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**Voltage Dependency of HV CT Ratio Errors**

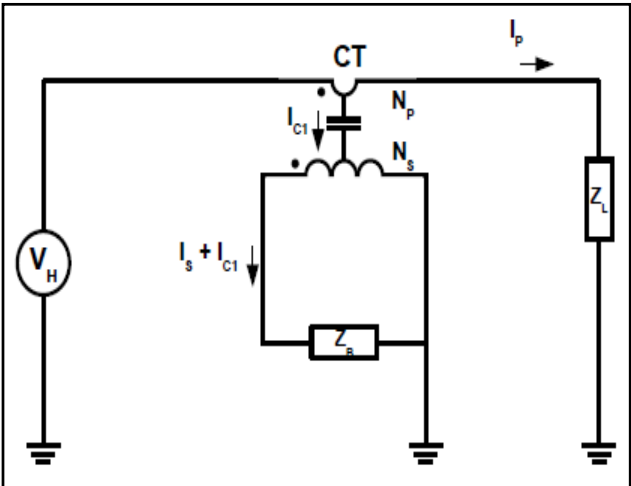
E. So,  
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National Research Council Canada

IEEE PES Transformers Committee Meeting  
23 October, 2013

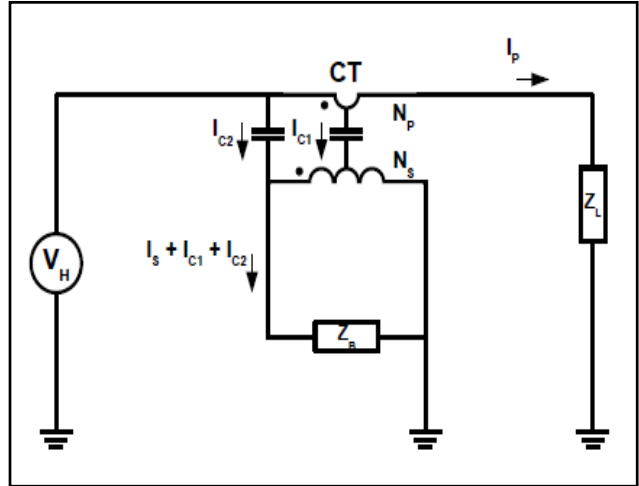
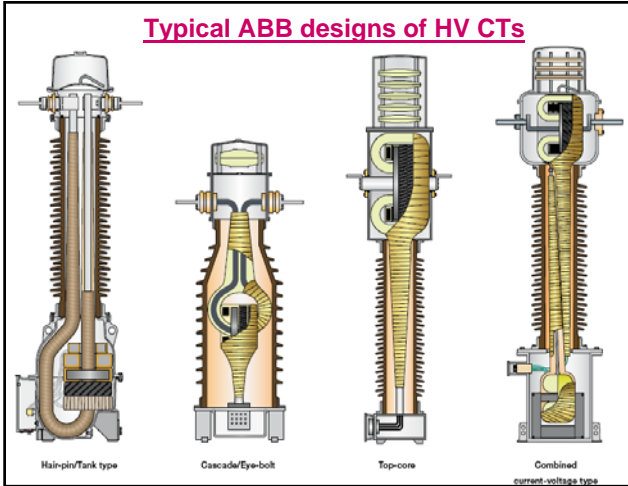
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- Problem**
- IEEE/IEC Standards defined Ratio Errors with ratio windings at ground potential.
  - HV CTs are calibrated with primary and secondary windings at ground potentials.
  - In actual use, the HV CT is operated with one, or the other, or both of these windings at a voltage which is substantially different from the test conditions at ground potential.

- Capacitive currents, which were not present or were negligible during calibrations, will then flow when the CT is in its intended operating conditions and connected to high voltage.
- Operating at high voltage may result in a significant variation of the CT error measured during calibration, especially at low operating currents.
- Ratio Errors of HV CTs are voltage dependent.
- Voltage dependency of Ratio Errors not recognized by IEEE/IEC standards, C57.13/60044-1.



**Typical ABB designs of HV CTs**



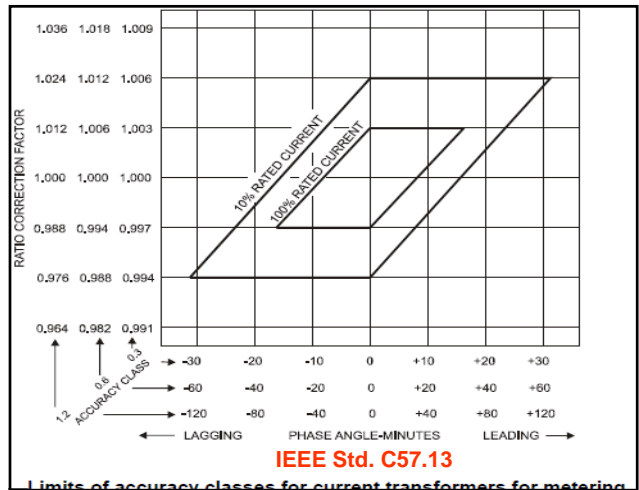
The transformer ratio errors are defined by the following equation:

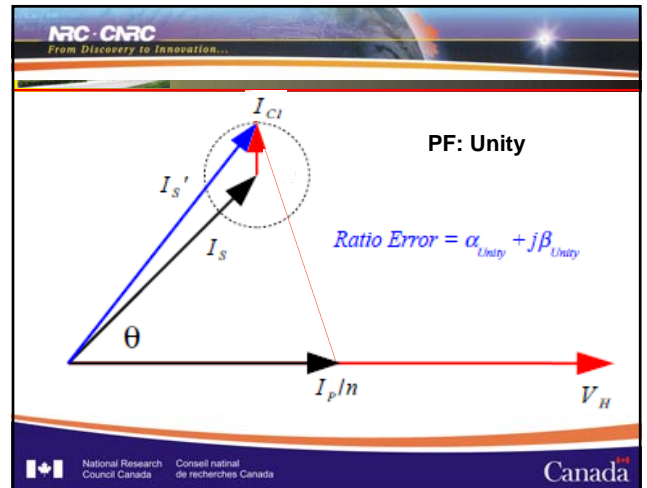
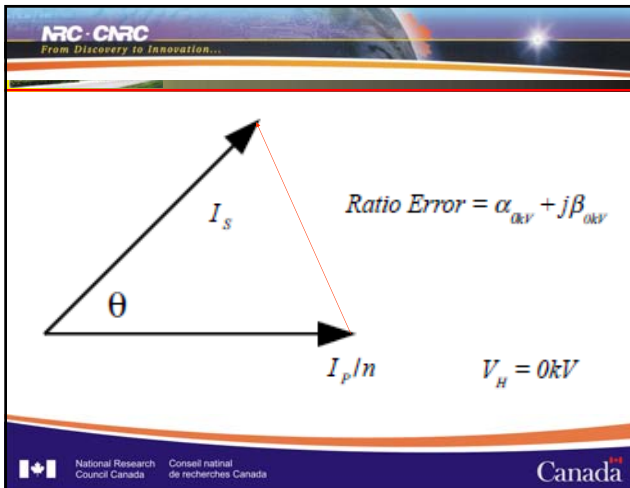
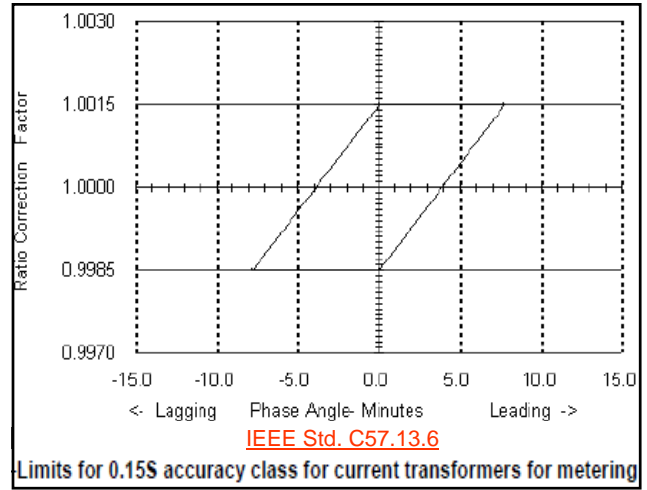
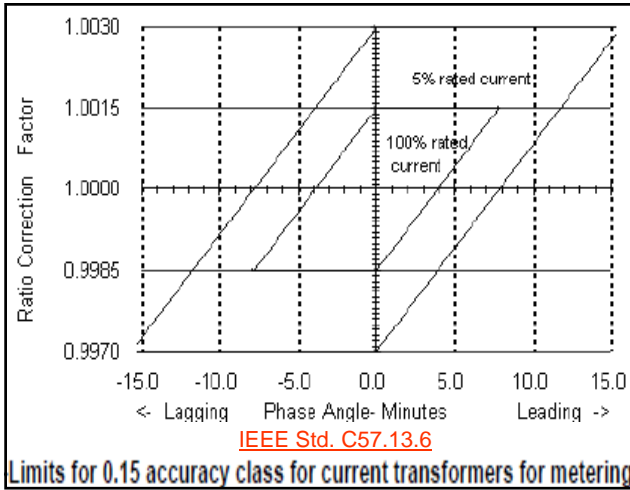
$$\alpha + j\beta = ((I_s - I_p/n) / (I_p/n)) \times 10^6$$

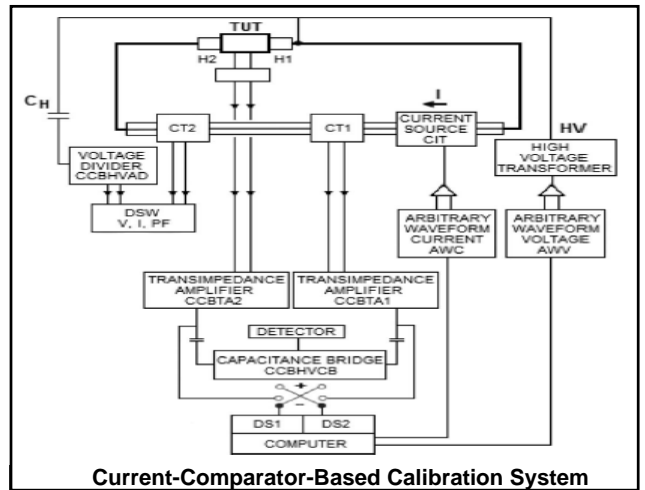
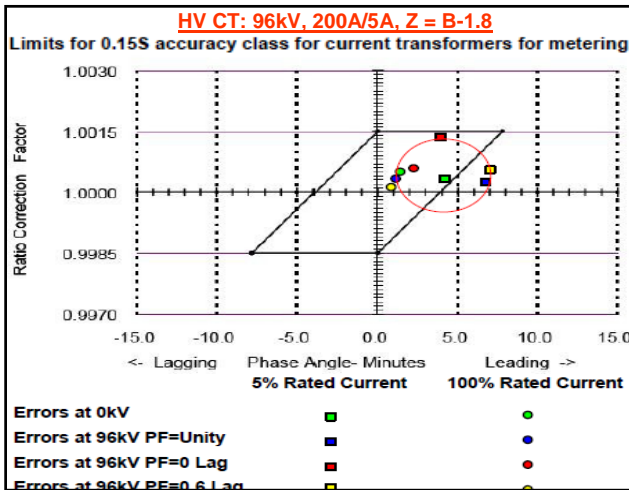
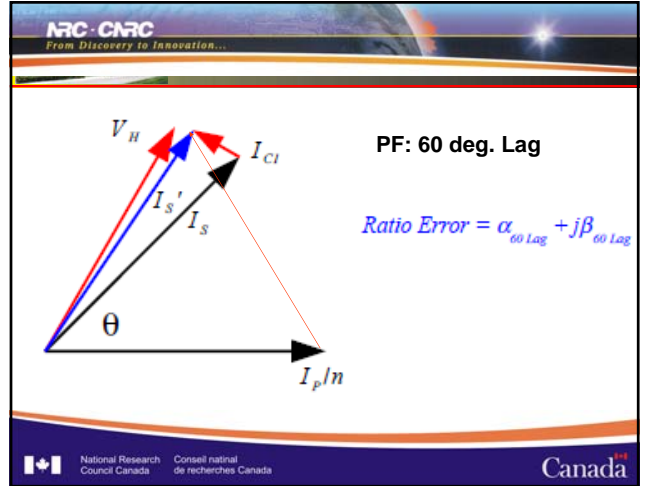
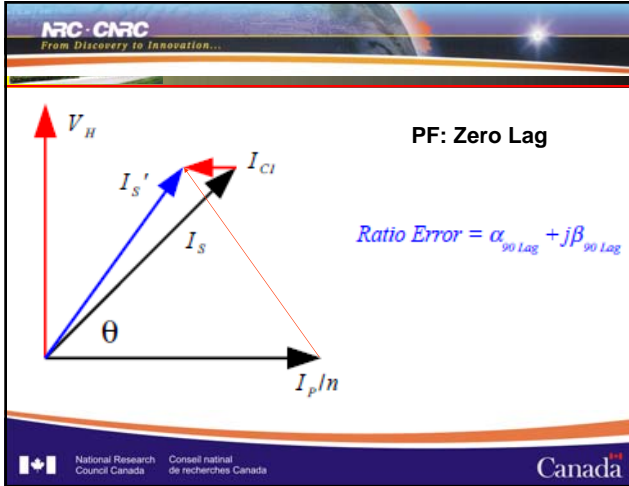
or  $RCF = 1 - (\alpha/10^6) = 1 - A$

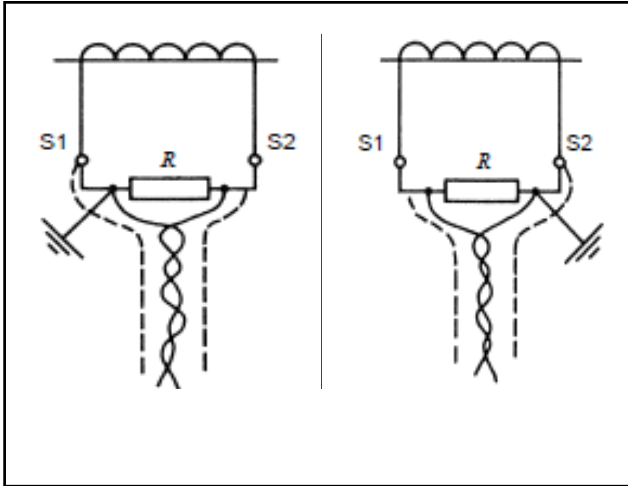
$PA = \beta/291 = B$

where:  $\alpha$  and  $\beta$  are the in-phase (magnitude) and quadrature (phase) errors,  $I_p$  and  $I_s$  are the primary and secondary currents, and  $n$  is the nominal ratio.









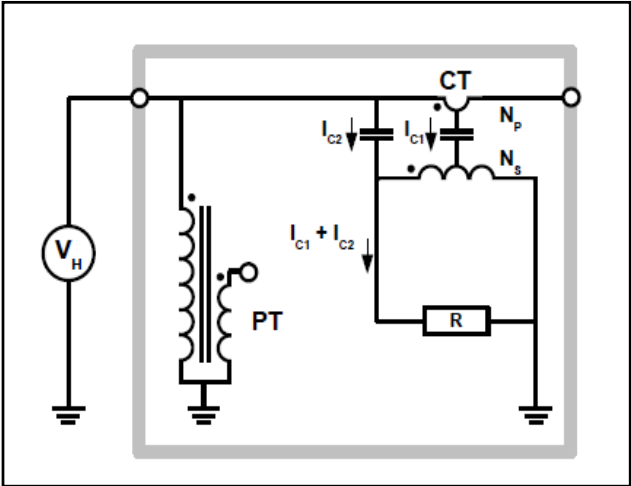
**IEC 60044-3\_Part 3**  
**Combined Transformers**

**Influence of the voltage transformer on the current transformer**

In the case of combined instrument transformers, the influence of the voltage transformer on the current transformer has to be tested as follows.

With an unexcited voltage transformer, the current error  $\epsilon_i$  and the phase displacement  $\delta_i$  of the current transformers are determined according to 11.4 and 12.4 of IEC 60044-1 (measurement 1).

A voltage equal to 120 % of the rated voltage and the rated voltage multiplied by the rated voltage factor shall then be applied to the terminal of the voltage transformer which is directly connected to a terminal of the current transformer, the latter not being excited. A capacitive current is generated in the current transformer by the voltage and this is measured as the voltage drop  $U_i$  across a resistor  $R$  connected to the secondary terminals of the current transformer. The burden of the secondary windings of the voltage transformer does not affect the results. They may therefore be open-circuited.



It generally suffices to determine the influence of voltage at 5 % of the rated current.

The variation of the current error is then

$$\pm \Delta \epsilon_i = \frac{U_i}{R \times 0,05 I_{SN}} \times 100 [\%] \text{ at } 5\% \text{ of the rated current.}$$

where

$R$  is expressed in ohms;

$U_i$  is expressed in volts;

$I_{SN}$  is the rated secondary current in amperes.

The variation of the phase displacement is then

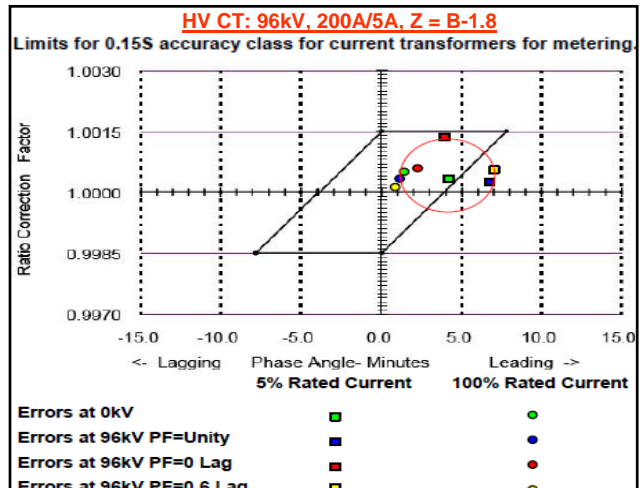
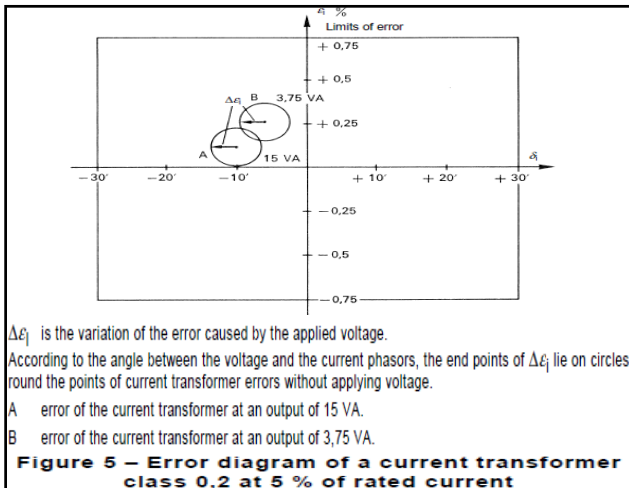
$$\pm \Delta \delta_i = \Delta \epsilon_i \times 34,4, \text{ in minutes, or}$$

$$\pm \Delta \delta_i = \Delta \epsilon_i, \text{ in centiradians;}$$

If the variations of the current error  $\pm \Delta \epsilon_i$  and of the phase displacement  $\pm \Delta \delta_i$  are added to the absolute values of the measuring results  $\epsilon_i$  and  $\delta_i$  obtained in Measurement 1 at 5 % of the rated current within the specified range of burden, then the values obtained

$$\pm \epsilon'_i = |\epsilon_i| + |\Delta \epsilon_i| \quad \text{and} \quad \pm \delta'_i = |\delta_i| + |\Delta \delta_i| \quad (\text{see Figure 5})$$

shall not exceed the limits of error for the current transformer given in 11.2 and 12.3 of IEC 60044-1. It must be ensured, however, that current errors do not exceed the limits of error, even between 5 % and 120 % of the rated current and in the case of extended current rating at the rated continuous thermal current.



#### Reference

### A Current-Comparator-Based System For Calibrating High-Voltage Current Transformers Under Actual Operating Conditions

Eddy So, *Fellow, IEEE*, Rejean Arseneau, *Senior Member, IEEE*,  
David Bennett and Michelle E. Frigault

IEEE Transaction on Instrumentation and Measurements, Vol. 60-7, July 2011

#### CONCLUSIONS

- The effect of voltage dependency on the ratio errors of HV CTs is dependent, not only on their operating voltage, but also on the phase of the primary current with respect to the operating voltage (Load Power Factor).
- At low currents the voltage dependency effects could render the CT to be no longer meeting its original accuracy class.
- Problem for Regulating Bodies that do Type Approval Tests and also for utilities/users, manufacturers. Also for IEEE/IEC Standards (?).

#### CONCLUSIONS (Cont.)

- Further study and evaluation on voltage dependency effects of different types and designs of high accuracy class HV CTs, in particular of class 0.2s, 0.15s, 0.1s, or better, under actual operating conditions of high voltage and not only sinusoidal current waveforms, but also distorted current waveforms.
- Proposal to the Instr. Trafo SC to consider CT voltage dependency characteristics to be mentioned in the next update of C57.13 and/or C57.13.6 "High-Accuracy Instr. Transformers".

## Questions?

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