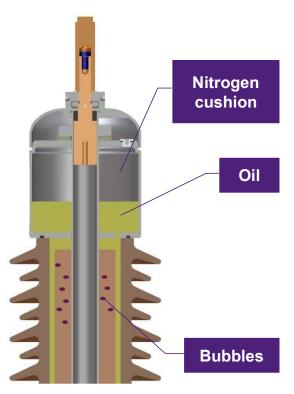


# "Bushing Cooldown Partial Discharge Test"

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## Gas Bubble Evolution in the oil of OIP Bushings



- Gas Bubble Evolution is a known phenomenon that can appear in oil impregnated paper bushings (OIP) of all manufacturers.
- The nitrogen from the Nitrogen Cushion dissolves partially in the oil of the bushing until an equilibrium is reached. When the bushing is heated, the temperature and pressure inside the bushing increase, leading to more nitrogen absorption and a higher gas saturation level. When the bushing cools down, the gas saturation level reduces. At this stage oversaturation of the oil with gas can occur and gas bubbles can be released to the oil.
- Gas bubble generation can occur during transformer testing (heat run test followed by cool down of the transformer and bushing). Subsequent electrical tests can lead to PD in the bushing and failure during the dielectric tests.
- Gas bubble generation can also occur in operation as the result of rapidly cooldown of a bushing or due to cyclic loading with/without cyclic variation of ambient temperature and solar radiation ⇒ Sustained PD activity inside the bushing shall be avoided in operation.

Proposal: Define a test procedure which allows to identify if a bushing design tends to produce partial discharge activity due to nitrogen bubbles during the FAT of the transformer.

The test conditions shall be severe enough to avoid sustained partial discharges under service conditions.

## Test Principles for the "Bushing Cooldown Partial Discharge Test"

#### Principle:

- 1. Put the bushing at a temperature rise to ambient which covers transformer-FAT and operating conditions
- 2. Wait until the oil of the bushing is saturated with nitrogen
- 3. Let the bushing cool down at the ambient temperature to create oversaturation of the bushing oil with nitrogen
- 4. Perform electrical tests of the bushing with measurement of PD activity

#### Comments:

- Point 1 can be achieved by installing the bushing on a heated oil vessel in a room with controlled temperature.
  However, for practical reasons it is easier to heat the complete bushing in an oven. This will reduce the time to reach saturation, and ensure a steeper temperature drop of the bushing. Nitrogen saturation can be indirectly monitored by measuring the pressure inside the bushing: a stabilization of pressure corresponds to a stabilization of nitrogen transfer between gas cushion and oil.
- Depending on the design, size, geometry and temperature of the bushing, the time constant for nitrogen
  dissolution into the oil can be in the range of several days. 99% saturation could potentially take several weeks.
   Prior storage of the bushing at ambient temperature for a longer time may help to reduce the heating time.
- To account for geometrical tolerances on components, the test should be performed on more than one sample. The proposal is to test 3 samples of a given design.

## **Temperature Conditions for the Cooldown PD Test**

IEEE Std C57.12.00-2021

IEEE Standard for General requirements for Liquid-Immersed Distribution, Power, and Regulating Transformers

5.11.1.5 Liquid temperature rise

The insulating liquid temperature rise above ambient temperature shall not exceed 65 °C when measured near the top of the main tank.

IEEE Std C57.19.00-2004

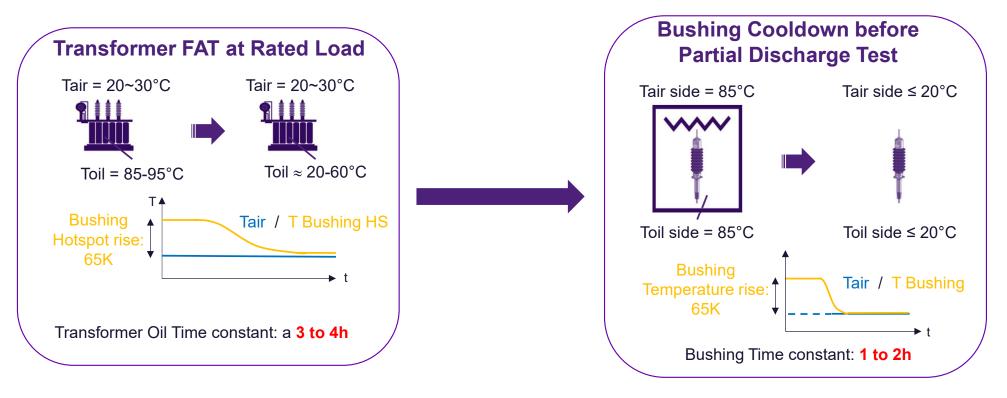
IEEE Standard General Requirements and Test Procedures for Power Apparatus Bushings

#### 5.4.1 Thermal basis of rating

The hottest-spot temperature rise above ambient air of any part of the bushing in contact with temperature index 105 insulation shall not exceed 75 K, when the inboard end is immersed in oil within 50 mm of the mounting flange with the oil having a rise of 65 K above the ambient air and the bushing is carrying rated current at rated frequency.

➤ The maximum Hotspot rise of a bushing on a transformer may not be achieved at the maximum load for an ONAN/ONAF cooled transformer. Therefore, the bushing hotspot rise may be in most cases lower than 75K, often in the range of 65K.

## **Temperature Conditions for the Cooldown PD Test**

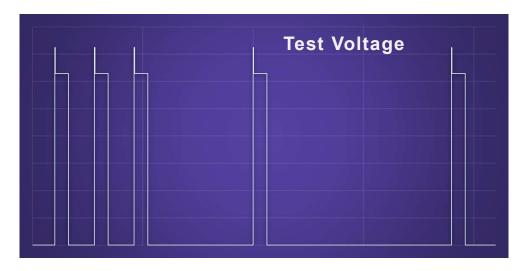


The conditions of the transformer FAT must be covered and overfulfilled during the bushing cooldown test:

- > Same temperature rise of the bushing against ambient as the bushing hotpot rise during the transformer FAT at Imax.
- > Assure saturation of the oil with nitrogen before cooldown.
- ➤ Cooldown-time to be shorter than the cooldown-time time on the transformer during FAT to compensate the higher N2 saturation during possible overloads during FAT and in service.

## **Proposed Test Procedure for the Cooldown PD Test**

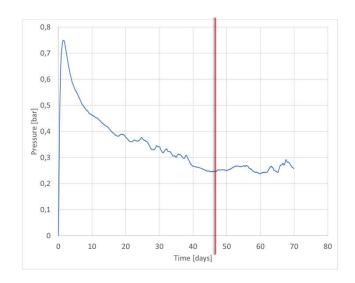
- Each sample is taken out of the oven and let to cool down
- PD measurements are started at beginning of bushing cooldown and are performed at several time instants during a 24 hours period.
- For each measurement step, the electrical test sequence is as per IEEE Std C57.12.00
  - Enhanced level 1.8 x nominal system voltage (line-to-ground) for 7200 cycles
  - 1.58 x nominal system voltage (line-to-ground) for 1 hour
- These electrical values cover the transformer FAT program and assure safe operating conditions.
- The bushing passes the test if there is no PD above 10pC measured during the test sequence.



## **Example: 230 kV OIP Bushing Cooldown PD Test**







Internal pressure during the saturation phase

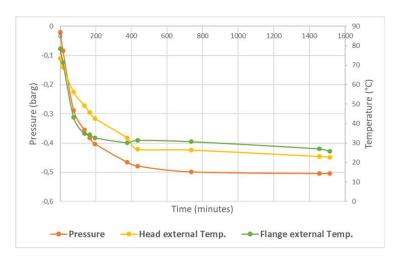
Table 1: Report for electrical tests

App. n*: 2J B5i57 Tension maximale				Client Customer						
Highest volta			230 kV	'						
Fréquence n	ominale		60 Hz		]					
Rated frequency				Comman	de					
Rated current 800 A				Order 7000296 / 30						
Essai selon Test as to		IEEE (	C57.19.0	01-2017	Plan d'en Drawing	combren	nent	4142682	21 / 07	
	ent montée /	Complete	lv assen	nbled	Didning		-			
partie sup. o	dans / upper ans / lower p	part in:		Huile/Oil Huile/Oil		dr dr		SF6 SF6	piètem	ent / turret
•	atmosphériqu		o4 mb	ar 21°C	24%	humidite	e relative	/ relative	humidity	
	is heated a								ncluding depr	
phase due t voltage test					g is remo	ved from	n the aut	oclave an	d installed in	
Time		Temperature (°C)		Internal Pressure	Voltage	PD	C1	PF	PD inception	PD extinction
		Head	Flange	(bar)	(kV)	(pC)	(pF)	(%)	voltage (kV)	voltage (k\
Removal from	n autoclave									
t <sub>0</sub> =										
Test under vo	oltage									
t: =					146	<1	487	0,42		
t <sub>1</sub> + 15 min					146	<1	483	0,41		
t <sub>1</sub> + 30 min				77	146	<1	487	0,40		
t <sub>1</sub> + 45 min					146	<1	486	0,37		
t <sub>1</sub> + 60 min					146	<1	486	0,36		
ts + 75 min					146	<1	486	0,34		
t <sub>1</sub> + 90 min					146	<1	485	0.33		
t <sub>1</sub> + 105 min					146	<1	485	0,33		
t <sub>1</sub> + 120 min					146	<1	485	031		
t <sub>1</sub> + 135 min					146	<1	485	931		
t <sub>1</sub> + 150 min					146	<1	484	0.31		
t <sub>1</sub> + 165 min					146	<1	484	0,30		
t <sub>1</sub> + 180 min					146	t	484	930		
t <sub>1</sub> + 195 min					146	1	484	930		
t <sub>1</sub> + 210 min					146	1	484	0,30		
t <sub>1</sub> + 225 min					146	1	483	929		
t <sub>1</sub> + 240 min					146	1	483	0,29		
t <sub>1</sub> + 255 min					146	١	483	929		
t <sub>1</sub> + 270 min					146	t	483	0,29		
t <sub>1</sub> + 285 min					146	1	483	929		
t <sub>1</sub> + 300 min					146	1	483	929		
Time		Temperature (*C)		Internal Pressure	Voltage	PD	C1	PF	PD inception	PD extinction
		Head	Flange	(bar)	(kV)	(pC)	(pF)	(%)	voltage (kV)	voltage (k\
tı + 315 min					146	ì	483	929		
t <sub>1</sub> + 330 min					146	1	483	929		
tı + 340 min					146	1	483	929		
t <sub>1</sub> + 340 min					240 (144 s)	2	<b>1</b> 83	928		
tı + 342 min					210 (60 mn)	2	183	0,28		

# **Example: 230 kV OIP Bushing Cooldown PD Test**







Internal pressure and external bushing temperatures during cooldown phase

Table 1: Report for electrical tests

App. n°: 21 B 515 <b>6</b>				Client Customer							
Tension maximale Highest voltage 230 kV				<b>v</b>							
Fréquence r Rated frequ		60 Hz									
Courant nor Rated curre		800 A			Commande Order 7000296 / 30						
Essai selon Test as to		IEEE	C57.19	01-2017	Plan d'encombrement Drawing 41426821 / 07						
Complèten	nent montée	/ Comple	tely asse	mbled	•						
partie sup. dans / upper partie inf. dans / lower p						SF6 piètement / turre					
	atmosphério ic conditions		foll m	oar 19°C	63 % hu	midité re	elative / re	elative hu	midity		
and installed in the high		Temperature (°C)  Head Flange		Internal Pressure (bar)	Voltage (kV)	PD (pC)	C1 (pF)	PF (%)	PD inception voltage (kV)	PD extinction voltage	
1. Remov	al from autoc	lave			1	1			(KV)	(kV)	
to =	6414	73.4	78,4	-0,02	-	Τ-		-	-	-	
2. Test un	der voltage	On The Control Control	Colemanius	a and the second second							
t <sub>1</sub> =	6H30	68.9	71.4	-0.084	240 (144 s)	41	487	0.43			
	7430	562	43,2	-0,288	210 (60 mn)	41	485	0,37			
	OR STATES SANCES	100	21.0	0.000	_			-	-	-	
t <sub>1</sub> + 2 h	8H30	49.3	34.8	-0,355		1 -	1				
t <sub>1</sub> + 2 h t <sub>1</sub> + 2,5 h	8H30	45.6	34,8	-0,383	-	-	+	-	-	2	
	THE CONTRACTOR OF THE		120000000000000000000000000000000000000	HORSE TO SELECT STATES	- 240 (144 s)	- (1	484	- O, 30	-	-	
t <sub>1</sub> + 2,5 h	3400	45.6	34.3	-0.383		10700100	484	0,30	-	-	
t <sub>1</sub> + 2,5 h	3400	42,6	34,3 32,7	-0,383 -0,403		(1			<u>-</u>	-	
t <sub>1</sub> + 2,5 h t <sub>1</sub> + 3 h	9400 9430	42.6 37.8	34,3 32,7 32,1	-0,387 -0,403 -0,436	210 (60 mn)	<1 <1	483	0,29	-	-	
t <sub>1</sub> + 2,5 h t <sub>1</sub> + 3 h	3400 3430	42.6 42.6 37.8 31.6	34.3 32.7 32.1 30.2	-0,387 -0,403 -0,436 -0,466	210 (60 mn) 240 (144 s)	(1 (1	482	0,23		-	
t <sub>1</sub> + 2,5 h t <sub>1</sub> + 3 h t <sub>1</sub> + 6 h	3 HOO 3 H30 12 H30	42.6 37.8 31.6 26.8	34,3 32,7 32,1 30,2 31,4	-0.38) -0.403 -0.436 -0,466 -0,479	210 (60 mn) 240 (144 s) 210 (60 mn)	<1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <1 <	482 482	0,23 0,28 928	-		
t <sub>1</sub> + 2,5 h t <sub>1</sub> + 3 h t <sub>1</sub> + 6 h	3 HOO 3 H30 12 H30	45.6 42.6 37.8 3 <b>1.6</b> 26.8 26,3	34,3 32,7 32,1 30,2 31,4 30,7	-0,38) -0,403 -0,436 -0,466 -0,479	210 (60 mn) 240 (144 s) 210 (60 mn) 240 (144 s) 210 (60 mn)	(4) (4) (1) (4) (4)	482 482 482	0,23 0,28 928 0,29			