

# AWGN Noise models for PHY Evaluation

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# Agreed Baseline ANEXT/AFEXT

[https://www.ieee802.org/3/dg/link\\_segment\\_090723.pdf](https://www.ieee802.org/3/dg/link_segment_090723.pdf)

## PSANEXT & PSAACR-F (July 2023)

PSANEXT:	$50 + 5 \times N$	$0.1 \leq f < 10$ MHz
	$50 + 5 \times N - 15 \times \log_{10}(f/10)$	$10 \leq f \leq 60$ MHz

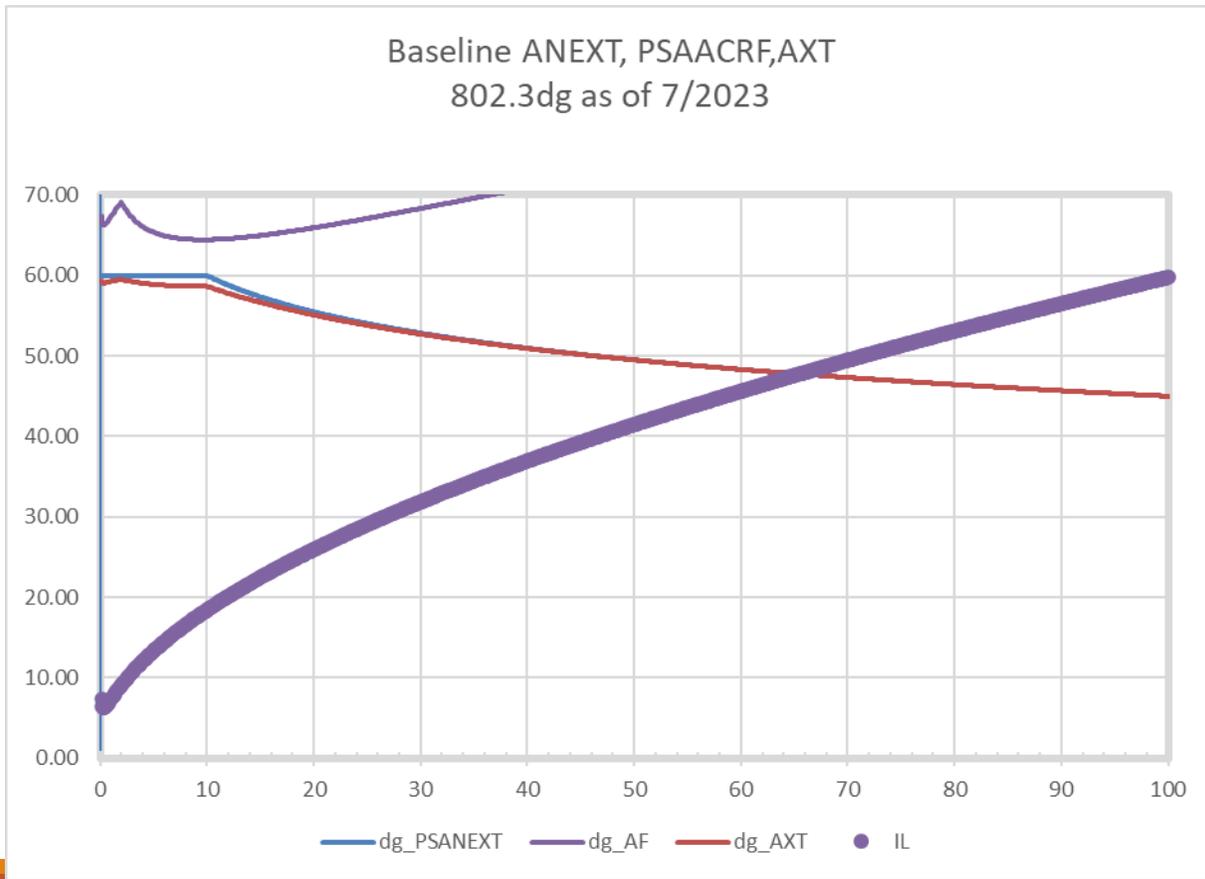
PSAACRF:	$50 + 5 \times N$	$0.1 \leq f < 2$ MHz
	$36 + 5 \times N - 20 \times \log_{10}(f/10)$	$2 \leq f \leq 60$ MHz

With N =	0	for $IL_{20} < 16$ dB
	$0.5 \times (IL_{20} - 16)$	for $16 \leq IL_{20} < 18$ dB
	1	for $18 \leq IL_{20} < 21$ dB
	$1 + 0.5 \times (IL_{20} - 21)$	for $21 \leq IL_{20} < 23$ dB
	2	for $23 \leq IL_{20}$ (dB)

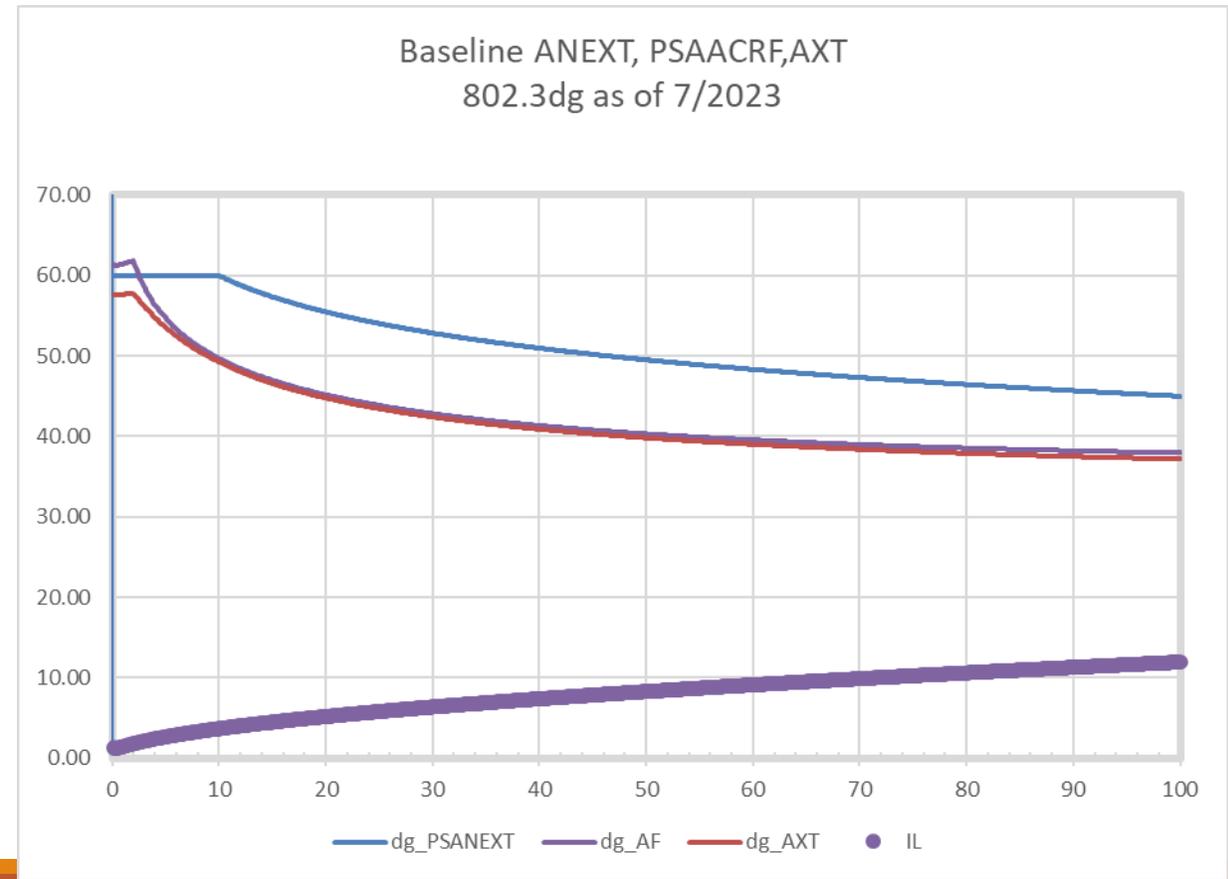
(f is in MHz)

# AFEXT dominates when disturber line is short

500m disturber



100m disturber (500m victim ANEXT/AACRF limits)



# Model Source for 100BASE-T1L

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Start with 10BASE-T1L PSD mask

- Lower 3 dB (halfway between 2 masks) (-54 -> -57dBm/Hz)
- Assume 10x baud for shape of PSD, adjust level to compensate for actual baud

Scale level with baud being evaluated:  $-10 \cdot \log_{10}(f_{\text{baud}}/7.5\text{MHz})$  dB

- E.g., 75 Mbaud means -57 dBm/Hz -> -67 dBm/Hz
- Call the flat PSD level ( $-57 - 10\log_{10}(f_{\text{baud}}/7.5\text{ MHz})$ ), TXpsd

Frequency-scale corner & rolloff:

- Extend corner frequency: (2.5 MHz -> 25 MHz)
- Scale rolloff by 10x as well: (-1.6 dB/MHz becomes -0.16 dB/MHz)

Result:  $\text{TXpsd}(0) = -57 - 10\log_{10}(f_{\text{baud}}/7.5\text{ MHz})$  dBm/Hz

- $\text{TXpsd}(f) = \text{TXpsd}(0)$  dBm/Hz for  $0 < f < 25\text{ MHz}$
- $\text{TXpsd}(f) = \text{TXpsd}(0) - 0.16 \cdot (f - 25\text{ MHz})$  dBm/Hz for  $25 \leq f < 125\text{ MHz}$

# Separated, equal-length Link model

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If no 10BASE-T1L connectors are adjacent to 100BASE-T1L we can use just the PSANEXT coupling model on long links, as this will dominate:

- Flat PSD Level :  $\text{TXpsd} = -117 - 10\log_{10}(f_{\text{baud}}/7.5 \text{ MHz})$

$\text{TXpsd} -60 \text{ dBm/Hz}$  for  $0 < f < 10 \text{ MHz}$

$\text{TXpsd} -60 -15\log_{10}(f/10) \text{ dBm/Hz}$  for  $10 \leq f < 25 \text{ MHz}$

$\text{TXpsd} -60 - 15\log_{10}(f/10) - 0.16(f-25\text{MHz}) \text{ dBm/Hz}$  for  $f \geq 25 \text{ MHz}$

# Separated Equal Length Long Line

Average over Nyquist band for 75 Mbaud signal is -122.7 dBm/Hz

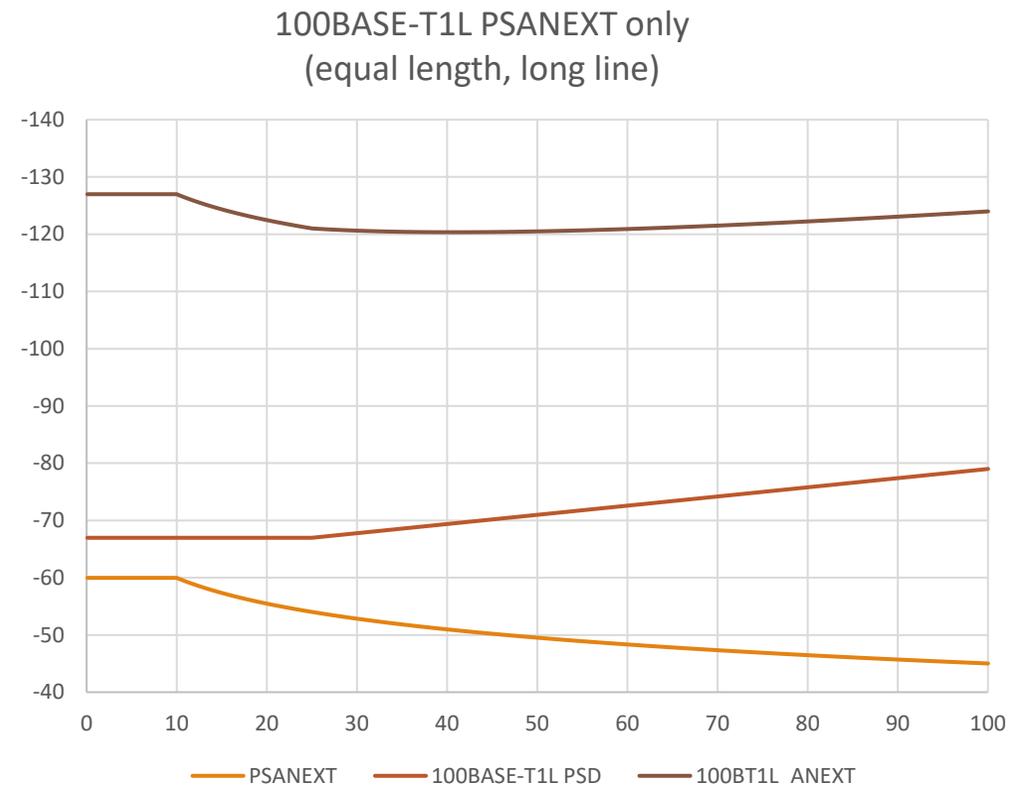
(average over 60 MHz is 1.1 dB lower)

Peak to peak ripple is 7 dB, with lower noise for  $f < 10$  MHz.

Recommend for this case, AWGN:

$-122.7 \text{ dBm/Hz} - 10\log_{10}(f_{\text{baud}}/75) \text{ dBm/Hz}$

0 to 60 MHz



# Dealing with near-far AXT

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Far-end crosstalk from shorter disturbers coupled in near to a receiver can dominate noise

If this is expected, recommend we implement a power back off strategy

BUT – we need to be careful with this because it will make shorter links more vulnerable with impulse noise.

For now, assume we use power back off and can use 500m AFEXT curve for 100BASE-T1L disturbers...

# Crosstalk from 10BASE-T1L

Likely 10 dB higher peak PSD (same launch voltage, less bandwidth) (higher for  $f < 8.5$  MHz)

Also, 10BASE-T1L does NOT have power backoff so we will have to consider short-line AFEXT

Adds 10dB to coupling starting at  $\sim 8.5$  MHz

Assume rolloff continues beyond floor at 12 MHz

**Short-line PSAFEXT from 10BASE-T1L will dominate at frequencies to  $\sim 17$  MHz based on mask & coupling**

$$\text{Upper PSD Limit } (f) \geq \begin{cases} -54 \text{ dBm/Hz} & 0 \leq f \leq 2.5 \\ -54 - 1.6 \times (f - 2.5) \text{ dBm/Hz} & 2.5 < f < 12.5 \\ -70 \text{ dBm/Hz} & 12.5 \leq f \leq 20 \end{cases}$$

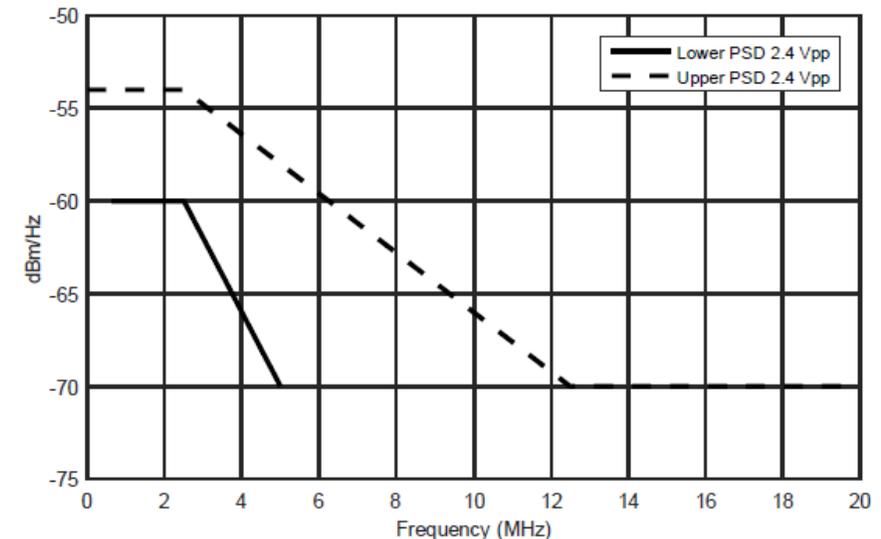


Figure 146-22—Transmitter Power Spectral Density, 2.4 Vpp Transmit Amplitude, Upper and Lower Masks

Source: IEEE Std 802.3-2022 Eqn 146-6 and Fig 146-22

# Mixed Crosstalk Disturbing source

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Equal parts 10BASE-T1L & 100BASE-T1L

- Reduce each disturbing PSD by 3dB to account for fewer disturbers

Use 100m AFEXT coupling model for 10BASE-T1L, ANEXT coupling model for 100BASE-T1L

# Separated Equal Length Long Line

Average over Nyquist band for 75 Mbaud signal is -120.3 dBm/Hz

(average over 60 MHz is 0.9 dB lower)

Peak to peak ripple is ~10 dB, with higher noise for  $f < 20$  MHz.

Recommend for this case, Sum of 2 AWGN sources

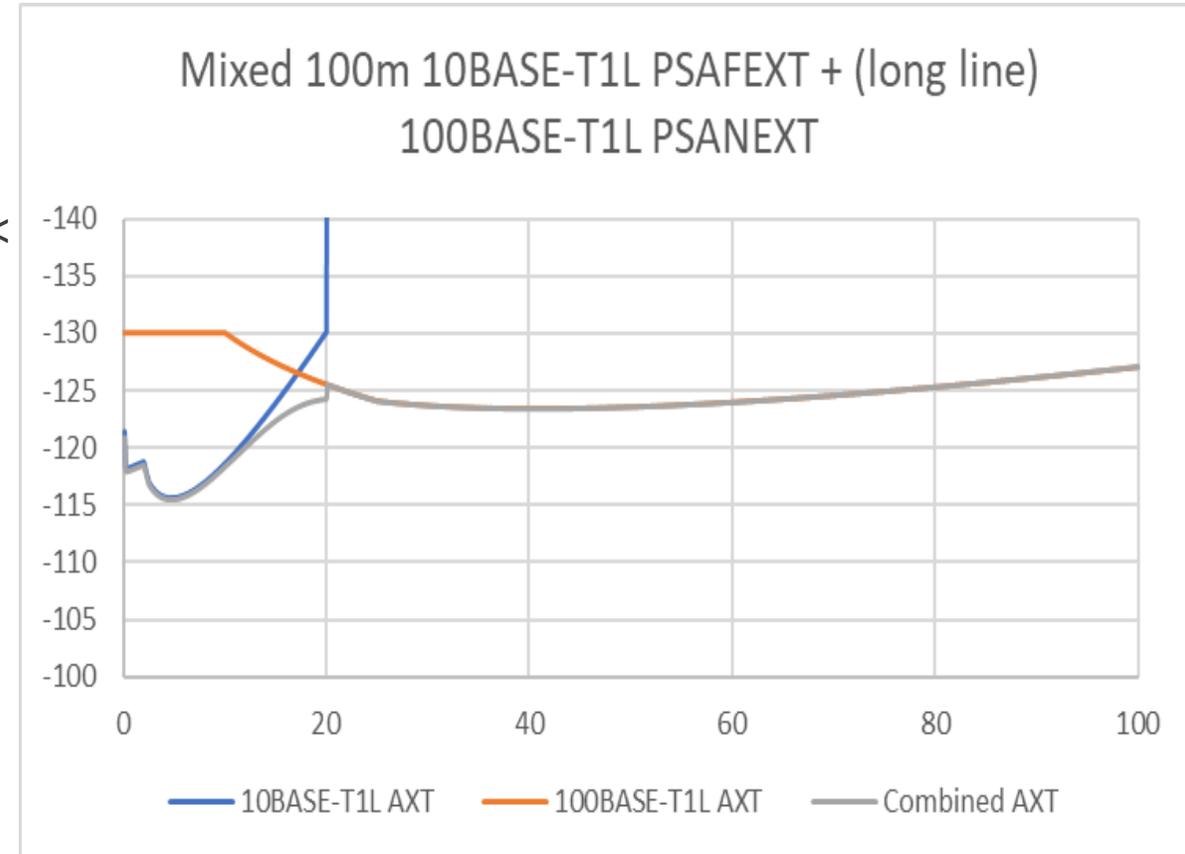
Source 1:

-123.5 dBm/Hz –  $10\log_{10}(f_{\text{baud}}/75)$  dBm/Hz

0 to 60 MHz

Source 2:

-117 dBm/Hz 0 to 20 Mhz, filtered by 2<sup>nd</sup> order LPF at 5 MHz



# Comments

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The main thing we need to determine is how we intend to deal with the near-far problem

If we don't, the 100BASE-T1L noise will be about 10 dB higher

The second thing we need to determine is whether 10BASE-T1L will be collocated with 100BASE-T1L

This drives the second model

Recommend for now we assume we deal with the near-far problem, but need to coexist with mixtures of 10BASE-T1L

These models are for PHY evaluation only – we will have to redo them when we write the Alien Crosstalk Rejection test.