to comments i-100 and i-29.				
[Editor's note: For reference the response to i-29 is ACCEPT and the suggested remedy is copied here: "Change FROM "The filtered voltage transfer function H(k)(f) calculated in Equation (93A-19) uses the filter Ht(f) defined by Equation (93A-46), where \beta is 2 and Tr is the 20% to 80% transition time at the Tx test reference" TO "The filtered voltage transfer function H(k)(f) calculated in Equation (93A-19) uses Tr equal to the 20% to 80% transition time at the Tx test reference." " For reference, the response to comment i-100 is "ACCEPT" and the suggested remedy is copied here: "Remove the phrase "and <beta> is 2" at line 50 here and in 137.10 (p251, 149)." "]				

Cl 136	SC 136.11.7	P234	L50	# i-100
Healey, Adam		Broadcom Ltd.		
Comment Type	TR	Comment Status A		
IEEE P802.3cd will end up being an amendment to IEEE Std 802.3-201x (currently IEEE P802.3 (IEEE 802.3cj) D3.0 which is in Sponsor ballot). The proposed changes and editing instructions should be aligned with the expected base document. The term <beta> has been removed from Equation (93A-46) (its value has been fixed at 2).				
SuggestedRemedy				
Remove the phrase "and <beta> is 2" at line 50 here and in 137.10 (p251, 149).				
Response		Response Status C		
ACCEPT.				

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CI 136 SC 136.11.7 P235 L18 # i-162
Dudek, Michael Cavium

Comment Type TR Comment Status A

The use of the approx 110 Ohm PCB trace in the COM calculation provides cables with impedances close to this value (or higher impedance still) a false improvement in COM relative to their expected system performance. It would be better to use 100 ohm PCB traces and it would be better to also change the package parameters to the nominal values used in clause 137. This however will significantly improve the COM values for the cable, implying better performance than is expected in the real system with hosts with 100 Ohm +/- 10% PCB traces. It will also increase the COM in the interference tolerance test resulting in more noise being added in the test.

SuggestedRemedy

In table 136-15 change Rd to 50 Ohms and Zc to 95 Ohm
On page 236 line 38 and line 49, and page 237 line 17 Change "parameter values given in Table 92-12" to "parameter values given in Table 92-12 except that Zc=100 Ohms"
On page 235 line 2 and in table 136-14 change the pass/fail spec for COM from 3dB to 4dB. Also in the PICs on page 244 line 6.
In Table 136-13 change the COM from 3 to 3.5dB.
A presentation will be provided.

Response Response Status C

ACCEPT IN PRINCIPLE.

Resolve using the response to comment i-161.

[Editor's note: For reference, the response to comment i-161 is copied here:

ACCEPT IN PRINCIPLE.

[Http://www.ieee802.org/3/cd/public/Jan18/dudek_3cd_01_0118.pdf](http://www.ieee802.org/3/cd/public/Jan18/dudek_3cd_01_0118.pdf) was reviewed.

Straw poll ET-2:

For 3rd bullet in slide 10 of dudek_3cd_01_0118

- A. Accept as is
- B. Accept changing snr to 32.2 dB
- C. Do not accept the changes

Chicago rules:

- A: 13
- B: 19
- C: 0

Straw poll ET-3

For "COM parameters" and "COM pass/fail criteria" in slide 10 of dudek_3cd_01_0118

- A. Accept all changes in both
- B. Accept only the changes in "COM parameters"
- C. Accept only the first four sub-bullets in "COM parameters" (Rd, Zc of package, Av/Afe, Ane), do not change the Zc for the PCB

D. Do not accept any of the changes
Chicago rules
A: 4, B: 14, C: 17, D: 3

Straw poll ET-4

For "COM parameters" in slide 10 of dudek_3cd_01_0118

- A. Accept all sub-bullets
 - B. Accept only the first four sub-bullets (Rd, Zc of package, Av/Afe, Ane), do not change the Zc for the PCB
- Choose one
A: 12, B: 12
Second count
A: 12, B: 10

Straw poll ET-5

For COM pass/fail criterion of cable test in slide 10 of dudek_01

- A. Change from 3.0 dB to 3.3 dB
 - B. Change from 3.0 dB to 3.2 dB
 - C. Change from 3.0 dB to 3.1 dB
 - D. No change
- Chicago rules
A: 7, B: 8, C: 9, D: 13

Implement the changes in slide 10 of dudek_3cd_01_0118 except for:

1. No change to "COM pass/fail criterion"
2. SNDR=32.2 dB instead of 32 dB

]

IEEE P802.3cd 50 Gb/s, 100 Gb/s, 200 Gb/s Ethernet Initial Sponsor ballot comments

CI 136 SC 136.11.7 P235 L18 # i-134
Dawe, Piers J G Mellanox Technologies

Comment Type TR Comment Status A

The COM impedances should be moved towards neutral, as explained in D2.0 comment 71 and 113.

Suggested Remedy

Make changes similar to D2.0 comment 71 and hidaka_3cd_01_0717

Response Response Status C

ACCEPT IN PRINCIPLE.

Resolve using the response to comment i-161.

[Editor's note: For reference, the response to comment i-161 is copied here:

ACCEPT IN PRINCIPLE.

[Http://www.ieee802.org/3/cd/public/Jan18/dudek_3cd_01_0118.pdf](http://www.ieee802.org/3/cd/public/Jan18/dudek_3cd_01_0118.pdf) was reviewed.

Straw poll ET-2:

For 3rd bullet in slide 10 of dudek_3cd_01_0118

- A. Accept as is
- B. Accept changing sndr to 32.2 dB
- C. Do not accept the changes

Chicago rules:

A: 13
B: 19
C: 0

Straw poll ET-3

For "COM parameters" and "COM pass/fail criteria" in slide 10 of dudek_3cd_01_0118

- A. Accept all changes in both
- B. Accept only the changes in "COM parameters"
- C. Accept only the first four sub-bullets in "COM parameters" (Rd, Zc of package, Av/Afe, Ane), do not change the Zc for the PCB
- D. Do not accept any of the changes

Chicago rules

A: 4, B: 14, C: 17, D: 3

Straw poll ET-4

For "COM parameters" in slide 10 of dudek_3cd_01_0118

- A. Accept all sub-bullets
 - B. Accept only the first four sub-bullets (Rd, Zc of package, Av/Afe, Ane), do not change the Zc for the PCB
- Choose one

A: 12, B: 12
Second count
A: 12, B: 10

Straw poll ET-5

For COM pass/fail criterion of cable test in slide 10 of dudek_01

- A. Change from 3.0 dB to 3.3 dB
 - B. Change from 3.0 dB to 3.2 dB
 - C. Change from 3.0 dB to 3.1 dB
 - D. No change
- Chicago rules
A: 7, B: 8, C: 9, D: 13

Implement the changes in slide 10 of dudek_3cd_01_0118 except for:

1. No change to "COM pass/fail criterion"
2. SNDR=32.2 dB instead of 32 dB

]

IEEE P802.3cd 50 Gb/s, 100 Gb/s, 200 Gb/s Ethernet Initial Sponsor ballot comments

Cl 136 SC 136.11.7 P235 L18 # i-60
 RAN, ADEE Intel Corporation

Comment Type TR Comment Status R

Package transmission line characteristic impedance is set at 90 Ohm. This is an increase from the default value in Annex 93A which is 78.2 Ohm.

The reason for the relatively low value 78.2 Ohm was that to typical packages (especially large ones with many lanes) have lower impedance to improve their matching to silicon and ball impedances, and to reduce the trace insertion loss. This is not expected to change; most practical packages will not have impedance close to 100 Ohm.

In practice, termination can be adjusted and board design can be optimized to match lower impedance package and improve performance (even if cables are 100 Ohm)

It is suggested to acknowledge the expected lower impedance of practical devices in the reference package and termination parameters: assume packages are 80 Ohm while termination and board are 90 Ohm (imperfect matching).

Also applies in 137.10 (Table 137-5).

SuggestedRemedy

In both Table 136-15, and Table 137-5, change the value of Zc to 80 Ohm and Rd to 45 Ohm.

In 136.11.7.1, add an exception to the parameter values from Table 92-12: Z_c is set to 90 Ohm.

Consider changing the reference impedance for channels from 100 Ohm to 85 Ohm (136.11.1 and 137.10, and COM tables).

Response Response Status U

REJECT.

The response to comment i-161 resulted in different changes than the ones in the suggested remedy.

Cl 136 SC 136.11.7 P235 L45 # i-17
 Anslow, Peter Ciena Corporation

Comment Type T Comment Status A

Comment #132 against D2.0 of the 802.3 revision project changed the name of COM parameter f_z to be "Continuous time filter, zero frequency for g_DC = 0". See: <http://www.ieee802.org/3/cj/comments/P8023-D2p0-Comments-Final-byID.pdf#page=35>
 When the P802.3cd draft is changed to become an amendment to the output of the revision, equivalent changes need to be made to the P802.3cd draft.

SuggestedRemedy

When the P802.3cd draft is changed to become an amendment to the output of the revision: Change the name of f_z to be "Continuous time filter, zero frequency for g_DC = 0" in Table 136-15 and Table 137-5

Response Response Status C

ACCEPT.

Cl 136 SC 136.11.7 P235 L45 # i-102
 Healey, Adam Broadcom Ltd.

Comment Type TR Comment Status A

IEEE P802.3cd will end up being an amendment to IEEE Std 802.3-201x (currently IEEE P802.3 (IEEE 802.3cj) D3.0 which is in Sponsor ballot). The proposed changes and editing instructions should be aligned with the expected base document. Parameter f_z has been given the more accurate name "Continuous time filter, zero frequency for g_DC = 0".

SuggestedRemedy

Change the name of parameter f_z in Tables 136-15 and 137-5 accordingly.

Response Response Status C

ACCEPT IN PRINCIPLE.

Resolve using the response to comment i-17.

[Editor's note: For reference, the response to comment i-17 was "ACCEPT" and the suggested remedy is copied here:

When the P802.3cd draft is changed to become an amendment to the output of the revision: Change the name of f_z to be "Continuous time filter, zero frequency for g_DC = 0" in Table 136-15 and Table 137-5

]

IEEE P802.3cd 50 Gb/s, 100 Gb/s, 200 Gb/s Ethernet Initial Sponsor ballot comments

CI 136 SC 136.11.7 P235 L51 # i-163
Dudek, Michael Cavium

Comment Type TR Comment Status A

It is intended that the same ASIC would be used for CR and KR.

SuggestedRemedy

Change the values of Av and Afe to 0.415 and Ane to 0.604

Response Response Status C

ACCEPT IN PRINCIPLE.

Resolve using the response to comment i-161.

[Editor's note: For reference, the response to comment i-161 is copied here:

ACCEPT IN PRINCIPLE.

http://www.ieee802.org/3/cd/public/Jan18/dudek_3cd_01_0118.pdf was reviewed.

Straw poll ET-2:

For 3rd bullet in slide 10 of dudek_3cd_01_0118

- A. Accept as is
- B. Accept changing snr to 32.2 dB
- C. Do not accept the changes

Chicago rules:

A: 13
B: 19
C: 0

Straw poll ET-3

For "COM parameters" and "COM pass/fail criteria" in slide 10 of dudek_3cd_01_0118

- A. Accept all changes in both
- B. Accept only the changes in "COM parameters"
- C. Accept only the first four sub-bullets in "COM parameters" (Rd, Zc of package, Av/Afe, Ane), do not change the Zc for the PCB
- D. Do not accept any of the changes

Chicago rules

A: 4, B: 14, C: 17, D: 3

Straw poll ET-4

For "COM parameters" in slide 10 of dudek_3cd_01_0118

- A. Accept all sub-bullets
- B. Accept only the first four sub-bullets (Rd, Zc of package, Av/Afe, Ane), do not change the Zc for the PCB

Choose one

A: 12, B: 12

Second count

A: 12, B: 10

Straw poll ET-5

For COM pass/fail criterion of cable test in slide 10 of dudek_01

- A. Change from 3.0 dB to 3.3 dB
- B. Change from 3.0 dB to 3.2 dB
- C. Change from 3.0 dB to 3.1 dB
- D. No change

Chicago rules

A: 7, B: 8, C: 9, D: 13

Implement the changes in slide 10 of dudek_3cd_01_0118 except for:

1. No change to "COM pass/fail criterion"
2. SNDR=32.2 dB instead of 32 dB

]

IEEE P802.3cd 50 Gb/s, 100 Gb/s, 200 Gb/s Ethernet Initial Sponsor ballot comments

Cl 136 SC 136.11.7.1 P236 L39 # i-135
 Dawe, Piers J G Mellanox Technologies

Comment Type TR Comment Status A

Using 109.8 ohm PCB impedance in COM could provide an incentive to build cables to that (wrong) impedance, which seems unhelpful.

SuggestedRemedy

Change text to ..."and the parameter values given in Table 92-12, with the exception that Zc is 100 [ohm]." Similarly in 136.11.7.1.1 and 136.11.7.1.2.

Response Response Status C

ACCEPT IN PRINCIPLE.

Resolve using the response to comment i-161.

[Editor's note: For reference, the response to comment i-161 is copied here:

ACCEPT IN PRINCIPLE.

http://www.ieee802.org/3/cd/public/Jan18/dudek_3cd_01_0118.pdf was reviewed.

Straw poll ET-2:

For 3rd bullet in slide 10 of dudek_3cd_01_0118

- A. Accept as is
 - B. Accept changing sn dr to 32.2 dB
 - C. Do not accept the changes
- Chicago rules:

A: 13
 B: 19
 C: 0

Straw poll ET-3

For "COM parameters" and "COM pass/fail criteria" in slide 10 of dudek_3cd_01_0118

- A. Accept all changes in both
 - B. Accept only the changes in "COM parameters"
 - C. Accept only the first four sub-bullets in "COM parameters" (Rd, Zc of package, Av/Afe, Ane), do not change the Zc for the PCB
 - D. Do not accept any of the changes
- Chicago rules
 A: 4, B: 14, C: 17, D: 3

Straw poll ET-4

For "COM parameters" in slide 10 of dudek_3cd_01_0118

- A. Accept all sub-bullets
- B. Accept only the first four sub-bullets (Rd, Zc of package, Av/Afe, Ane), do not change the Zc for the PCB

Choose one
 A: 12, B: 12
 Second count
 A: 12, B: 10

Straw poll ET-5

For COM pass/fail criterion of cable test in slide 10 of dudek_01

- A. Change from 3.0 dB to 3.3 dB
- B. Change from 3.0 dB to 3.2 dB
- C. Change from 3.0 dB to 3.1 dB
- D. No change

Chicago rules
 A: 7, B: 8, C: 9, D: 13

Implement the changes in slide 10 of dudek_3cd_01_0118 except for:

1. No change to "COM pass/fail criterion"
2. SNDR=32.2 dB instead of 32 dB

]

Cl 136A SC 136A.2 P379 L21 # i-173
 Dudek, Michael Cavium

Comment Type T Comment Status A

It is strange to say that characteristics are constrained in an informative section.

SuggestedRemedy

Change the sentence to "The recommended transmitter characteristics at TP0 as measured at TP0a are described in 137.9.2"

Response Response Status C

ACCEPT.

Cl 136A SC 136A.3 P379 L26 # i-174
 Dudek, Michael Cavium

Comment Type T Comment Status A

It is strange to say that characteristics are constrained in an informative section.

SuggestedRemedy

Change the sentence to "The recommended receiver characteristics at TP5 as measured at TP5a are described in 137.9.3"

Response Response Status C

ACCEPT.

IEEE P802.3cd 50 Gb/s, 100 Gb/s, 200 Gb/s Ethernet Initial Sponsor ballot comments

Cl 136A SC 136A.7 P381 L43 # i-175
 Dudek, Michael Cavium

Comment Type E Comment Status A

The Channel Operating Margin (min) value is not in Table 136-15 and this is a normative value not an informative value.

SuggestedRemedy

Delete section 136A.7

Response Response Status C

ACCEPT IN PRINCIPLE.

Change the content of 136A.7 to:

The Channel Operating Margin (COM) for the channel between TP0 and TP5, computed using the procedure in 93A.1 and the parameters in Table 137-5, is recommended to be greater than or equal to 3 dB.

Cl 136C SC 136C.1 P387 L41 # i-160
 Dudek, Michael Cavium

Comment Type T Comment Status A AC-coupling

The requirement for the AC coupling of the cable is a cable requirement not an MDI requirement. Exactly where the AC coupling is in the cable is not important.

SuggestedRemedy

Delete this paragraph here and insert an equivalent somewhat modified paragraph in section 136.11 Paragraph to say "For 50GBASE-CR, 100GBASE-CR2, and 200GBASE-CR4, the lanes are AC-coupled. The AC-coupling shall be within the cable assembly. It is recommended that it is within the plug connectors. It should be noted that there may be various methods for AC-coupling in actual implementations. The low-frequency 3 dB cutoff of the AC-coupling shall be less than 50 kHz. It is recommended that the value of the coupling capacitors be 100 nF. The capacitor limits the inrush charge and baseline wander." Change the reference on Page 225 line 6 to 136.11

Response Response Status C

ACCEPT IN PRINCIPLE.

Delete paragraph P387, L41.

Insert paragraph in 136.11, at P233, L42:

"For 50GBASE-CR, 100GBASE-CR2, and 200GBASE-CR4, the lanes are AC-coupled. The AC-coupling shall be within the cable assembly. It is recommended that it is within the plug connectors. It should be noted that there may be various methods for AC-coupling in actual implementations. The low-frequency 3 dB cutoff of the AC-coupling shall be less than 50 kHz. It is recommended that the value of the coupling capacitors be 100 nF. The capacitor limits the inrush charge and baseline wander."

In the sentence Page 225 line 5 and 6, change the reference to 136.11 and delete "plug connectors".

In PICS item CA9, change the reference from 136.12 to 136.11.

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Cl 136C SC 136C.1 P387 L41 # i-143
 Dawe, Piers J G Mellanox Technologies

Comment Type T Comment Status A AC-coupling

The paragraph about AC coupling, which should be a property of and requirement on the cable not the MDI, is in the wrong place. The subclause reference in PICS CA9 is wrong.

SuggestedRemedy

Move this paragraph to 136.11 just before 136.11.1 (older clauses have it in the equivalent of 136.12, which is not really correct but at least it's in the clause). Update the subclause reference in PICS CA9.

Response Response Status C

ACCEPT IN PRINCIPLE.

Resolve using the response to comment i-160.

[Editor's note: For reference, the response to comment i-160 is copied here:

ACCEPT IN PRINCIPLE.

Delete paragraph P387, L41.

Insert paragraph in 136.11, at P233, L42:
 "For 50GBASE-CR, 100GBASE-CR2, and 200GBASE-CR4, the lanes are AC-coupled. The AC-coupling shall be within the cable assembly. It is recommended that it is within the plug connectors. It should be noted that there may be various methods for AC-coupling in actual implementations. The low-frequency 3 dB cutoff of the AC-coupling shall be less than 50 kHz. It is recommended that the value of the coupling capacitors be 100 nF. The capacitor limits the inrush charge and baseline wander."

In the sentence Page 225 line 5 and 6, change the reference to 136.11 and delete "plug connectors".

In PICS item CA9, change the reference from 136.12 to 136.11.

]

Cl 137 SC 137.9.2 P251 L22 # i-106
 Healey, Adam Broadcom Ltd.

Comment Type TR Comment Status A Tx electrical

The jitter requirements at TP2 are identical to the jitter requirements at TP0a. It seems that the uncorrelated jitter allowances should be larger at TP2 to account for a) the reduction in the slope of the waveform due to channel loss combined with b) the addition of noise in the form connector crosstalk. A similar concern was raised during the IEEE P802.3bj/D3.1 ballot (see comment r01-44 in <http://www.ieee802.org/3/bj/comments/P8023bj-D3p1-Comments_Final_byID.pdf>). See also <http://www.ieee802.org/3/bj/public/mar14/healey_3bj_03_0314.pdf>. No change was made to the IEEE P802.3bj draft because all lanes (the lane under test and aggressors) transmit the same test pattern (PRBS9). This was due to limitations on the configuration of the test pattern generators. It was postulated that crosstalk from PRBS9 aggressors would appear as correlated interference and show up in the SNDR results (as linear fit error) and not in uncorrelated noise/jitter results. However, the Clause 120 test pattern generator definition allows the PRBS13Q pattern to be sent only on the lane under test while aggressors send PRBS31Q (or a valid xxxBASE-R signal). For this case, it seems connector crosstalk will appear in uncorrelated jitter measurements and an increase in the TP2 jitter allowance (relative to TP0a) is warranted.

SuggestedRemedy

Increase uncorrelated jitter limits at TP2 to account for connector crosstalk. While there may be concerns that this would allow lower quality transmitters with low loss/noise host channels, one can always point to 136A.2 as a statement that such transmitters are still not allowed. This is expected to have no impact on channel compliance since the COM parameters are based on TP0/TP0a requirements.

Response Response Status C

ACCEPT IN PRINCIPLE.

Based on the comment, we are assuming that the commenter was referring to 136.9.3, not 137.9.2.

http://www.ieee802.org/3/cd/public/Jan18/healey_3cd_01_0118.pdf was reviewed.

Per comment i-140, J4u was changed to J3u with a value of 0.106 at TP0a, therefore the suggested remedy has to be modified accordingly

The increase in J3u from TP0a to TP2 based on the analysis in the presentation is 0.009 UI.

In Table 136-11, change from J4u with value 0.118 to J3u with value 0.115, and add a reference to the new subclause added by comment i-140. Add a footnote to the output jitter row with the text:

"J4u, JRMS, and Even-odd jitter measurements are made with a single transmit equalizer setting selected to compensate for the loss of the host channel".

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CI 137 SC 137.9.2 P251 L23 # i-136
 Dawe, Piers J G Mellanox Technologies

Comment Type TR Comment Status A ERL

Now that COM is defined with a near-neutral termination and package impedance, we don't expect transmitter return loss to align to the COM model any more. This RL is much tighter than CEI-56G-LR-PAM4 at low (and high) frequency (although apparently looser between 4 and 9 GHz). At low frequencies it is tighter than the channel RL, which seems back to front. The effect of (good) RL at low frequency is much less than the less good RL at higher frequencies anyway, and there is less concern about end-to-end reflections at higher frequencies than in C2C because the loss is higher when the receiver is challenged. So we can go back to what we had a few drafts ago, or go forward to something like ERL.

SuggestedRemedy

Either: Insert a new first item in the list of exceptions to Table 120D-1, create a new equation for Tx RL that is similar to the CI.93 and the channel RL at low frequencies; $12 - 0.625f$, $8.7 - 0.075f$. Add figure to illustrate.

Or: change to an ERL spec or similar for the transmitter. Same Nb set to 12.

Response Response Status U

ACCEPT IN PRINCIPLE.

Implement the changes according to http://www.ieee802.org/3/cd/public/Jan18/ran_3cd_01_0118.pdf.

CI 137 SC 137.9.2 P251 L28 # i-71
 Mellitz, Richard Samtec, Inc.

Comment Type TR Comment Status A ERL

Comments and supporting presentations in prior drafts reported difficulty making SNDR and SNR_ISI measurements. SNR_ISI is a small difference of large numbers. Thus, is somewhat problematic. Return loss is a measurement of reflections. However, return loss does not comprehend a DFE and SNR_ISI does. Re-Reflection was also not considered in SNR_ISI. Loss is a part of a return loss measurement making a short package look much worse than a long package. However, on the average short packages may perform better a performance limits. (approximately 3 to 3.5 dB of COM).

SuggestedRemedy

ERL is a direct measure of pertinent reflections in the context of package loss and a DFE, plus allowing for a specific budgeted amount of channel reflection derived from channel ERL. Remove item 3 in exception list. Add exception item indicating that in Table 120D-1 "differential output return loss (min)" is replaced with ERL (min) which shall be greater than 16.2 dB using $\beta_x = 10.7e9$, and $\rho_x = 0.318$, PTDR $T_r = 18.9ps$, and N_b is set by this clause. Also add annex 137A describing ERL computation. See presentation on implementation.

Response Response Status C

ACCEPT IN PRINCIPLE.

Implement the changes according to http://www.ieee802.org/3/cd/public/Jan18/ran_3cd_01_0118.pdf.

CI 137 SC 137.9.2 P251 L28 # i-137
 Dawe, Piers J G Mellanox Technologies

Comment Type TR Comment Status A ERL

Transmitter output residual ISI, SNR_ISI (min) 36.8 dB (Clause 136) and 43 dB (Clause 137) is still too high - can barely measure the IC through the test fixture. The warning NOTE in 120D.3.1.7 (where it's "only" 34.8 dB) shows the issue, but doesn't solve it. D2.0 comment 140, D21. comment 49.

SuggestedRemedy

Change to ERL spec or similar for the transmitter. Same Nb set to 12. Delete the SNR_ISI spec.

Response Response Status U

ACCEPT IN PRINCIPLE.

Implement the changes according to http://www.ieee802.org/3/cd/public/Jan18/ran_3cd_01_0118.pdf.

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Cl 137 SC 137.9.2 P251 L29 # i-138
 Dawe, Piers J G Mellanox Technologies

Comment Type TR Comment Status R Tx electrical

Signal-to-noise-and-distortion ratio (min), increased to 33.3 dB (Clause 136) and to 32.5 dB (Clause 137) for all Tx emphasis settings, is still too high. D2.0 comment 139, D2.1 comment 50. It turns out that the SNDR method captures sort of "high frequency distortion" that is filtered out by a real channel and receiver 3fb/4 bandwidth (see 93A.1.4.1), partly unfiltered by the equalizer. So it should be measured in something less than ~19 GHz.

SuggestedRemedy

Add ", when sigma_e and sigma_n are found from signals observed with a fourth-order Bessel-Thomson low-pass response with 19.34 GHz 3 dB bandwidth. NOTE--pmax is found from a signal observed with a fourth-order Bessel-Thomson low-pass response with 33 GHz 3 dB bandwidth." If we wish, we can tweak the limit for pmax and measure it in the same 19.34 GHz, which would more correctly remove the harmonics from the measurement.

Response Response Status U

REJECT.

The sigma_TX term in COM is calculated under the assumption that the spectrum of the noise and the distortion is identical to the spectrum of the ideal signal at the transmitter output (sinc shaped per Eq. 93A-23). If that is the case, the signal, noise and distortion all go through the same transfer function, which includes the transmitter, receiver, and channel (Eq. 93A-19).

The actual effect on the receiver depends on the Tx noise and distortion spectrum (if high frequencies dominate, sigma_tx is too high because they will be more attenuated by channel and Rx than the signal; if low frequencies dominate, sigma_tx is too low since they will be less attenuated).

The suggested remedy includes a specific new filter for noise and distortion measurement but there is insufficient evidence that this filter is more suitable than the current filter.

Cl 137 SC 137.9.2 P251 L29 # i-105
 Healey, Adam Broadcom Ltd.

Comment Type TR Comment Status A Tx electrical

The minimum SNDR at TP2 (subject to confirmation per the editor's note) is 33.3 dB. However, in 136A.2 it is stated that "the transmitter characteristics at TP0 are constrained at TP0a by 137.9.2" and 137.9.2 sets the minimum SNDR at TP0a at 32.5 dB. Is it a reasonable expectation for the SNDR at TP2 to be better than the SNDR at TP0a? Comparing 100GBASE-CR4 to 100GBASE-KR4 (and 25GBASE-CR to 25GBASE-KR), the minimum SNDR at TP2 is 1 dB lower than the minimum SNDR at TP0a. This seems to make more sense since, while some noise and distortion observed at TP0a will be attenuated by the host channel, the numerator of the SNDR equation (linear fit pulse peak) is also reduced and the crosstalk of the host connector is an additional noise source. While there may be concerns that this would allow lower quality transmitters with low loss host channels, one can always point to 136A.2 as a statement that such transmitters are still not allowed. Finally, this is expected to have no impact on channel compliance since the COM parameters are based on TP0/TP0a requirements.

SuggestedRemedy

Set the "confirmed" minimum SNDR at TP2 to be less than the minimum SNDR at TP0a. A margin of 1 dB is suggested based on the margin allocated for 100GBASE-CR4 and 25GBASE-CR.

Response Response Status C

ACCEPT IN PRINCIPLE.

Resolve using the response to comment i-161.

[Editor's note: For reference, the response to comment i-161 is copied here:

ACCEPT IN PRINCIPLE.

http://www.ieee802.org/3/cd/public/Jan18/dudek_3cd_01_0118.pdf was reviewed.

Straw poll ET-2:

For 3rd bullet in slide 10 of dudek_3cd_01_0118

- A. Accept as is
- B. Accept changing sndr to 32.2 dB
- C. Do not accept the changes

Chicago rules:

- A: 13
- B: 19
- C: 0

Straw poll ET-3

For "COM parameters" and "COM pass/fail criteria" in slide 10 of dudek_3cd_01_0118

- A. Accept all changes in both
- B. Accept only the changes in "COM parameters"
- C. Accept only the first four sub-bullets in "COM parameters" (Rd, Zc of package, Av/Afe,

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Ane), do not change the Zc for the PCB
 D. Do not accept any of the changes
 Chicago rules
 A: 4, B: 14, C: 17, D: 3

Straw poll ET-4

For "COM parameters" in slide 10 of dudek_3cd_01_0118
 A. Accept all sub-bullets
 B. Accept only the first four sub-bullets (Rd, Zc of package, Av/Afe, Ane), do not change the Zc for the PCB
 Choose one
 A: 12, B: 12
 Second count
 A: 12, B: 10

Straw poll ET-5

For COM pass/fail criterion of cable test in slide 10 of dudek_01
 A. Change from 3.0 dB to 3.3 dB
 B. Change from 3.0 dB to 3.2 dB
 C. Change from 3.0 dB to 3.1 dB
 D. No change
 Chicago rules
 A: 7, B: 8, C: 9, D: 13

Implement the changes in slide 10 of dudek_3cd_01_0118 except for:
 1. No change to "COM pass/fail criterion"
 2. SNDR=32.2 dB instead of 32 dB

]

Cl 137	SC 137.9.2	P251	L30	# i-140
Dawe, Piers J G		Mellanox Technologies		

Comment Type	TR	Comment Status	A	Tx electrical
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This clause with a BER of 2.4e-4 needs a J3u spec, just as 120D with a BER of 1e-5 uses J4u. Using J3u enables a shorter measurement as well as a more relevant, accurate one. The J3u value can be found using eq 136-7 and 136-8 to convert Table 120D1's J_rms and J4u to A_DD and sigma_RJ, then used again with Q3 instead of Q4 to find J_rms (same as original) and J3u.

Suggested Remedy

Add exception 5: the J4u limit in Table 120E-1 does not apply but the maximum J3u is 0.106 UI.

In Eq 136-7 and 136-8 and the NOTE, change J4u to J3u, Q4=3.8906 to Q3=3.2905, Q(Q3) = 5 x 10^-4.

Jrms and its value don't change.

If wished, add an informative NOTE in 137.9.2 saying that the J3u limit here is consistent with the J4u limit in Table 120D-1.

Add a new subclause:

136.9.3.n J3u Jitter

J3u is defined similarly to J4u (see 120D.3.1.8). J3u is defined as the time interval that includes all but 10^-3 of fJ(t), from the 0.05th to the 99.95th percentile of fJ(t).

Response	Response Status	C
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ACCEPT IN PRINCIPLE.

The informative note in the suggested remedy is correct only in case the jitter distribution matches the dual-Dirac model exactly (with A_DD=0.02 UI and Sigma_RJ=0.01 UI). It is not true in general, and real transmitters may meet one specification and fail another.

In 137.9.2, add exception 5: the J4u limit in Table 120E-1 does not apply but the maximum J3u is 0.106 UI.

In Eq 136-7 and 136-8 and the NOTE, change J4u to J3u, Q4=3.8906 to Q3=3.2905, Q(Q3) = 5 x 10^-4.

Jrms and it value don't change.

Add a new subclause:

136.9.3.n J3u Jitter

J3u is defined similarly to J4u (see 120D.3.1.8). J3u is defined as the time interval that includes all but 10^-3 of fJ(t), from the 0.05th to the 99.95th percentile of fJ(t).

The informative note in the suggested remedy is correct only in case the jitter distribution matches the dual-Dirac model exactly (with A_DD=0.02 UI and Sigma_RJ=0.01 UI). It is not true in general, and real transmitters may meet one specification and fail another. Therefore it will not be added.

Implement with editorial license.

IEEE P802.3cd 50 Gb/s, 100 Gb/s, 200 Gb/s Ethernet Initial Sponsor ballot comments

CI 137 SC 137.9.3 P251 L35 # i-141
 Dawe, Piers J G Mellanox Technologies

Comment Type TR Comment Status A ERL

Now that COM is defined with a near-neutral termination and package impedance, receiver mismatch is the receiver designer's concern, not the standard's, unless it is very extreme, because the receiver interference tolerance test finds its effect combined with other receiver attributes. And we don't expect receiver return loss to align to the COM model any more. This RL is much tighter than CEI-56G-LR-PAM4 at low (and high) frequency (although apparently looser between 4 and 9 GHz). At low frequencies it is tighter than the channel RL, which is the wrong way round. The effect of (good) RL at low frequency is much less than the less good RL at higher frequencies anyway. So we can go back to what we had a few drafts ago, or go forward to something like ERL.

SuggestedRemedy

Either: Insert a new first item in the list of exceptions to Table 120D-5, create a new equation for Rx RL that is similar to the Cl.93 and the channel RL at low frequencies; 12 -0.625f, 8.7-0.075f. Add figure to illustrate or point to the figure for Tx RL (see another comment).
 Or: change to an ERL spec or similar for the receiver. I think it can be more lenient than the transmitter spec because we have the receiver interference tolerance test.

Response Response Status U

ACCEPT IN PRINCIPLE.

Implement the changes according to
http://www.ieee802.org/3/cd/public/Jan18/ran_3cd_01_0118.pdf.

CI 137 SC 137.9.3 P251 L43 # i-72
 Mellitz, Richard Samtec, Inc.

Comment Type TR Comment Status A ERL

Clause 137.9.3 specifies return loss pointing to Table 120D-5. Return loss is a measurement of reflections. There is no direct tie-in to channel return loss. However, return loss does not comprehend a DFE and insertion loss as a part of a return loss measurement making a short package look much worse than a long package. However, on the average short packages may perform better a performance limits. (approximately 3 to 3.5 dB of COM).

SuggestedRemedy

ERL is a direct measure of pertinent reflections in the context of package loss and a DFE, plus allowing for a specific budgeted amount of channel reflection derived from channel ERL. Add exception item indicating that in Table 120D-5 "differential input return loss (min)" is replaced with ERL (min) which shall be greater than 16.2 dB using beta_x=10.7e9, and rho_x=0.318, PTDR T_r=18.9ps, and N_b is set by this clause. Also add annex 137A describing ERL computation. See presentation on implementation.

Response Response Status C

ACCEPT IN PRINCIPLE.

Implement the changes according to
http://www.ieee802.org/3/cd/public/Jan18/ran_3cd_01_0118.pdf.

CI 137 SC 137.10 P251 L49 # i-31
 RAN, ADEE Intel Corporation

Comment Type T Comment Status A beta

Following the updates in the revision project (as of 802.3cj D3.0), the correction term beta is not needed any more.

SuggestedRemedy

Delete "and \beta is 2".

Response Response Status C

ACCEPT IN PRINCIPLE.

Resolve using the response to comment i-100.

[Editor's note: For reference, the response to comment i-100 is "ACCEPT" and the suggested remedy is copied here:
 "Remove the phrase "and <beta> is 2" at line 50 here and in 137.10 (p251, 149)."
]

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CI 137 SC 137.10.2 P253 L40 # i-73
Mellitz, Richard Samtec, Inc.

Comment Type TR Comment Status A ERL

Return loss has not been demonstrated to sufficiently limit COM variability. There is no clear relation between the DFE in the reference signaling architecture and portions of reflections which are re-reflected. Apparently, there is no clear tie-in between the input/output return loss and channel return loss. ERL addresses these reflections directly and provided a linkage to input/output return loss.

SuggestedRemedy

Rename clause 137.10.2 from "Return Loss" to "Effective Return Loss". Remove all the content of 137.10.2. Replace with: "The minimum effective return loss of the channel shall be greater than 10.2 dB only when COM is less than 4 dB computed using $\beta_x=10.7e9$, $\rho_x=0.15$, PTDR Tr=18.9ps, and N_b is set by this clause."

Response Response Status C

ACCEPT IN PRINCIPLE.

Implement the changes according to
http://www.ieee802.org/3/cd/public/Jan18/ran_3cd_01_0118.pdf.

CI 137 SC 137.12.3 P256 L40 # i-55
RAN, ADEE Intel Corporation

Comment Type E Comment Status A <bucket>

Large font size in "RS(544,514)".

SuggestedRemedy

Fix it.

Response Response Status C

ACCEPT.

CI 137 SC 137.12.4.3 P258 L47 # i-164
Dudek, Michael Cavium

Comment Type T Comment Status A <bucket>

Clause 137.9.1 contains an exception to 93.8.1.1. We should therefore refer to 137.9.1

SuggestedRemedy

Change 93.8.1.1 to 137.9.1

Response Response Status C

ACCEPT IN PRINCIPLE.

(accepting the suggested remedy)

In item TC1, change "subclause" from 93.8.1.1 to 137.9.1, adding internal cross-reference.

CI 137 SC 137.12.4.3 P258 L50 # i-56
RAN, ADEE Intel Corporation

Comment Type T Comment Status A <bucket>

Differential and common mode return loss are defined in Table 120D-1.

SuggestedRemedy

Change "value/comment" in TC3 and TC3 to "Per Table 120D-1".

Response Response Status C

ACCEPT IN PRINCIPLE.

Change "value/comment" in both TC3 and TC4 from "Meets equation constraints" to "Per Table 120D-1".

CI 137 SC 137.12.4.4 P259 L24 # i-165
Dudek, Michael Cavium

Comment Type T Comment Status A <bucket>

Clause 137.9.1 contains an exception to 93.8.2.1. We should therefore refer to 137.9.1

SuggestedRemedy

Change 93.8.2.1 to 137.9.1

Response Response Status C

ACCEPT IN PRINCIPLE.

(accepting the suggested remedy)

In item RC1, change "subclause" from 93.8.2.1 to 137.9.1, adding internal cross-reference.

CI 138 SC 138 P261 L1 # i-122
Dawe, Piers J G Mellanox Technologies

Comment Type TR Comment Status R

This clause has received next to no attention - it's still the baseline. It needs more (some) study.

SuggestedRemedy

Do the work. Show technical feasibility for the draft spec (after improvements). The alternative is to withdraw the clause, which would be a pity.

Response Response Status W

REJECT.

No change to document suggested.

The presentation http://www.ieee802.org/3/cd/public/Jan18/king_3cd_02_0118.pdf was reviewed and provides supporting evidence for the specification in Clause 138.

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Cl 138 SC 138.1 P263 L12 # i-57
 RAN, ADEE Intel Corporation

Comment Type E Comment Status R
 "The 50GBASE-SR, 100GBASE-SR2 and 200GBASE-SR4 sublayers provide point-to-point 50, 100, and 200 Gigabit Ethernet links over one, two, or four, pairs of multimode fiber, up to at least 100 m"

This text is oddly placed after the list of references. It repeats the text in P261 L9 (four paragraphs before) almost verbatim, except that the word "PMD" is replaced by the three specific PMD names, and the words "with a reach of" are omitted.

This repetition is unnecessary.

SuggestedRemedy

Delete the quoted text.

Response Response Status C

REJECT.

The first occurrence is in the opening paragraph describing the PMDs in clause 138; the 'repetition' may be helpful to the reader because it occurs in a later (3 pages later) part of the overview section which is describing, and adjacent to, the sublayer diagram.

Cl 138 SC 138.7.1 P272 L17 # i-119
 Dawe, Piers J G Mellanox Technologies

Comment Type TR Comment Status R
 A TDECQ limit of 4.9 seems very high, given that the same fibres and transmitter and receiver front-ends that should not be worse can do 100GBASE-SR4 (PAM2, almost the same signalling rate) without the FFE.

SuggestedRemedy

This needs more study. We should be able to use information from 802.3bm.

Response Response Status W

REJECT.

No change to document suggested.
 The issue caused by a TDECQ limit of 4.9 dB has not been clarified. There is precedence for this kind of transmitter quality metric to be higher in MMF specifications than in SMF specifications.

Cl 138 SC 138.8.2 P274 L18 # i-5
 Anslow, Peter Ciena Corporation

Comment Type T Comment Status A <bucket>
 Comments #128 and #130 against D2.0 of the 802.3 revision project removed TIA-455-127-A-2006 from the references section of the base standard. See:
<http://www.ieee802.org/3/cj/comments/P8023-D2p0-Comments-Final-byID.pdf#page=33>
 This comment proposes to make equivalent changes to the P802.3cd draft.

SuggestedRemedy

- In 138.8.2, delete "TIA/EIA-455-127-A or"
- In 138.11.4.4 OM2, delete "TIA/EIA-455-127-A or"
- In 139.7.2, and 140.7.2:
 change the subclause title to "Wavelength and side mode suppression ratio (SMSR)"
 in the text change "wavelength" to "wavelength and SMSR" and delete "TIA/EIA-455-127-A or"
- In Table 139-10: replace the em-dash with a cross-reference to subclause 139.7.2
- In Table 140-10: replace the em-dash with a cross-reference to subclause 140.7.2
- In 139.11.4.5 OM2 and 140.11.4.4 OM2:
 change "Center wavelength" to "Center wavelength and SMSR"
 delete "TIA/EIA-455-127-A or"

Response Response Status C

ACCEPT.

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Cl 138 SC 138.8.5 P274 L31 # i-79
Liu, Hai-Feng Intel Corporation

Comment Type TR Comment Status R

The sub-eye threshold levels in current TDECQ measurement are determined by the OMAouter and the average optical power of the PAM4 eye diagram (Pave) as defined in equations (121-1), (121-2) and (121-3). While this is good for perfectly linear PAM4 signals with 3 equal eye amplitudes, it would lead to pessimistic TDECQ values as compared to the link sensitivity penalty measurements where thresholds are adjusted by real receivers to achieve the lowest BER even if the signal is not perfectly linear.

Several vendors have contributed data (way_3bs_01a_0717, tamura_3bs_01a_0917, baveja_3cd_01_1117) showing many units that are able to close the link with good sensitivity/BER margin would fail to meet the maximum TDECQ specification, causing good transmitters to be failed.

SuggestedRemedy

Propose to adopt threshold optimization in TDECQ measurement as described in mazzini_120617_3cd_adhoc-v2 with the additional constraints on the allowable adjustment range.

Detailed presentation to be submitted for the January meeting with the summary of the proposal, measurement data to support the proposal, and suggested changes in details.

Response Response Status U

REJECT.

The presentation http://www.ieee802.org/3/cd/public/Jan18/liu_3cd_01a_0118.pdf was reviewed.

It does not provide sufficient details to implement.

It is not clear that the suggested remedy would be an improvement to the draft.

Also http://www.ieee802.org/3/cd/public/Jan18/king_3cd_01_0118.pdf was presented in support of the adequacy of the current specification.

Cl 138 SC 138.8.5 P274 L39 # i-116
Dawe, Piers J G Mellanox Technologies

Comment Type TR Comment Status R

It seems that it is possible to make a bad transmitter (e.g. with a noisy or distorted signal), use emphasis to get it to pass the TDECQ test, yet leave a realistic, compliant receiver with an unreasonable challenge, such as high peak power, high crest factor, or a need to remove emphasis from the signal, contrary to what equalizers are primarily intended to do. Note the receiver is tested for a very slow signal only, not for any of these abusive signals. This is an issue for all the PAM4 optical PMDs, although it may be worse for MMF because of the high TDECQ limit.

SuggestedRemedy

1. To screen for noisy or distorted signals with heavy emphasis
Define $TDECQ_{rms} = 10 \cdot \log_{10}(A_{RMS}/(s^3 \cdot Q_t \cdot R))$ where A_{RMS} is the standard deviation of the measured signal after the 13.28125 GHz filter response, Q_t and R are as already in Eq 212-12. s is the standard deviation of a fast clean signal with OMA=2 and without emphasis, observed through the 13.28125 GHz filter response (around 0.7). Set limit for $TDECQ_{rms}$ according to what level of dirty-but-emphasised signal we decide is acceptable, add max $TDECQ_{rms}$ row to each transmitter table. Alternatively, if the same relative limit is acceptable for all PAM4 optical PMDs, the limit could be here in the TDECQ procedure. Similarly in clauses 139, 140.
2. To protect the TIA input, consider a peak power spec as in Clause 86.
3. To protect the TIA and any AGC and TIA from unreasonable signals, consider a crest factor spec.
4. To protect the receiver from having to "invert" heavily over-emphasised signals, set a minimum cursor weight.
To protect the equalizer from having to support unnecessary settings for waveforms that can't or shouldn't ever happen, constrain the cursor position - see other comments .

Response Response Status W

REJECT.

The need for additional transmitter specs has not been established, and insufficient evidence has been provided that the proposed remedy fixes the claimed problem.

A contribution is invited that demonstrates the problem (a waveform that passes TDECQ but cannot be decoded by a reasonable receiver implementation) and that the proposed additional requirement prevents this issue from occurring. A similar proposal to create a $TDECQ_{rms}$ spec was suggested in comment #02-35 against 802.3bs D3.2, which was similarly rejected.

A peak power spec has not been shown to be necessary, and a definition and value has not been provided.

A crest factor limit has not been shown to be necessary, and a definition and value has not been provided.

The need for a limit to cursor weight has not been established.

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Cl 138 SC 138.8.5.1 P274 L51 # i-120
 Dawe, Piers J G Mellanox Technologies

Comment Type TR Comment Status A

Excluding scenarios that won't happen will pave the way to more efficient receivers (see another comment). A worst signal will involve a slow transmitter (not "anti-causal") and modal dispersion that might appear anti-causal but is contained by the launch and fibre specs, and the receiver (near to neutral). The combination won't be very strongly "anti-causal".
 TR because it may take us a while to find enough evidence on what might/won't happen with a range of fibres.

SuggestedRemedy

Add "The reference equalizer shall not use more than two? three? pre-cursor taps." Define pre-cursor. Or the taps could be numbered and this rule expressed in terms of the cursor position.

Response Response Status W

ACCEPT IN PRINCIPLE.

See resolution to comment i-107

[Editor's note: For reference, the response to comment i-107 is copied here:

ACCEPT IN PRINCIPLE.

Implement the changes proposed in
http://www.ieee802.org/3/cd/public/Jan18/king_3cd_03_0118.pdf with editorial license

]

Cl 138 SC 138.8.5.1 P274 L54 # i-95
 Kirkland, William

Comment Type T Comment Status R

I believe that the following "NOTE" in the TDECQ reference equalizer is NOT true, especially since there is no requirement on the reference tap location. NOTE--This reference equalizer is part of the TDECQ test and does not imply any particular receiver implementation. Not specifying the reference location clearly allows the system to favour both response with significant pre-cursors or post cursors. The use of FFE in this way precludes the use of a CTLE.

SuggestedRemedy

Remove the note. I suspect most people understand the implications on a 5 T t-spaced equalizer.

Response Response Status C

REJECT.

The NOTE is correct. The FFE reference equalizer does not preclude use of a CTLE in an implementation, but a CTLE equalizer is probably not a good choice for MMF links (where ~ 50% of all links will have anti-causal impulse responses) or SMF links where chirp and chromatic dispersion can cause asymmetric pulse distortion.

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CI 138 SC 138.8.8 P275 L16 # i-58
 RAN, ADEE Intel Corporation

Comment Type TR Comment Status R

The SRS methodology in 121.8.9.1 and 121.8.9.3 has several flaws that need to be addressed:

- Half of the SECQ should be obtained without noise or jitter, using the combination of low-pass filter and E/O converter (which is marked as "Tunable" in Figure 139-5, and also in Figure 122-5, but not in Figure 121-6). Different E/O converters that may be used in the test setup may have different characteristics (noise and BW), which will result in very different setting for the low-pass filter. This freedom enables very different test conditions, some of which may be favorable for some devices.

- The remaining SECQ is met by adjusting the Gaussian noise (with unspecified power), sinusoidal interferer amplitude (with unspecified amplitude and frequency), and low-pass filter (with no specified limits); the sinusoidal jitter stress (which is specified) also affects SECQ. There are too many degrees of freedom here, which again enable very different test conditions (as demonstrated in http://www.ieee802.org/3/cd/public/Nov17/chang_3cd_01_1117.pdf).

- The effect of sinusoidal jitter on SECQ measurement is difficult to predict, since the measurement is done with a CRU (which tracks all frequencies to some extent). Also, the pattern used for calibration is very short and the length captured is not specified (e.g. no requirement to measure at least a full cycle of the sinusoidal jitter, which may be much longer than the test pattern). This may result in repeatability problems.

The too many degrees of freedom need to be limited, ideally to one knob that has to be turned to reach the required SECQ. This is the motivation for the proposed change.

Also applies to 139.7.9 and 140.7.9.

SuggestedRemedy

Add exceptions or additions to the methods of 121.8.9.1 and 121.8.9.3 including the following:

1. Specify the combined bandwidth of the E/O and the low-pass filter (without equalization), e.g. -3 dB at 15 GHz (or an agreed upon value). This may be measured using a different transmitter (e.g. sinusoidal generator). This step is prior to any SECQ measurement
2. Specify that the target SECQ is achieved by addition of Gaussian noise only (without sinusoidal interference), this will be the knob to turn to achieve the SECQ.
3. Specify that SECQ is calibrated once before addition of sinusoidal jitter, and calibration is not repeated for every jitter frequency. (If necessary, reduce SECQ target to accommodate for expected jitter effect).

Implement the chosen solution (with different bandwidth and SECQ targets) also in 139.7.9 and 140.7.9.

Response REJECT. Response Status W

It has not been demonstrated that there is a problem with the draft, nor has it been demonstrated that the proposed remedy fixes it.

The work presented in http://www.ieee802.org/3/cd/public/Nov17/chang_3cd_01_1117.pdf showed good correlation between SECQ and Rx sensitivity and the freedom to set up the SRS stress was explored quite thoroughly.

The freedom to set up the SRS test source is a balance between pragmatism and precision; the SECQ test metric ensures that the penalty (for the reference equalizer) of the induced stresses for different test source set-ups, is identical.

[Editor's note: Comments i-82, i-83 and i-84 address a similar issue.]

CI 138 SC 138.8.8 P275 L28 # i-93
 Kirkland, William

Comment Type T Comment Status R

Again, the use of approximately with an excessive amount of significant figures. "approximately 13.28125 GHz". Just how close does one have to be to satisfy this requirement?. This occurs in TDECQ sections as well.

SuggestedRemedy

one half the baud rate, or x times the baud rate. If there is give or take, then there should be a +/- accuracy spec., I suspect 13.3 GHz is sufficient.

Response REJECT. Response Status C

The current text refers back to subclause 121.8.5.1 which describes the combined O/E and oscilloscope bandwidth to be "approximately 13.28125 GHz." It also goes on to say that "Compensation may be made for any deviation from an ideal fourth-order Bessel-Thomson response." Deviation from a BT4 bandwidth of 13.28125 GHz introduces a measurement difference, which may be compensated for. It is left to the implementer to decide the trade-off between bandwidth accuracy vs the degree of compensation that would be required.

The intent is that the measurement definition should describe an exact reference receiver bandwidth which can be implemented using a combination of inexact components and compensation techniques.

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Cl 138 SC 138.10 P277 L13 # i-59
 RAN, ADEE Intel Corporation
 Comment Type E Comment Status A <bucket>
 Paragraph is not justified (i.e. it is aligned left).
 SuggestedRemedy
 Format as regular clause text.
 Response Response Status C
 ACCEPT.

Cl 139 SC 139.6.1 P292 L49 # i-22
 Anslow, Peter Ciena Corporation
 Comment Type T Comment Status A
 There are errors in P802.3bs D3.5 in Table 122-9, 122-10, and Table 122-16 that have propagated through to the P802.3cd draft.
 For IEEE 802.3 single-mode optical PMD clauses, the optical return loss of the transmitter compliance channel usually matches the Optical return loss tolerance (max) value in the transmit characteristics table.
 Also, in the IEEE Std 802.3bs-2017 amendment, because of the increased sensitivity of the PAM4 modulation format to MPI, the Optical return loss tolerance (max) value was calculated from coherent addition of the worst case discrete reflectances allowed in the channel.
 For Clause 122 in draft D2.0 of P802.3bs, the values for 200GBASE-FR4 and 400GBASE-FR8 were 17.8 dB and those for 200GBASE-LR4 and 400GBASE-LR8 were 15.7 dB in both places. These values were correctly derived from one -26 dB reflectance from the receiver combined with 4 or 6 -35 dB reflectances in the channel for the FR or LR cases respectively. However, in D2.1 of P802.3bs a more complicated set of requirements for discrete reflectances in the channel were introduced. This allowed 10 x -40 dB reflections for FR and 10 x -38 dB reflections for LR. This changed the worst case combined reflection values to 16.5 dB and 15.1 dB for FR and LR respectively. Unfortunately, while the values in Table 122-9 and 122-10 were changed accordingly, the values in Table 122-16 were not. In D3.2 of P802.3bs a further small change was made to the maximum reflectances in the channel so that for FR the worst case was 10 x -41 dB reflections and for LR it was 8 x -37 dB reflections. See http://www.ieee802.org/3/bs/public/adhoc/smf/17_05_16/anslow_01_0517_smf.pdf This again changed the worst case combined reflection values, this time to 17.1 dB and 15.6 dB for FR and LR respectively. Unfortunately, none of the values in Table 122-9, 122-10, or Table 122-16 were changed accordingly and these errors were taken over into the P802.3cd draft.
 A comment has been submitted to the revision project to fix this in Table 122-9, Table 122-10, and Table 122-16.
 SuggestedRemedy
 In Table 139-6:
 change "RIN16.5OMA (max)" to "RIN17.1OMA (max)"
 change "RIN15.1OMA (max)" to "RIN15.6OMA (max)"
 change the Optical return loss tolerance (max) values for FR and LR from 16.5 dB and 15.1 dB to 17.1 dB and 15.6 dB, respectively
 In Table 139-11:
 change the Optical return loss for 50GBASE-FR from 17.8 dB to 17.1 dB
 change the Optical return loss for 50GBASE-LR from 15.7 dB to 15.6 dB
 In 139.7.7:
 in the title change "(RIN16.5OMA and RIN15.1OMA)" to "(RIN17.1OMA and RIN15.6OMA)"
 in a) change "16.5 dB for 50GBASE-FR and 15.1 dB for 50GBASE-LR" to "17.1 dB for 50GBASE-FR and 15.6 dB for 50GBASE-LR"

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Response *Response Status* **C**
ACCEPT.

Cl **139** *SC* **139.7.5** *P296* *L20* # **i-80**
Liu, Hai-Feng Intel Corporation

Comment Type **TR** *Comment Status* **R**

The sub-eye threshold levels in current TDECQ measurement are determined by the OMAouter and the average optical power of the PAM4 eye diagram (Pave) as defined in equations (121-1), (121-2) and (121-3). While this is good for perfectly linear PAM4 signals with 3 equal eye amplitudes, it would lead to pessimistic TDECQ values as compared to the link sensitivity penalty measurements where thresholds are adjusted by real receivers to achieve the lowest BER even if the signal is not perfectly linear.
Several vendors have contributed data (way_3bs_01a_0717, tamura_3bs_01a_0917, baveja_3cd_01_1117) showing many units that are able to close the link with good sensitivity/BER margin would fail to meet the maximum TDECQ specification, causing good transmitters to be failed.

SuggestedRemedy

Propose to adopt threshold optimization in TDECQ measurement as described in mazzini_120617_3cd_adhoc-v2 with the additional constraints on the allowable adjustment range.
Detailed presentation to be submitted for the January meeting with the summary of the proposal, measurement data to support the proposal, and suggested changes in details.

Response *Response Status* **U**
REJECT.

See resolution to comment i-79

[Editor's note: For reference, the response to comment i-79 is copied here:

REJECT.

The presentation http://www.ieee802.org/3/cd/public/Jan18/liu_3cd_01a_0118.pdf was reviewed.
It does not provide sufficient details to implement.
It is not clear that the suggested remedy would be an improvement to the draft.
Also http://www.ieee802.org/3/cd/public/Jan18/king_3cd_01_0118.pdf was presented in support of the adequacy of the current specification.

]

Cl **139** *SC* **139.7.5.4** *P297* *L52* # **i-117**
Dawe, Piers J G Mellanox Technologies

Comment Type **TR** *Comment Status* **A**

An equalizing optical receiver has to search through and optimise many dimensions - this flexibility has a cost in design and test, and possibly time to start the link, power and sensitivity. Excluding scenarios that won't happen will pave the way to more efficient receivers in the future. It seems that an SMF signal that needs the equalizer could be slow, "causal" like an electrical signal, to "neutral" like a BT4 filter, to mildly anti-causal in appearance - maybe. But not strongly "anti-causal". We can make practical use of such knowledge (even if the search space would be different for a different PMD).
TR because it may take us a while to find enough evidence on what might/won't happen with a range of transmitter implementations.

SuggestedRemedy

Add "The reference equalizer shall not use more than two pre-cursor taps." Define pre-cursor. Or the taps could be numbered and this rule expressed in terms of the cursor position.

Response *Response Status* **W**

ACCEPT IN PRINCIPLE.

See resolution to comment i-107

[Editor's note: For reference, the response to comment i-107 is copied here:

ACCEPT IN PRINCIPLE.

Implement the changes proposed in http://www.ieee802.org/3/cd/public/Jan18/king_3cd_03_0118.pdf with editorial license

]

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Cl 139 SC 139.7.5.4 P297 L52 # i-107
 Sun, Junqing Credo Semiconductor

Comment Type T Comment Status A

5-tap T/2-spaced reference receiver has no more than 2 UI precursor coverage. Current reference equalizer with 5-tap T-spaced FFE allows up to 4 precursors. On one hand, a good system does not need so many precursors. On the other hand, supporting so many precursors may allow problematic transmitters to enter the market. This forces receivers to have high complexity and power to ensure interop. Given the fact that no more than 2 precursors are needed in the tests having been reported (e.g. mazzini_01a_0517_smf.pdf), the number of precursors shall be limited to no more than two.

SuggestedRemedy

Add a constraint on main tap location:

139.7.5.4 TDECQ reference equalizer
 The reference equalizer for 50GBASE-FR and 50GBASE-LR is a 5 tap, T spaced, feed-forward equalizer (FFE), where T is the symbol period. The sum of the equalizer tap coefficients is equal to 1. Main tap location shall not be higher than three.

Response Response Status C

ACCEPT IN PRINCIPLE.

Implement the changes proposed in
http://www.ieee802.org/3/cd/public/Jan18/king_3cd_03_0118.pdf with editorial license

Cl 139 SC 139.7.5.4 P298 L1 # i-94
 Kirkland, William

Comment Type T Comment Status R

I believe that the following "NOTE" in the TDECQ reference equalizer is NOT true, especially since there is no requirement on the reference tap location. NOTE--This reference equalizer is part of the TDECQ test and does not imply any particular receiver implementation. Not specifying the reference location clearly allows the system to favour both response with significant pre-cursors or post cursors. The use of FFE in this way precludes the use of a CTLE.

SuggestedRemedy

Remove the note. I suspect most people understand the implications on a 5 T t-spaced equalizer.

Response Response Status C

REJECT.

See resolution to comment i-95

[Editor's note: For reference, the response to comment i-95 is copied here:

REJECT.

The NOTE is correct. The FFE reference equalizer does not preclude use of a CTLE in an implementation, but a CTLE equalizer is probably not a good choice for MMF links (where ~ 50% of all links will have anti-causal impulse responses) or SMF links where chirp and chromatic dispersion can cause asymmetric pulse distortion.

]

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Cl 139 SC 139.7.9.1 P298 L45 # i-82
Liu, Hai-Feng Intel Corporation

Comment Type TR Comment Status R

PAM4 test results have shown (see chang_3cd_01_1117, particularly p. 20) that the composition and ratio of the stressors in the stressed receiver sensitivity test has a strong impact on link performance. In particular, the same SECQ can generate widely varying BER performance from the same receiver depending on whether the dominant stressor added to the bandwidth filtering was Gaussian noise or sinusoidal interferer. To address this we propose to more specifically prescribe the stressor ratio used to create the stressed Rx sensitivity conformance test input, to avoid understressing the receiver and causing interoperability issues.

SuggestedRemedy

In the second paragraph of section 139.7.9.1, after the existing sentence "The combination of the low-pass filter and the E/O converter should...", add the sentence "Of the remaining dB value of stressed eye closure (SECQ), at least half should be from the Gaussian noise stressor."

Response Response Status U

REJECT.

http://www.ieee802.org/3/cd/public/Nov17/chang_3cd_01_1117.pdf showed good correlation between SECQ and Rx sensitivity and the freedom to set up the SRS stress was explored quite thoroughly.

The freedom to set up the SRS test source is a balance between pragmatism and precision; the SECQ test metric ensures that the penalty (for the reference equalizer) of the induced stresses for different test source set-ups, is identical.

A late presentation http://www.ieee802.org/3/cd/public/Jan18/schube_3cd_01a_0118.pdf was reviewed also addressing the claimed problem. There was no consensus to make a change to the draft and further work was necessary to investigate the problem and provide a complete proposed remedy.

[Editor's note: Comment i-58 addresses a similar issue.]

Cl 139 SC 139.7.9.2 P299 L54 # i-83
Liu, Hai-Feng Intel Corporation

Comment Type TR Comment Status R

[note that a comment is needed in this section in addition to the comment above to avoid any confusion with the less clear instructions in the referenced 802.3bs section 121.8.9.2] PAM4 test results have shown (see chang_3cd_01_1117, particularly p. 20) that the composition and ratio of the stressors in the stressed receiver sensitivity test has a strong impact on link performance. In particular, the same SECQ can generate widely varying BER performance from the same receiver depending on whether the dominant stressor added to the bandwidth filtering was Gaussian noise or sinusoidal interferer. To address this we propose to more specifically prescribe the stressor ratio used, to avoid understressing the receiver and causing interoperability issues.

SuggestedRemedy

Add the following sentence to the end of section 139.7.9.2: "As outlined in section 139.7.9.1 above, half of the dB value of stressed eye closure (SECQ) should be from bandwidth limitations from the low-pass filter and E/O converter, while of the remaining dB value of stressed eye closure (SECQ), at least half should be from the Gaussian noise stressor."

Response Response Status U

REJECT.

See response to comment i-82

[Editor's note: For reference, the response to comment i-82 is copied here:

REJECT.

[Http://www.ieee802.org/3/cd/public/Nov17/chang_3cd_01_1117.pdf](http://www.ieee802.org/3/cd/public/Nov17/chang_3cd_01_1117.pdf) showed good correlation between SECQ and Rx sensitivity and the freedom to set up the SRS stress was explored quite thoroughly.

The freedom to set up the SRS test source is a balance between pragmatism and precision; the SECQ test metric ensures that the penalty (for the reference equalizer) of the induced stresses for different test source set-ups, is identical.

A late presentation http://www.ieee802.org/3/cd/public/Jan18/schube_3cd_01a_0118.pdf was reviewed also addressing the claimed problem. There was no consensus to make a change to the draft and further work was necessary to investigate the problem and provide a complete proposed remedy.

[Editor's note: Comment i-58 addresses a similar issue.]

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IEEE P802.3cd 50 Gb/s, 100 Gb/s, 200 Gb/s Ethernet Initial Sponsor ballot comments

Cl 140 SC 140.1 P309 L14 # i-85
 Maki, Jeffery Juniper Networks, Inc.

Comment Type **TR** Comment Status **R** jitter mismatch <cc>

Table 140-1 lists a variety of AUI options (e.g., CAUI-4 C2M, 100GAUI-4 C2M, 100GAUI-2 C2M) to build a PHY using a 100GBASE-DR PMD with no explicit regard to the potential mismatch of the output jitter of the AUI and the compliant output jitter of the 100GBASE-DR PMD.

SuggestedRemedy

Add text stating, "The PMA between the AUI and the PMD is responsible for adapting the output jitter of the chosen AUI option to meet the compliant output jitter of the 100GBASE-DR PMD."

Response Response Status **U**

REJECT.

There is no consensus to make the proposed change.

Cl 140 SC 140.1 P309 L33 # i-15
 Anslow, Peter Ciena Corporation

Comment Type **E** Comment Status **A** <bucket>

There are some items of text in Table 140-1 that should be cross-references.

SuggestedRemedy

Make the following into cross-references: on lines 33 to 38, "135D", "135E", "135F", "135G"

Response Response Status **C**

ACCEPT.

Cl 140 SC 140.3.2 P311 L39 # i-13
 Anslow, Peter Ciena Corporation

Comment Type **T** Comment Status **A**

Clause 140 defines the 100GBASE-DR PMD, so the skew constraints are those for a 100G PHY not a 50G PHY. Consequently, the cross-references in 140.3.2 should point to Clause 80 and Clause 83 rather than Clause 131 and Clause 135.

SuggestedRemedy

On line 39, change:

"Skew and Skew Variation are defined in 131.5 and specified at the points SP0 to SP7 shown in Figure 131-3." to:

"Skew and Skew Variation are defined in 80.5 and specified at the points SP0 to SP7 shown in Figure 80-8."

On line 43 change:

"Skew at SP2 is limited to 43 ns as defined by 135.5.3.5." to:

"Skew at SP2 is limited to 43 ns as defined by 83.5.3.4."

On page 312, line 1, change:

"For more information on Skew and Skew Variation, see 131.5." to:

"For more information on Skew and Skew Variation, see 80.5."

Response Response Status **C**

ACCEPT.

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Cl 140 SC 140.3.2 P311 L39 # i-127
 Dawe, Piers J G Mellanox Technologies

Comment Type E Comment Status A

Wrong reference: this is 100G, 131.5 is for 50G.

SuggestedRemedy

Change 131.5 to 80.5, twice. Change Figure 131-3 to Figure 80-8.

Response Response Status C

ACCEPT IN PRINCIPLE.

See response to comment i-13

[Editor's note: For reference, the response to comment i-13 was "ACCEPT" and the suggested remedy is copied here:

On line 39, change:

"Skew and Skew Variation are defined in 131.5 and specified at the points SP0 to SP7 shown in Figure 131-3." to:

"Skew and Skew Variation are defined in 80.5 and specified at the points SP0 to SP7 shown in Figure 80-8."

On line 43 change:

"Skew at SP2 is limited to 43 ns as defined by 135.5.3.5." to:

"Skew at SP2 is limited to 43 ns as defined by 83.5.3.4."

On page 312, line 1, change:

"For more information on Skew and Skew Variation, see 131.5." to:

"For more information on Skew and Skew Variation, see 80.5."

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Cl 140 SC 140.3.2 P311 L49 # i-125
 Dawe, Piers J G Mellanox Technologies

Comment Type TR Comment Status R Skew <cc>

The Skew at SP4 (the receiver MDI) has to be the same as the Skew at SP3 (the transmitter MDI) for this serial PMD.

SuggestedRemedy

Correct the numbers at SP4 and SP5. Correct Table 80-5, Summary of Skew constraints, at least for SP2-6, e.g. by using Table 131-5 (corrected) for 100G serial.

Response Response Status U

REJECT.

Resolve with the response to comment i-123.

[Editor's note: For reference, the response to comment i-123 is copied here:

REJECT.

The skew constraints for 100G in Table 80-5 and for 50G in Table 131-5 are consistent with the budget and methodology adopted by 802.3ba and 802.3bg and used in subsequent projects (e.g., 802.3bm, 802.3bs).

The skew constraints are established to ensure that the FEC/PCS skew tolerance is sufficient to support the worst case skew for any currently specified or potential (within reason) future PHY (e.g., 2-lane PMD for reach longer than 40 km). This is accomplished by having the same skew constraint at SP5 regardless of the PMD type.

The skew constraint at SP5 includes allocation for skew accumulated through the TX PMD (SP2 to SP3), the medium (SP3 to SP4), and the RX PMD (SP4 to SP5). Rather than specifying unique values for SP3, SP4, and SP5 based on PMD type, the adopted approach was to use the same numbers for all PMD types for consistency.

The approach described above is consistent for all PHY types defined by 802.3ba and subsequent projects. For instance, the medium skew accumulation (SP3 to SP4) of 80 ns was based on an 80 km multi-lane optical PMD. Nevertheless, the same value is used for other PMDs where the skew would be considerably lower (e.g., 100GBASE-SR4, 100GBASE-KR4, 100GBASE-CR4, etc.).

This specification methodology does not preclude an engineered implementation that optimizes the FEC/PCS skew buffering based on assumed lower PMD and medium skew accumulation. However, it should be noted that this implementation would not be compliant to 802.3cd.

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Cl 140 SC 140.6.2 P316 L42 # i-78
 Lewis, David Lumentum

Comment Type TR Comment Status A

Stressed receiver sensitivity (OMAAouter) (max) is measured with a single value of SECQ, 3.4 dB. Receivers tested are therefore verified to be compliant at worst case stress levels. However this is not sufficient because stressed sensitivity is supposed to improve linearly as the stress level (SECQ) is reduced from 3.4 dB down to 1.4 dB, at which point sensitivity needs to be better than -3.9 dBm. For very low stress signals, with SECQ between 0.9 and 1.4 dB, sensitivity can have the same value (-3.9 dBm) because compliant transmitters have OMA (min) of -0.8 dBm in this region. The concern is that a receiver can be designed to pass the current SRS test by having strong equalization for the impairments present in the SRS test signal, but at the same time may have high enough noise to not meet the sensitivity requirements at lower values of SECQ.

SuggestedRemedy

In Table 140-7:
 Change the value of Stressed receiver sensitivity (OMAAouter) (max) from -1.9 to "below the mask in Figure - XX"
 Delete the entry for Receiver sensitivity (OMAAouter) (max) and note c.
 Change the value of Stressed receiver sensitivity (OMAAouter) (max) from -1.9 to "below the mask in Figure - XX"
 Change the value of Stressed eye closure for PAM4 (SECQ) from 3.4 to "vary between 0.9 and 3.4"
 Add Figure - XX:

Response Response Status C

ACCEPT IN PRINCIPLE.

Implement the changes proposed in
http://www.ieee802.org/3/cd/public/Jan18/king_3cd_04_0118.pdf with editorial license in Clauses 138, 139 and 140.

Cl 140 SC 140.7.5 P319 L19 # i-108
 Sun, Junqing Credo Semiconductor

Comment Type TR Comment Status A

5-tap T/2-spaced reference receiver has no more than 2 UI precursor coverage. Current reference equalizer with 5-tap T-spaced FFE allows up to 4 precursors. A good system does not need so many precursors. Meanwhile supporting so many precursors may allow problematic transmitters to enter the market. This forces receivers to implement many precursors to ensure interop. Therefore receiver hardware complexity and power are increased, although these precursors are not needed for good systems. Given the fact that no more than 2 precursors are needed in the tests having been reported (e.g. mazzini_01a_0517_smf.pdf), the number of precursors shall be limited to no more than two.

SuggestedRemedy

Add one more exception:

Main tap location of the reference equalizer shall not be higher than three.

Response Response Status C

ACCEPT IN PRINCIPLE.

See resolution to comment i-107

[Editor's note: For reference, the response to comment i-107 is copied here:

ACCEPT IN PRINCIPLE.

Implement the changes proposed in
http://www.ieee802.org/3/cd/public/Jan18/king_3cd_03_0118.pdf with editorial license

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IEEE P802.3cd 50 Gb/s, 100 Gb/s, 200 Gb/s Ethernet Initial Sponsor ballot comments

CI 140 SC 140.7.5 P319 L19 # i-81
Liu, Hai-Feng Intel Corporation

Comment Type TR Comment Status R

The sub-eye threshold levels in current TDECQ measurement are determined by the OMAouter and the average optical power of the PAM4 eye diagram (Pave) as defined in equations (121-1), (121-2) and (121-3). While this is good for perfectly linear PAM4 signals with 3 equal eye amplitudes, it would lead to pessimistic TDECQ values as compared to the link sensitivity penalty measurements where thresholds are adjusted by real receivers to achieve the lowest BER even if the signal is not perfectly linear.

Several vendors have contributed data (way_3bs_01a_0717, tamura_3bs_01a_0917, baveja_3cd_01_1117) showing many units that are able to close the link with good sensitivity/BER margin would fail to meet the maximum TDECQ specification, causing good transmitters to be failed.

SuggestedRemedy

Propose to adopt threshold optimization in TDECQ measurement as described in mazzini_120617_3cd_adhoc-v2 with the additional constraints on the allowable adjustment range.

Detailed presentation to be submitted for the January meeting with the summary of the proposal, measurement data to support the proposal, and suggested changes in details.

Response Response Status U

REJECT.

See resolution to comment i-79

[Editor's note: For reference, the response to comment i-79 is copied here:

REJECT.

The presentation http://www.ieee802.org/3/cd/public/Jan18/liu_3cd_01a_0118.pdf was reviewed.

It does not provide sufficient details to implement.

It is not clear that the suggested remedy would be an improvement to the draft.

Also http://www.ieee802.org/3/cd/public/Jan18/king_3cd_01_0118.pdf was presented in support of the adequacy of the current specification.

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CI 140 SC 140.7.5 P319 L22 # i-121
Dawe, Piers J G Mellanox Technologies

Comment Type E Comment Status A

I don't think the reference equalizer as described in 121.8.5.4 is suitable because there, T the symbol period is twice what we need here.

SuggestedRemedy

Add text explaining that the symbol period T is not the same as in 121.8.5.4.

Response Response Status C

ACCEPT IN PRINCIPLE.

change:

"using a reference equalizer as described in 121.8.5.4"

to:

"using a reference equalizer as described in 121.8.5.4 where T is the symbol period for 100GBASE-DR"

CI 140 SC 140.7.5 P319 L23 # i-118
Dawe, Piers J G Mellanox Technologies

Comment Type TR Comment Status A

Excluding scenarios that won't happen will pave the way to more efficient receivers (see another comment). It seems that a 100 Gb/s/lane SMF signal that needs the equalizer will be slow (slower relative to the signalling rate than a 50 Gb/s/lane signal), and in the range of "causal" like an electrical signal, to "neutral" like a BT4 filter, to mildly anti-causal in appearance - maybe. But not so extremely lopsided that the a fourth postcursor would be better than a single precursor, nor strongly "anti-causal" the other way.

TR because it may take us a while to find enough evidence on what might/won't happen with a range of transmitter implementations.

SuggestedRemedy

Add "The reference equalizer shall use one or two pre-cursor taps." Define pre-cursor. Or the taps could be numbered and this rule expressed in terms of the cursor position.

Response Response Status W

ACCEPT IN PRINCIPLE.

See resolution to comment i-107

[Editor's note: For reference, the response to comment i-107 is copied here:

ACCEPT IN PRINCIPLE.

Implement the changes proposed in

http://www.ieee802.org/3/cd/public/Jan18/king_3cd_03_0118.pdf with editorial license

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Cl 140 SC 140.7.9 P320 L15 # i-84
Liu, Hai-Feng Intel Corporation

Comment Type TR Comment Status R

PAM4 test results have shown (see chang_3cd_01_1117, particularly p. 20) that the composition and ratio of the stressors in the stressed receiver sensitivity test has a strong impact on link performance. In particular, the same SECQ can generate widely varying BER performance from the same receiver depending on whether the dominant stressor added to the bandwidth filtering was Gaussian noise or sinusoidal interferer. To address this we propose to more specifically prescribe the stressor ratio used to create the stressed Rx sensitivity conformance test input, to avoid understressing the receiver and causing interoperability issues.

SuggestedRemedy

Add the following bullet to the end of section 140.7.9, "Of the remaining half of stressed eye closure (SECQ) that is not generated by bandwidth limitations from the low-pass filter and E/O converter, at least half of the remaining stress (in dB of SECQ) should be from the Gaussian noise stressor."

Response Response Status U

REJECT.

See resolution to comment i-82

[Editor's note: For reference, the response to comment i-82 is copied here:

REJECT.

[Http://www.ieee802.org/3/cd/public/Nov17/chang_3cd_01_1117.pdf](http://www.ieee802.org/3/cd/public/Nov17/chang_3cd_01_1117.pdf) showed good correlation between SECQ and Rx sensitivity and the freedom to set up the SRS stress was explored quite thoroughly.

The freedom to set up the SRS test source is a balance between pragmatism and precision; the SECQ test metric ensures that the penalty (for the reference equalizer) of the induced stresses for different test source set-ups, is identical.

A late presentation http://www.ieee802.org/3/cd/public/Jan18/schube_3cd_01a_0118.pdf was reviewed also addressing the claimed problem. There was no consensus to make a change to the draft and further work was necessary to investigate the problem and provide a complete proposed remedy.

[Editor's note: Comment i-58 addresses a similar issue.]

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