

IEEE P802.3ck D1.3 100/200/400 Gb/s Electrical Interfaces Task Force 4th Task Force review comments

CI 162 SC 162.8.11 P144 L16 # 1

Lusted, Kent Intel Corporation

Comment Type TR Comment Status X

In the IEEE 802.3cd-2018 project, an updated PMD Control Function (i.e. link training) was defined and specified in CI 136.8.11.

Among other things, specific changes enabled the link training protocol to support link establishment between two devices without using CI 73 Auto-Negotiation (i.e. for the customer use case of "forced PHY speed" on the link).

The currently defined state machine in Clause 136.8.11 (Figure 136-7) does not autonomously recover from a partner breaking frame lock during link training (Note: observed when the Clause 73 Auto-Negotiation state machine is not used.) Unless a high-level management agent (i.e. SW or FW) detects the condition, the result could be either a link down (i.e. link never comes up) or a link oscillation (up/down/up/down/etc). One reason is that the signals local_tf_lock and remote_tf_lock are only checked moving from the SEND_TF state to the TRAIN_LOCAL state. Another is that there is no clear indication between the two end points that the link has been restarted (without AN73 present). There are other reasons as well, not listed here.

SuggestedRemedy

Update the PMD control state diagram to account for this situation. Some solutions include, but are not limited to:

- increase the duration of the holdoff_timer to exceed that of the max_wait_timer (>= 12 seconds)
- add monitoring of the local and received frame lock status after the initial frame lock is achieved
- implement an abort signaling mechanism

See presentation to be submitted for TF consideration.

Proposed Response Response Status O

CI 120F SC 120F.3.2.3 P213 L31 # 2

Mellitz, Richard Samtec

Comment Type TR Comment Status X

DFE4_RSS > 0.05 may be difficult to achieve with test equipment. The published C2C have a DFE4_RSS range between 0.03 V and 0.065 with a mean of 0.047 .

SuggestedRemedy

Since these represent design expectation set DFE4_RSS to 0.03 which would be achievable in test setups.

Proposed Response Response Status O

CI 162 SC 162.9.3 P146 L27 # 3

Mellitz, Richard Samtec

Comment Type TR Comment Status X

The ERL range is between 7.3 dB and 18.8 for published channels that representative of 100G Host designs.

SuggestedRemedy

Set ERL (min) to 7.3 dB in Table 162.-10

Proposed Response Response Status O

CI 162 SC 162.9.4 P151 L44 # 4

Mellitz, Richard Samtec

Comment Type TR Comment Status X

The ERL range is between 7.3 dB and 18.8 for published channel that representative of 100G Host designs.

SuggestedRemedy

Set ERL (min) to 7.3 dB in Table 162.-13

Proposed Response Response Status O

CI 163 SC 163.9.2 P176 L50 # 5

Mellitz, Richard Samtec

Comment Type TR Comment Status X

We need to specify V_peak/V_f not V_peak. I.e. pulse peak loss

SuggestedRemedy

Change
Difference between measured and reference linear fit pulse peak
To
Difference between measured and reference linear fit pulse peak loss (min) d(V_peak/V_f)

Proposed Response Response Status O

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Cl 163 SC 163.9.2.2 P 178 L 29 # 6 [REDACTED]
 Mellitz, Richard Samtec
 Comment Type **TR** Comment Status **X**
 TP0a is moot and replaced by TP0v
 SuggestedRemedy
 remove references to TP0a.
 Proposed Response Response Status **O**

Cl 163 SC 163.9.3.2 P 181 L 1 # 9 [REDACTED]
 Mellitz, Richard Samtec
 Comment Type **TR** Comment Status **X**
 There is no reason why the receive test fixture specification should be different from the transmitter one.
 SuggestedRemedy
 Point to the transmitter specification for test fixture
 Proposed Response Response Status **O**

Cl 163 SC 163.9.3 P 180 L 17 # 7 [REDACTED]
 Mellitz, Richard Samtec
 Comment Type **TR** Comment Status **X**
 TP5a is moot and replaced by TP5v
 SuggestedRemedy
 remove references to TP5a and replace with TP5v.
 Proposed Response Response Status **O**

Cl 163 SC 163.10.3 P 186 L 41 # 10 [REDACTED]
 Mellitz, Richard Samtec
 Comment Type **TR** Comment Status **X**
 The ERL range is between 9.7 dB and 23.5 dB for published channel that representative of 100G KR designs.
 SuggestedRemedy
 change the TBD in in line 41 to 9.7 dB
 Proposed Response Response Status **O**

Cl 163 SC 163.9.3 P 180 L 26 # 8 [REDACTED]
 Mellitz, Richard Samtec
 Comment Type **TR** Comment Status **X**
 There is no reason why the receive ERL specification should be different from the transmitter ones.
 SuggestedRemedy
 Point to the transmitter specification for DERL
 Proposed Response Response Status **O**

Cl 163 SC 163.13.4.4 P 192 L 33 # 11 [REDACTED]
 Mellitz, Richard Samtec
 Comment Type **TR** Comment Status **X**
 TP5a is moot and replaced by TP5v
 SuggestedRemedy
 remove references to TP5a and replace with TP5v. Change RC2 to DERL at TP5v
 Proposed Response Response Status **O**

IEEE P802.3ck D1.3 100/200/400 Gb/s Electrical Interfaces Task Force 4th Task Force review comments

Cl 163 SC 163.13.4.3 P 192 L 8 # 12
 Mellitz, Richard Samtec
 Comment Type **TR** Comment Status **X**
 We are not specifying ERL directly
 SuggestedRemedy
 Change TC2 to DERL at TP0v
 Proposed Response Response Status **O**

Cl 120F SC 120F.3.1 P 208 L 20 # 13
 Mellitz, Richard Samtec
 Comment Type **TR** Comment Status **X**
 We need to specify V_{peak}/V_f not V_{peak} i.e. pulse peak loss
 SuggestedRemedy
 Change
 Difference between measured and reference linear fit pulse peak
 To
 Difference between measured and reference linear fit pulse peak loss (min) $d(V_{peak}/V_f)$
 Proposed Response Response Status **O**

Cl 120F SC 120F.3.2 P 211 L 32 # 14
 Mellitz, Richard Samtec
 Comment Type **TR** Comment Status **X**
 TP5a is moot and replaced by TP5v
 SuggestedRemedy
 point to Rx table in 163 line done in table 120F-1
 Proposed Response Response Status **O**

Cl 162 SC 162.11 P 156 L 39 # 15
 DiMinico, Christopher MC Communications
 Comment Type **TR** Comment Status **X**
 Provide specifications for Differential to common-mode return loss 162.11.4

SuggestedRemedy
 Replace TBD with equation reference in Table 162–16—Cable assembly characteristics summary.
 Add text and equation 162.11.4 Differential to common-mode return loss
 The differential to common-mode return loss, in dB, of the cable assembly shall meet
 Equation (xx)
 $CDRL(f) \geq$
 $22 - 10 * f / 26.56, 0.05 \leq f \leq 26.56$
 $15 - 3 * f / 26.56, 26.56 < f \leq 40$
 Where
 f is the frequency in GHz
 See supporting presentation diminico_3ck_1020.pdf
 Proposed Response Response Status **O**

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CI 162 SC 162.11 P 156 L 41 # 16

DiMinico, Christopher MC Communications

Comment Type **TR** Comment Status **X**

Provide specifications for Differential to common-mode conversion loss 162.11.5

SuggestedRemedy

Replace TBD with equation reference in Table 162–16—Cable assembly characteristics summary.

Add text and equation 162.11.5 Differential to common-mode conversion loss

The difference between the cable assembly differential to common-mode conversion loss and the cable assembly insertion loss shall meet Equation (xx).

$$CDCL(f) - IL(f) \geq$$

$$10, 0.05 \leq f \leq 26.56$$

$$27-17*f/26.56, 26 < f \leq 33.2$$

$$5.75, 33.2 < f \leq 40$$

Where
f is the frequency in GHz

See supporting presentation diminico_3ck_1020.pdf

Proposed Response Response Status **O**

CI 162 SC 162.11.2 P 157 L 10 # 17

DiMinico, Christopher MC Communications

Comment Type **TR** Comment Status **X**

Replace TBD

SuggestedRemedy

Replace TBD with 0.05

Proposed Response Response Status **O**

CI 162A SC 162A.4 P 248 L 42 # 18

DiMinico, Christopher MC Communications

Comment Type **TR** Comment Status **X**

Replace TBD with equation

SuggestedRemedy

$$ILPCB_{max}(fGHz)=0.9809*(0.471*SQRT(f)+0.1194*f+0.002*(f^2))$$

for
0.01 GHz $\leq f \leq$ 50 GHz

See supporting presentation diminico_3ck_1020.pdf

Proposed Response Response Status **O**

CI 162A SC 162A.4 P 249 L 39 # 19

DiMinico, Christopher MC Communications

Comment Type **TR** Comment Status **X**

Replace TBD with equation

SuggestedRemedy

$$ILHOST(f)=1.5658*(0.471*SQRT(f)+0.1194*f+0.002*(f^2))$$

for
0.01 GHz $\leq f \leq$ 50 GHz

See supporting presentation diminico_3ck_1020.pdf

Proposed Response Response Status **O**

CI 162B SC 162B.1.3.6 P 260 L 48 # 20

DiMinico, Christopher MC Communications

Comment Type **TR** Comment Status **X**

Replace TBD

SuggestedRemedy

Replace TBD with 1.6 mV

Proposed Response Response Status **O**

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Cl 162B SC 162B.1.3.1 P 255 L 35 # 21
 DiMinico, Christopher MC Communications
 Comment Type **TR** Comment Status **X**
 Modify Equation (162B-3) ILMTFMAX > 40 GHz to align with achievable MTF insertion loss
 SuggestedRemedy
 See supporting presentation diminico_3ck_1020.pdf
 Proposed Response Response Status **O**

Cl 162B SC 162B.1.3.2 P 256 L 46 # 22
 DiMinico, Christopher MC Communications
 Comment Type **TR** Comment Status **X**
 Modify Equation (162B-6) DRL(f) > 40 GHz to align with achievable MTF return loss
 SuggestedRemedy
 See supporting presentation diminico_3ck_1020.pdf
 Proposed Response Response Status **O**

Cl 163 SC 163.9.3.2 P 181 L 3 # 23
 Ben-Artsi, Liav Marvell Semiconductor Ltd.
 Comment Type **E** Comment Status **X**
 According to direction of the entire path, TP5a is the input to the test fixture and not the output
 SuggestedRemedy
 Change: "Unless otherwise noted, measurements of the receiver are made at the output of a test fixture (TP5a) as shown in Figure 163-5." to: "Unless otherwise noted, measurements of the receiver are made at the input of a test fixture (TP5a) as shown in Figure 163-5."
 Proposed Response Response Status **O**

Cl 163 SC 163.9.3.2 P 181 L 19 # 24
 Ben-Artsi, Liav Marvell Semiconductor Ltd.
 Comment Type **T** Comment Status **X**
 The test fixture insertion loss of 1.2-1.6dB is not commonly feasible
 SuggestedRemedy
 Recommend adjusting TP5a-TP5 fixture characteristics to be the same as those defined for TP0-TP0a.
 Can either define less than 5dB of loss and ILD less than 0.2dB, or even in a simpler manner, just refer to 163.9.2.1.1 (insertion loss), 163.9.2.1.2 (ERL) and 163.9.2.1.3 (common mode RL)
 Proposed Response Response Status **O**

Cl 163 SC 163.9.3.2 P 181 L 26 # 25
 Ben-Artsi, Liav Marvell Semiconductor Ltd.
 Comment Type **T** Comment Status **X**
 The differential return loss of the test fixture is defined to meet Equation (163-2) and 163-3 which are an incorrect reference
 SuggestedRemedy
 Recommend replacing with a reference to 163.9.2.1.2 (Tx test fixture ERL)
 Proposed Response Response Status **O**

Cl 163 SC 163.9.2.2 P 178 L 39 # 26
 Ben-Artsi, Liav Marvell Semiconductor Ltd.
 Comment Type **T** Comment Status **X**
 The transmitter and receiver test fixture informative examples are irrelevant, since they have extremely low loss
 SuggestedRemedy
 Recommend changing equation 163.1 to $IL(F) = 0.01 + 0.292 \cdot \sqrt{F} + 0.0936 \cdot F$ (F in GHz), which is more realistic and meets 4dB of loss at 26.5625GHz. It is also referred to in 163.9.3.2 on page 181 lines 22-24
 Proposed Response Response Status **O**

IEEE P802.3ck D1.3 100/200/400 Gb/s Electrical Interfaces Task Force 4th Task Force review comments

CI 93A SC 93A.1 P 195 L 24 # 27

Healey, Adam Broadcom Inc.

Comment Type E Comment Status X

What is a "pad" in this context and does the description really fit this parameter? Note that this change to the parameter name, should it persist, should be propagated to every COM parameter table in IEEE Std 802.3 and not just the ones created or modified by this amendment. This does not seem worthwhile since the change to the name does not add any descriptive value.

SuggestedRemedy

Remove "pad" from the description of this parameter (i.e., undo the change). Update Tables 162-18, 163-11, and 120F-7 accordingly.

Proposed Response Response Status O

CI 93A SC 93A.1 P 195 L 24 # 28

Healey, Adam Broadcom Inc.

Comment Type E Comment Status X

93A.1.2 exists in this document.

SuggestedRemedy

Add a cross-reference link.

Proposed Response Response Status O

CI 163 SC 163.9.2 P 176 L 44 # 29

Healey, Adam Broadcom Inc.

Comment Type T Comment Status X

The reference to 163A.3.2.2 is in danger of becoming circular. Annex 163A is mostly written to be generic and states that PHY/interface-specific parameters are "specified by the clause that invokes this method". However, no such specifications can be found in this clause, or in Annex 120F, that provides this information. This includes "test channel requirements", electrical characteristics used to compute $S^{(tp)}$, values for T_r , f_r , A_t , T_b , etc. One could assume that "test channel" requirements are given in the transmitter test fixture definition in 163.9.2.1, and the other values are the same as those used to compute COM from 163.10.1, but this should not be left to assumptions. It is unclear whether test 1 or test 2 (or test 1 AND test 2) characteristics for $S^{(tp)}$ should be used and clarity on this point needs to be provided.

SuggestedRemedy

Add a new subclause to Clause 163 and change the reference for "dERL", "dvf", and "dvpeak" to this new subclause. The content of this subclause should be specifications for the PMD/interface-specific parameters that Annex 163A says are to be defined by the "clause that invokes this method". Similar changes would be necessary for Annex 120F.

Proposed Response Response Status O

CI 163A SC 163A.2 P 281 L 4 # 30

Healey, Adam Broadcom Inc.

Comment Type E Comment Status X

The "test channel" requirements are not defined by the clause that invokes this method but "test fixture" requirements might be. It seems like this is the only place "transmitter test channel" or "test channel" are used. The same entity is referred to as the "TP0-TP0v channel" in 163A.3.1.

SuggestedRemedy

Change the title of 163A.2 to "Test fixture" and replace its contents with the following: "The test fixture is between test points TP0 and TP0v as shown in Figure 163A-2. Test fixture requirements are specified by the clause that invokes this method."

Proposed Response Response Status O

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Cl 163 SC 163.9.2.3 P 179 L 39 # 31

Healey, Adam Broadcom Inc.

Comment Type T Comment Status X

It seems that "T_fx" should be 0 for TP0v-based ERL method given the test fixture is to be embedded and not de-embedded (and not time-domain gated).

SuggestedRemedy

Replace the following sentence "The value of Tfx is twice the delay from TP0 to TP0v." with "The value of T_fx is 0." A similar change would also be appropriate for 120F.3.1.1.

Proposed Response Response Status O

Cl 163 SC 163.9.2.3 P 179 L 44 # 32

Healey, Adam Broadcom Inc.

Comment Type E Comment Status X

"The reference for obtaining the reference ERL is defined in 163A.3.1." is an awkward sentence.

SuggestedRemedy

120F.3.1.1 has somewhat different wording and 163.9.2.3 could be changed to match. At a minimum, change the sentence to: "The reference transmitter ERL is defined in 163A.3.1."

Proposed Response Response Status O

Cl 120F SC 120F.3.1.1 P 209 L 6 # 33

Healey, Adam Broadcom Inc.

Comment Type E Comment Status X

The parameter is defined to be "dERL" and not "[DELTA]ERL".

SuggestedRemedy

Update the name to be consistent.

Proposed Response Response Status O

Cl 93A SC 93A.5.1 P 202 L 41 # 34

Healey, Adam Broadcom Inc.

Comment Type E Comment Status X

The notation used in Equation (93A-58a) is unnecessarily obscure. I assume it is intended to set $H_{tw}(f)$ to 1 when $tw = 0$ and to the Tukey window function when $tw = 1$.

SuggestedRemedy

Remove the "tw" qualification from the terms in Equation (93A-58a). Add a sentence that states that $H_{tw}(f)$ is defined by Equation (93-58a) when tw is 1 and $H_{tw}(f)$ is 1 when tw is 0 or is not defined. Remove the definition of "tw" from the variable list (page 203, line 12).

Proposed Response Response Status O

Cl 163A SC 163A.3.1 P 281 L 25 # 35

Healey, Adam Broadcom Inc.

Comment Type T Comment Status X

In Figure 163A-2, termination resistance at TP0v should represent an instrument and not a device (i.e., it should be the reference resistance R_0 and not the device resistance R_d).

SuggestedRemedy

Replace " R_0 " with " R_d ".

Proposed Response Response Status O

Cl 163A SC 163A.3.1.1 P 281 L 48 # 36

Healey, Adam Broadcom Inc.

Comment Type T Comment Status X

Equation (93-17) defines GAMMA1 and GAMMA2 to be equal and furthermore a function of R_d . The termination at the TP0v should represent an instrument load and therefore would be better defined to be R_0 independent of R_d .

SuggestedRemedy

Change the first paragraph of 163A.3.1.1 to the following: "Calculate the voltage transfer function, $H_{21}(f)$ from the scattering parameters of the virtual reference channel, $S^{\wedge}(0)$, using Equation (93A-18) where GAMMA1 is given by Equation (93A-17) and GAMMA2 is set to 0. In Equation (93A-17), the single-ended reference resistance R_0 is set to 50 [Ohms] and the single-ended termination resistance, R_d , specified by the clause that invokes this method."

Proposed Response Response Status O

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Cl 163A SC 163A.3.1.2 P 282 L 30 # 37

Healey, Adam Broadcom Inc.

Comment Type T Comment Status X

Equation (93A-58) and Equation (93A-59) do not calculate the PDTR response from $S^{(0)}$. There is an additional step required to obtain the reflection coefficient $s_{ii}(f)$ for the case where R_d is not equal to R_0 . Also, the value of T_{fx} should be 0.

SuggestedRemedy

Replace the contents of 163A.3.1.2 with the following: "The reference reflection coefficient at TP0v is given by Equation (93A-7) where $[s_{22}]^{(x)}$ is GAMMA1 as defined by Equation (93A-17) and $[s_{ij}]^{(y)}$ are the components of the scattering matrix of the virtual reference channel $S^{(0)}$. In Equation (93A-17), the single-ended reference resistance R_0 is set to 50 [Ohms] and the single-ended termination resistance, R_d , specified by the clause that invokes this method. The reference pulse time-domain reflection (PTDR) response is computed from the reference reflection coefficient at TP0v using Equation (93A-58) and Equation (93A-59). The reference ERL value is determined from the reference PTDR response using the method in 93A.5.2 with T_{fx} set to 0 and other parameters specified by the clause that invokes this method."

Proposed Response Response Status O

Cl 163A SC 163A.3.1.1 P 282 L 18 # 38

Healey, Adam Broadcom Inc.

Comment Type E Comment Status X

In Equation (163A-3), the upper limit of the summation (N_v) should have a capital "N". In addition, the unit interval symbol (T_b) should have a capital "T".

SuggestedRemedy

Fix the typos.

Proposed Response Response Status O

Cl 163A SC 163A.3.1.1 P 282 L 25 # 39

Healey, Adam Broadcom Inc.

Comment Type T Comment Status X

The annex is mostly written to be generic so citing the specific value for N_v defined in 162.9.3.1.2 seems out of place. Will the same value of N_v apply to future clauses that may employ this method?

SuggestedRemedy

Change the definition of N_v to the following: "represents the number of symbols to include in the steady state voltage calculation". Add a sentence that the value of N_v is defined by the clause that invokes this method.

Proposed Response Response Status O

Cl 163 SC 163.9.3.1 P 180 L 34 # 40

Healey, Adam Broadcom Inc.

Comment Type T Comment Status X

Now that the transmitter has relaxed test fixture requirements and taken a "test fixture embedding" approach, it seems appropriate for the receiver to follow suit.

SuggestedRemedy

Update 163.9.3.2 by changing references to "TP5a" to "TP5v" and add a pointer to 163.9.2.1 for test fixture requirements. Replace the specification of "ERL (min)" in Table 163-9 with a specification of "dERL" as is done for the transmitter and update 163.9.3.1 accordingly. Implement similar changes in Annex 120F. Update Annex 163A to include calculation of the reference ERL at TP5v (which should largely be a "mirror image" of the material currently describing the calculation of the reference ERL at TP0v). For interference tolerance and jitter tolerance test channel calibration, exceptions to 93A.2 and Annex 93C would need to be made to substitute TP0 to TP0v (and TP5v to TP5) replicas for their TP0 to TP0a (And TP5a to TP5) counterparts.

Proposed Response Response Status O

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CI 120G SC 120G.3.1 P 226 L 17 # 41

Healey, Adam Broadcom Inc.

Comment Type T Comment Status X

ESMW (eye symmetry mask width) is "TBD". Similarly, eye width specifications for stressed input parameters are also "TBD". These parameters will be difficult to define for a reference receiver that includes decision feedback equalization unless the behavior of the feedback signal in the vicinity of the threshold crossings is clearly defined. However, there are other, simpler means to enforce that the reference receiver output has a useable eye width. The most straight-forward implementation for this draft is to expand on a feature of the eye height and vertical eye closure measurement procedure referred to in 120G.5.2 item h). This items points to 120E.4.2 and 120E.4.3 for the method to measure eye height, vertical eye closure, and other parameters. Step 4) in 120E.4.3 states that the distribution of the signal voltage (from which eye height and vertical eye closure are derived) is to be measured over a window "within 0.025 UI of time TCmid". This essentially averages the distribution over the time window or, thought of a different way, is similar to having a uniform jitter distribution around TCmid. Use of such a window reduces the measured eye height and vertical eye closure for signals with narrower eye widths. The width of the window can be increased to provide higher degrees of protection.

SuggestedRemedy

Remove references to ESMW and eye height from Annex 120G. Change 120G.5.2 item h) to the following: "From the eye diagram, compute eye height and vertical eye closure using the methodologies defined in 120E.4.2 and 120E.4.3 with the following exceptions. The value of TCmid is set to the sampling phase t_s determined in step d) (skipping steps 1) through 3) from 120E.4.2). The CDFs of the signal voltages computed in 120E.4.2 steps 4) through 6) are the average values over the time interval $t_s - 0.05$ UI to $t_s + 0.05$ UI. The feedback coefficients $b(n)$ determined in step d) are constant over the averaging time interval."

Note that eye height and vertical eye closure limits may need to be adjusted to account for the reductions to these values via the averaging window.

Proposed Response Response Status

CI 163 SC 163.9.2 P 176 L 35 # 42

Healey, Adam Broadcom Inc.

Comment Type T Comment Status X

The signaling rate range can be reduced to +/-50 ppm with minimal impact to the overall cost of the system. A lower signaling rate range can be leveraged by implementations to improve performance margin. However, interoperability with implementations that use 50 Gb/s/lane (and lower) AUIs must be preserved. The proposed changes encourage migration to higher-precision frequency references while maintaining compatibility with prior implementations with up +/-100 ppm tolerance.

SuggestedRemedy

This proposed change leverages terms from Clause 45 that describe how MDIO manageable devices are organized in the Physical Layer stack. The first is the idea that sublayers may be in the same "package" or in different packages (see IEEE Std 802.3-2018 45.1.1). The definition of a "package" is vendor specific (could be a chip, module, or other entity). The second is that a PMA that is not in the same package as the PMD is designated as a "separated PMA" (see IEEE Std 802.3-2018, 45.2.1). The third concept that is important to the proposed definition is that a PMA, by itself, has no control over the signaling rate tolerance. The frequency offset at the PMA output is inherited from the PMA input. Since the PMA has no control over this, it does not make sense to impose a specification on the PMA signaling rate range except for specific circumstances. Similar arguments can be made for PMD outputs as they inherit the frequency precision from the PMA.

In Table 162-9, Table 163-5, Table 120F-1, and Table 120G-1, change "signaling rate" (or "signaling rate per lane (range)") to 53.125 +/- 50 ppm and add a footnote to indicate 1) that the +/-50 ppm tolerance applies to PMA (and PMD) that are in the same package as the PCS and 2) that in other cases, the signaling rate is related to the signaling rate from the higher (separated PMA) sublayer.

In Table 120G-3, change "signaling rate per lane (range)" to "signaling rate per lane" with a value of 53.125. In 120G.3.1.1 (and/or a footnote to Table 120G-3), state the signaling rate tolerance at the module output is inherited from the PMD receiver input.

Also change 120G.3.1.1 to agree with changes Table 120G-1 and Table 120G-3.

No change to the input signaling rate range requirements in Table 162-12, Table 120G-4, and Table 120G-7 is needed because they continue to represent the largest extent of the signaling rate range for all allowed configurations of the Physical Layer stack.

Add a recommendation (to either Annex 120A or Annex 135A) that the signaling rate tolerance of the output of a "legacy" PCS/PMA (interface is not 100GAUI-1, 200GAUI-2, or 400GAUI-4) be constrained to +/-50 ppm when used with a separated PMA that has a 100GAUI-1, 200GAUI-2, or 400GAUI-4 interface.

Proposed Response Response Status

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Cl 45 SC 45.2.1.135a P 54 L 11 # 43
 Slavick, Jeff Broadcom
 Comment Type TR Comment Status X
 We've added a footnote stating that the new PRESETs are PHY dependent support, so is C(-3).
 SuggestedRemedy
 Add a footnote to Tables 45-103a, 45-103b, 45-103c and 45-104d attached to the Coefficient Select and Coefficient Select Echo text stating "Support for a given coefficient is PHY dependent."
 Proposed Response Response Status O

Cl 162 SC 162.9.3.1.5 P 150 L 20 # 44
 Slavick, Jeff Broadcom
 Comment Type TR Comment Status X
 When testing how small you can make the signal there is no constraint on the other tap settings.
 SuggestedRemedy
 Add the following to the start of the sentence "With c(-3), c(-2), c(-1) and c(1) set to zero and c(0)"
 Proposed Response Response Status O

Cl 162 SC 162.9.3.1.5 P 150 L 20 # 45
 Slavick, Jeff Broadcom
 Comment Type E Comment Status X
 The order of the ranges tests was +1, -1, -2, -3 prior to add 0, but we placed 0 at the end instead of in it's position in the descending list.
 SuggestedRemedy
 Move the requirement for testing c(0) range to be the third paragraph (between +1 and -1)
 Proposed Response Response Status O

Cl 162 SC 162.1 P 133 L 17 # 46
 Ran, Adele Intel
 Comment Type E Comment Status X
 Incorrect cross reference "Figure 162-3"
 SuggestedRemedy
 Change to "Table 162-3"
 Proposed Response Response Status O

Cl 162 SC 162.9.3 P 146 L 42 # 47
 Ran, Adele Intel
 Comment Type T Comment Status X
 (CC)
 for c(0), PRESET 2 in Table 162-11 has a value of 0.5 (+/-half of a step). To enable this value, the maximum value at minimum state should be no higher than 0.5.
 Change should also be applied in 162.9.3.1.5.
 Also applies to KR, Table 163-5 (163.9.2) and to AUI-C2C, Table 120F-1 (120F.3.1.1) which should work over lower-loss channels.
 SuggestedRemedy
 Change 0.54 to 0.5, in all places listed in the comment.
 Proposed Response Response Status O

IEEE P802.3ck D1.3 100/200/400 Gb/s Electrical Interfaces Task Force 4th Task Force review comments

CI 162 SC 162.9.3 P 146 L 48 # 48

Ran, Adeo Intel
 Comment Type T Comment Status X

(CC)
 The even-odd jitter limit of 0.019 UI (less than 360 fs) was not met by several different transmitters tested in lab environment. The same parts showed good link performance over challenging channels.

This requirement seems difficult to meet and not too important for interoperability. It seems that much higher EOJ can be tolerated by existing receivers.

For reference, in multiple generations of NRZ PMDs the allowed EOJ is 0.035 UI; for C2M and for optical PMDs it is not defined at all.

Also applies to KR, Table 163-5 (163.9.2) and to AUI-C2C, Table 120F-1 (120F.3.1.1)

SuggestedRemedy

For parameter "Even-odd jitter, pk-pk" change "value" from 0.019 to 0.035, in all places listed in the comment.

Proposed Response Response Status O

CI 162 SC 162.9.3 P 147 L 1 # 49

Ran, Adeo Intel
 Comment Type T Comment Status X

Footnote d includes important information for measurement that should be stated in the test procedure, not as a comment on the table (it does not change the specification).

SuggestedRemedy

Delete footnote d and instead add an informative NOTE in 162.9.3.3 (which is referred to by clause 163 and should also be used for 120F).

Also delete footnote e in Table 163-5.

Proposed Response Response Status O

CI 162 SC 162.9.3.1.4 P 149 L 43 # 50

Ran, Adeo Intel
 Comment Type E Comment Status X

"When coef_sel is -3, -2, -1, 0, or 1," - the list includes all possible values, so there is no need for this phrase.

SuggestedRemedy

Delete the quoted phrase.

Proposed Response Response Status O

CI 162 SC 162.9.3.1.5 P 150 L 20 # 51

Ran, Adeo Intel
 Comment Type E Comment Status X

(0) is set in italics

SuggestedRemedy

set to upright

Proposed Response Response Status O

IEEE P802.3ck D1.3 100/200/400 Gb/s Electrical Interfaces Task Force 4th Task Force review comments

CI 162 SC 162.9.3.3 P 150 L 40 # 52

Ran, Adeo Intel

Comment Type T Comment Status X

The method in 120D.3.1.8.2 is very specific about using PRBS13Q.

Physical measurements of even-odd jitter with PRBS13Q at 53.125 GBd show a much wider distribution and larger values compared with shorter test patterns.

Since even-odd jitter is inherently a high frequency effect (fb/2), this variability seems to be a measurement artifact. The considerations mentioned in NOTE 1 of 120D.3.1.8.2 may be limiting the accuracy of measurements at this signaling rate.

If a device can be tested with a shorter pattern which enables calculation of even-odd jitter, the measurement can be made more accurate; such results should be acceptable.

The comment also applies to 120F.3.1.3.

SuggestedRemedy

Add the following exception in 162.9.3.3:

The pattern used for Even-odd jitter measurement may be PRBS13Q or any shorter odd-length pattern that includes the 12 possible transitions between two different PAM4 symbols.

In 120F.3.1.3, change the cross-reference for EOJ measurement from 120D.3.1.8.2 to 162.9.3.3.

Proposed Response Response Status O

CI 93A SC 93A.1.2.3 P 199 L 14 # 53

Ran, Adeo Intel

Comment Type T Comment Status X

Equation 93A-12A has a typo - denominator should be a sum (as in equation 93A-12).

SuggestedRemedy

Change "-" to "+" in the denominator.

Proposed Response Response Status O

CI 120F SC 120F.3.1 P 208 L 14 # 54

Ran, Adeo Intel

Comment Type E Comment Status X

Reference to dERL in the table should be the subclause that specifies parameters and points to the annex.

SuggestedRemedy

Change reference for dERL in table 120F-1 from 163A.3.2.2 to 120F.3.1.1.

Proposed Response Response Status O

CI 120F SC 120F.3.1.1 P 209 L 6 # 55

Ran, Adeo Intel

Comment Type E Comment Status X

Delta sign appears here (Δ ERL) but the difference term is called dERL.

Also on line 26.

SuggestedRemedy

Change Delta to d in both cases.

Proposed Response Response Status O

CI 120F SC 120F.3.1.1 P 209 L 4 # 56

Ran, Adeo Intel

Comment Type E Comment Status X

Subclause heading "Transmitter effective return loss" should be consistent with "Transmitter ERL" in 163.9.2.3.

SuggestedRemedy

Change heading to "Transmitter ERL".

Proposed Response Response Status O

IEEE P802.3ck D1.3 100/200/400 Gb/s Electrical Interfaces Task Force 4th Task Force review comments

Cl 163A SC 163A.3.1.1 P 282 L 5 # 57
 Ran, Adeo Intel
 Comment Type E Comment Status X
 In "Tr" r should be in subscript.
 SuggestedRemedy
 per comment.
 Proposed Response Response Status O

Cl 163A SC 163A.3.1 P 281 L 40 # 58
 Ran, Adeo Intel
 Comment Type T Comment Status X
 "The scattering parameters for the reference package, S(tp), are determined using the method in 93A.1.2, with electrical characteristics specified in the clause that invokes this method"
 Typically there are two reference package for the Tx and two possibly other ones for the Rx. It is not stated which one should be used.
 A DUT should be allowed to be as "bad" as the worst of the two reference packages for any of the parameters.
 Editorially it seems that this should be stated separately in 163A.3.1.1 for v_peak and v_f and in 163A.3.1.2 for ERL (although the same rule applies in both cases).
 SuggestedRemedy
 Add a sentence in 163A.3.1.1 after the paragraph "The reference pulse response peak (...) is the peak value of h(t)"
 such as the following:
 "If the invoking clause lists more than one set of reference package parameters, the calculation is performed with each set, and the minimum value is used as the reference value."
 Add a similar sentence at the end of 163A.3.1.1 (after the definition of v_f(ref)) and at the end of 163A.3.1.2 (for ERL reference).
 Proposed Response Response Status O

Cl 163A SC 163A.3.2.2 P 283 L 12 # 59
 Ran, Adeo Intel
 Comment Type E Comment Status X
 Both ERL(ref) and ERL(meas) in equation 163A-6 are undefined terms.
 SuggestedRemedy
 Add below the equation
 "Where
 ERL(ref) is the ERL reference value defined in 163A.3.1.2
 ERL(meas) is the measured Effective return loss"
 Proposed Response Response Status O

Cl 163 SC 163.9.2 P 176 L 44 # 60
 Ran, Adeo Intel
 Comment Type E Comment Status X
 Reference to dERL in the table should be the subclause that specifies parameters and points to the annex.
 SuggestedRemedy
 Change reference for dERL in Table 163-5 from 163A.3.2.2 to 163.9.2.3.
 Proposed Response Response Status O

IEEE P802.3ck D1.3 100/200/400 Gb/s Electrical Interfaces Task Force 4th Task Force review comments

CI 163 SC 163.9.2 P 176 L 44 # 61

Ran, Adeo Intel
 Comment Type T Comment Status X

Table 163-5 has multiple TBDs.

Reference ERL, v_f and v_{peak} are calculated with an idealized package model. Real products deviate from this model, so the limit values may need adjustment.

v_f and v_{peak} may be degraded by a device or package, but that can be mitigated using higher than minimum launch voltage and some equalization. So for dv_f and dv_{peak} , a minimum of 0 V may be acceptable.

There is no straightforward method to improve ERL. So to allow a wide range of implementations, the minimum dERL should be less than 0 dB. A minimum of -3 dB may be acceptable.

SuggestedRemedy

Change value for dv_f in Table 163-5 from TBD to 0.

Change value for dv_{peak} in Table 163-5 from TBD to 0.

Change value for dERL in Table 163-5 from TBD to -3.

Proposed Response Response Status O

CI 163 SC 163.9.2 P 176 L 48 # 62

Ran, Adeo Intel
 Comment Type T Comment Status X

dv_f and dv_{peak} refer directly to 163A.3.2.1, but some parameters are missing for the calculations:

A_t - should be taken from table 163-11 (or specify as the value 0.4 V)

z_p - should be the maximum value from table 163-11

SuggestedRemedy

Add a subclause under 163.9.2 (similar to 163.9.2.3 for dERL) to define the calculation of dv_f and dv_{peak} ; in that subclause, point to 163A.3.2.1 and supply the required parameters as in the comment.

Proposed Response Response Status O

CI 163 SC 163.9.2 P 177 L 5 # 63

Ran, Adeo Intel
 Comment Type E Comment Status X

abs step size " for c(-3), c(-2), c(-1), c(0), and c(1)"

This list includes all possible values, so it is redundant. Clause 162 has "for all taps" instead.

SuggestedRemedy

Change the quoted words to "for all taps", both for min and for ax.

Proposed Response Response Status O

CI 163 SC 163.9.2.1.1 P 177 L 48 # 64

Ran, Adeo Intel
 Comment Type T Comment Status X

ILD definition in 93A.4 should be cross referenced.

This definition requires some parameters. Specifically the transition time T_t , which should correspond to the observable transition time at TP0 (larger than the internal value).

SuggestedRemedy

Append "Insertion loss deviation is calculated as specified in 93A.4, where T_t is 0.1 ns, and f_b and f_t values are taken from Table 163-11."

Proposed Response Response Status O

IEEE P802.3ck D1.3 100/200/400 Gb/s Electrical Interfaces Task Force 4th Task Force review comments

CI 163 SC 163.9.2.1.2 P 178 L 21 # 65

Ran, Adeo Intel

Comment Type T Comment Status X

Per resolution of comment 154 against D1.2 there should be a requirement on test fixture ERL:

"The ERL at TP0v shall be greater than or equal to TBD".

This part has not been implemented.

With N=20 the ERL of the test fixture is expected to be very good. The TBD may be changed to 15 dB (same as in clause 137) if there is consensus.

SuggestedRemedy

Add the following sentence after the table"

"The ERL at TP0v shall be greater than or equal to TBD dB".

Consider changing TBD to 15 dB.

Proposed Response Response Status O

CI 163 SC 163.9.2.3 P 179 L 43 # 66

Ran, Adeo Intel

Comment Type E Comment Status X

"The reference for obtaining the reference"

SuggestedRemedy

Change to "The method for obtaining the reference"

Proposed Response Response Status O

CI 163 SC 163.9.3.1 P 180 L 33 # 67

Ran, Adeo Intel

Comment Type T Comment Status X

The method of Annex 163A can be used for receiver ERL just like it is for transmitter ERL, that is, specify difference from a reference value.

In the case of the receiver, there may be a tradeoff between optimizing for ERL and optimizing for BER. The receiver should be allowed more design freedom. Therefore the minimum dERL should be lower than for the receiver.

A minimum dERL of -5 dB may be acceptable. Alternatively, dERL can be made informative (recommendation).

Also applies to 120F.3.2.1.

SuggestedRemedy

Change receiver ERL subclause (163.9.3.1) to match 163.9.2.3.

In Table 163-9, change ERL (min) to dERL(Min) with value -5 dB.

Change subclause 120F.3.2.1 to match 163.9.3.1 (apply the change above).

In Table 120F-4, change ERL (min) to dERL(Min) with value -5 dB.

Consider changing Rx dERL from a normative specification (shall) to a recommendation (should).

Proposed Response Response Status O

CI 163 SC 163.9.3.2 P 181 L 3 # 68

Ran, Adeo Intel

Comment Type T Comment Status X

Receiver test fixture defined here is not realistic (IL of 1.2-1.6 dB at 25.56 GHz). The test fixture specification should be similar to the transmitter's test fixture.

SuggestedRemedy

Change the receiver test fixture subclause (163.9.3.2) to match 163.9.2.1 or point to it.

Proposed Response Response Status O

IEEE P802.3ck D1.3 100/200/400 Gb/s Electrical Interfaces Task Force 4th Task Force review comments

Cl 163 SC 163.9.3.2 P 181 L 3 # 69

Ran, Adeo Intel

Comment Type E Comment Status X

The receiver test fixture characteristics should be defined before the measurements performed with it, as in the transmitter. Currently Receiver ERL appears first.

SuggestedRemedy

Move subclause 163.9.3.2 before 163.9.3.1.

Proposed Response Response Status O

Cl 163 SC 163.9.3.3 P 181 L 34 # 70

Ran, Adeo Intel

Comment Type T Comment Status X

The exception that "transmitter equalization is configured by management..." is taken from the AUI-C2C (Annex 120D) which does not have a training protocol.

This clause is for the KR PMD that does have a training protocol defined, so this exception is out of place. The procedure in Annex 93C should be used as is.

SuggestedRemedy

Delete the sentence "with the exception that transmitter equalization is configured by management (see 120D.3.2.3) to the settings that provide the lowest FEC symbol error ratio".

Proposed Response Response Status O

Cl 163 SC 163.9.3.3 P 181 L 42 # 71

Ran, Adeo Intel

Comment Type T Comment Status X

In item b, Equation 163-2 is a calculation of A_DD, not related to return loss.

The transmitter's test fixture only has an ERL spec, and that is defined from TP0v towards the DUT. It is not an appropriate ERL for TP5 replica (e.g. has only N=20 UI).

The breakout from the package is typically controlled by the PMD's vendor and is practically part of the DUT. Therefore we should not add ERL specifications for the TP5 replica - they may be irrelevant and even incorrect for a specific implementation.

This is similar to the case of a transmitter's test fixture where ERL is specified toward the DUT, but not from the DUT toward TP0v.

Instead, the test channel's ERL should be specified to meet the ERL specifications in 163.10.3.

Also applies in 120F.3.2.3 item b which has "The return loss of the test setup in Figure 93C-4 measured at TP5 replica towards TPt meets the return loss specifications in 163.9.2.1" - but there are no return loss specifications in 163.9.2.1 anymore.

SuggestedRemedy

Replace item b with the following:

The return loss of the test channel measured at TP5a towards TPt meets the requirements in 163.10.3.

Apply similar change in 120F.3.2.3 with the reference to requirements in 120F.4.3 instead.

Proposed Response Response Status O

Cl 163 SC 163.9.3.3 P 182 L 5 # 72

Ran, Adeo Intel

Comment Type E Comment Status X

In item e), the phrase "where Q3 is 3.2905" should be moved below the equations, with and explanation of what Q3 stands for (as in 136.9.4.2.3).

Alternatively, the equations can be replaced by cross reference to equations 136-8 and 136-9.

SuggestedRemedy

per comment.

Proposed Response Response Status O

IEEE P802.3ck D1.3 100/200/400 Gb/s Electrical Interfaces Task Force 4th Task Force review comments

Cl 163 SC 163.9.2.2 P 178 L 28 # 73

Brown, Matt Huawei
 Comment Type T Comment Status X

The example test fixture using TP0a is no longer required. See the following ad hoc presentation;
https://www.ieee802.org/3/ck/public/adhoc/sept16_20/brown_3ck_adhoc_01a_091620.pdf

SuggestedRemedy

Remove 163.9.2.2 and reference TP0v instead of TP0a for all transmitter specifications for KR (Clause 163) and C2C (Annex 120F).

Proposed Response Response Status O

Cl 163 SC 163.9.2.3 P 179 L 44 # 74

Brown, Matt Huawei
 Comment Type E Comment Status X

Wording

SuggestedRemedy

Change "The reference for obtaining" to "The method for obtaining".

Proposed Response Response Status O

Cl 163 SC 163.9.3.2 P 181 L 1 # 75

Brown, Matt Huawei
 Comment Type E Comment Status X

The test fixture should be defined before defining test specifications and methods. As was done for the TX test fixture subclause, move the RX TF subclause to before the ERL subclause.

SuggestedRemedy

Move 163.9.3.2 ahead of 163.9.3.1.

Proposed Response Response Status O

Cl 93A SC 93A.5.1 P 202 L 45 # 76

Brown, Matt Huawei
 Comment Type T Comment Status X

The variable f_r used in equation 93A-58b is not included in the associated variable list.

SuggestedRemedy

Add fr and its definition to the variable list below Equation 93A-58b.

Proposed Response Response Status O

Cl 120F SC 120F.3.1.1 P 209 L 14 # 77

Brown, Matt Huawei
 Comment Type E Comment Status X

The parameter name "Difference between measured and reference effective return loss" is a real mouthful. A more concise name would be beneficial.

SuggestedRemedy

Change "Difference between measured and reference effective return loss" to "difference effective return loss". Apply throughout 163, 120F, and 163A.

Proposed Response Response Status O

Cl 120F SC 120F.3.1.1 P 209 L 18 # 78

Brown, Matt Huawei
 Comment Type E Comment Status X

The parameter name "Difference between measured and reference steady-state voltage" is a real mouthful. A more concise name would be beneficial.

SuggestedRemedy

Change "Difference between measured and reference steady-state voltage" to "difference steady-state voltage". Apply throughout 163, 120F, and 163A.

Proposed Response Response Status O

IEEE P802.3ck D1.3 100/200/400 Gb/s Electrical Interfaces Task Force 4th Task Force review comments

CI 120F SC 120F.3.1.1 P 209 L 21 # 79

Brown, Matt Huawei
 Comment Type E Comment Status X

The parameter name "Difference between measured and reference linear fit pulse peak" is a real mouthful. A more concise name would be beneficial.

SuggestedRemedy

Change "Difference between measured and reference linear fit pulse peak" to "linear fit pulse peak". Apply throughout 163, 120F, and 163A.

Proposed Response Response Status O

CI 120F SC 120F.3.1.1 P 209 L 6 # 80

Brown, Matt Huawei
 Comment Type E Comment Status X

delta_ERL should be dERL.

SuggestedRemedy

Replace all instances of delta_ERL with dERL.

Proposed Response Response Status O

CI 163 SC 163.9.3.2 P 181 L 1 # 81

Brown, Matt Huawei
 Comment Type T Comment Status X

In Draft 1.3, the transmitter test fixture specification (TP0 to TP0a) was replaced with a new test fixture specification (TP0 to TP0v). The receiver test fixture should be rewritten to match the new transmitter test fixture specification.

SuggestedRemedy

Align the receiver test fixture specification with the new transmitter test fixtures specification based upon slide 12 of the following presentation:
https://www.ieee802.org/3/ck/public/adhoc/sept16_20/brown_3ck_adhoc_01a_091620.pdf
 In 163 and 120F, replace all references to TP5a with TP5v.

Proposed Response Response Status O

CI 120F SC 120F.3.1 P 208 L 14 # 82

Brown, Matt Huawei
 Comment Type T Comment Status X

A value for dERL is required. If an appropriate reference transmitter is defined, then a value of 0 should be correct.

SuggestedRemedy

Replace TBD with 0.

Proposed Response Response Status O

CI 120F SC 120F.3.1 P 208 L 18 # 83

Brown, Matt Huawei
 Comment Type T Comment Status X

A value for dv_f is required. If an appropriate reference transmitter is defined, then a value of 0 should be correct.

SuggestedRemedy

Replace TBD with 0.

Proposed Response Response Status O

CI 120F SC 120F.3.1 P 208 L 21 # 84

Brown, Matt Huawei
 Comment Type T Comment Status X

A value for dv_peak is required. If an appropriate reference transmitter is defined, then a value of 0 should be correct.

SuggestedRemedy

Replace TBD with 0.

Proposed Response Response Status O

IEEE P802.3ck D1.3 100/200/400 Gb/s Electrical Interfaces Task Force 4th Task Force review comments

CI 120F SC 120F.3.2.1 P 211 L 40 # 85
 Brown, Matt Huawei
 Comment Type T Comment Status X
 The receiver ERL should be defined and measured in the same way as for the transmitter.
SuggestedRemedy
 Assuming that the receiver test fixture is aligned with the transmitter test fixture, specify the receiver ERL using the same specification as the transmitter ERL using dERL in 120F.3.1.1. In Table 120F-3, replace the the parameter name and set the specification to 0 dB.
 Proposed Response Response Status O

CI 120F SC 120F.3.2.3 P 213 L 1 # 86
 Brown, Matt Huawei
 Comment Type T Comment Status X
 For the SNDR measurement in item e) of receiver interference tolerance test considerations the value for N_p is not set.
SuggestedRemedy
 Replace TBD with an appropriate value.
 Proposed Response Response Status O

CI 120F SC 120F.4.3 P 217 L 44 # 87
 Brown, Matt Huawei
 Comment Type T Comment Status X
 The ERL value is specified as TBD.
SuggestedRemedy
 Replace TBD with an appropriate value.
 Proposed Response Response Status O

CI 120G SC 120G.3.1 P 226 L 17 # 88
 Brown, Matt Huawei
 Comment Type T Comment Status X
 Host output eye symmetry mask width (ESMW) value is TBD. Discussion during D1.2 comment resolution revealed that an eye width measurement using the currently defined reference receiver and related methodology as defined is not meaningful.
SuggestedRemedy
 Either fix the methodology and provide a value or replace with an appropriate alternative specification.
 Proposed Response Response Status O

CI 120G SC 120G.3.1 P 226 L 17 # 89
 Brown, Matt Huawei
 Comment Type T Comment Status X
 In Table 120G-1, the reference for host output eye symmetry mask width (ESMW) value points to 120G.3.1.6. However, 120G.3.1.6 does not specify how to measure ESMW or what to do with it.
SuggestedRemedy
 In 120G.3.1.6, add methodology for ESMW and explain the relevance.
 Proposed Response Response Status O

CI 120G SC 120G.3.1 P 226 L 23 # 90
 Brown, Matt Huawei
 Comment Type T Comment Status X
 The host output ERL value is TBD.
SuggestedRemedy
 Replace TBD with an appropriate value.
 Proposed Response Response Status O

IEEE P802.3ck D1.3 100/200/400 Gb/s Electrical Interfaces Task Force 4th Task Force review comments

Cl 120G SC 120G.3.1 P 226 L 26 # 91

Brown, Matt Huawei
 Comment Type T Comment Status X

The host output minimum transition time value is TBD. Since the transition time is measured after considerable loss and parasitics between the host device and the measurement point it seems unnecessary to specify this parameter.
 Alternately, use the transition time used in the the various COM simulations (7.5 ps).

SuggestedRemedy

Delete the host output transition time.
 Alternately replace TBD with 7.5 ps.

Proposed Response Response Status O

Cl 120G SC 120G.3.1.6 P 228 L 24 # 92

Brown, Matt Huawei
 Comment Type T Comment Status X

The parameter values for the host output eye opening crosstalk source are TBD as follows: "The crosstalk generator is calibrated at TP4 (without the use of a reference receiver) with target differential peak-to-peak amplitude of TBD mV and slew time of TBD ps between -TBD V and +TBD V." Use the maximum peak to peak value from Table 120G-1, range of 20% to 80%, and minimum transition time from Table 120G-1 (value proposed in another comment).

SuggestedRemedy

Replace with the following:
 The crosstalk generator is calibrated at TP4 (without the use of a reference receiver) with target differential peak-to-peak amplitude of 870 mV and slew time of 7.5 ps between -261 V and +261 V.

Proposed Response Response Status O

Cl 120G SC 120G.3.2 P 229 L 17 # 93

Brown, Matt Huawei
 Comment Type T Comment Status X

Module output near-end and far-end eye symmetry mask width (ESMW) values are TBD. Discussion during D1.2 comment resolution revealed that an eye width measurement using the currently defined reference receiver and related methodology as defined is not meaningful.

SuggestedRemedy

Either fix the methodology and provide a value or replace with an appropriate alternative specification.

Proposed Response Response Status O

Cl 120G SC 120G.3.2 P 229 L 17 # 94

Brown, Matt Huawei
 Comment Type T Comment Status X

In Table 120G-3, the reference for module output near-end and far-end eye symmetry mask width (ESMW) points to 120G.3.1.6. However, 120G.3.1.6 does not specify how to measure ESMW or what to do with it.

SuggestedRemedy

In 120G.3.1.6, add methodology for ESMW and explain the relevance.

Proposed Response Response Status O

Cl 120G SC 120G.3.2 P 229 L 29 # 95

Brown, Matt Huawei
 Comment Type T Comment Status X

The module output ERL value is TBD.

SuggestedRemedy

Replace TBD with an appropriate value.

Proposed Response Response Status O

IEEE P802.3ck D1.3 100/200/400 Gb/s Electrical Interfaces Task Force 4th Task Force review comments

CI 120G SC 120G.3.2 P 229 L 26 # 96
 Brown, Matt Huawei
 Comment Type T Comment Status X
 Module output far-end pre-cursor ISI ratio value is TBD. The related measurement methodology was rewritten in D1.3.
 SuggestedRemedy
 Replace TBD with an appropriate value.
 Proposed Response Response Status O

CI 120G SC 120G.3.3 P 231 L 43 # 99
 Brown, Matt Huawei
 Comment Type T Comment Status X
 The host input ERL value is TBD.
 SuggestedRemedy
 Replace TBD with an appropriate value.
 Proposed Response Response Status O

CI 120G SC 120G.3.2 P 229 L 32 # 97
 Brown, Matt Huawei
 Comment Type T Comment Status X
 The module output minimum transition time value is TBD. Since the transition time is measured after considerable loss and parasitics between the host device and the measurement point it seems unnecessary to specify this parameter.
 Alternately, use the transition time used in the the various COM simulations (7.5 ps).
 SuggestedRemedy
 Delete the host output transition time.
 Alternately replace TBD with 7.5 ps.
 Proposed Response Response Status O

CI 120G SC 120G.3.3.2 P 232 L 18 # 100
 Brown, Matt Huawei
 Comment Type T Comment Status X
 In Table 120G-6 for host input stressed signal the value for eye width is TBD.
 SuggestedRemedy
 Replace TBD with an appropriate value.
 Proposed Response Response Status O

CI 120G SC 120G.3.2.2 P 230 L 14 # 98
 Brown, Matt Huawei
 Comment Type T Comment Status X
 The parameter values for the module output eye opening crosstalk source are TBD as follows:
 "The crosstalk generator is calibrated at TP1a (without the use of a reference receiver) with target differential peak-to-peak amplitude of TBD mV and target transition time of TBD ps."
 Use the maximum peak to peak value and minimum transition time value (proposed in another comment) from Table 120G-1.
 SuggestedRemedy
 Replace with the following:
 "The crosstalk generator is calibrated at TP1a (without the use of a reference receiver) with target differential peak-to-peak amplitude of 900 mV and target transition time of 7.5 ps."
 Proposed Response Response Status O

CI 120G SC 120G.3.3.2 P 232 L 18 # 101
 Brown, Matt Huawei
 Comment Type T Comment Status X
 In Table 120G-6 for host input stressed signal there are specifications for both far-end eye symmetry mask width (ESMW) and eye width (EW). ESMW is not mentioned in the stressed input procedure nor does it seem relevant.
 SuggestedRemedy
 Delete ESMW row in Table 120G-6.
 Proposed Response Response Status O

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CI 120G SC 120G.5.2 P 241 L 23 # 102

Brown, Matt Huawei
 Comment Type T Comment Status X

For each C2M interface, there is a specification for eye symmetry mask width (ESMW) and there is a pointer to 120G.5.2. However, 120G.5.2 does not specify a method for ESMW; it specifies a method only EH, EW, and VEC. ESMW is discussed in 120E.4.2, but even there its not really clear what to do with it.

SuggestedRemedy
 Add methodology for ESMW and explain the relevance.

Proposed Response Response Status O

CI 120G SC 120G.3.3.2.1 P 233 L 32 # 103

Brown, Matt Huawei
 Comment Type T Comment Status X

For the host stressed input the crosstalk source transition parameters are TBD as follows: "The counter propagating crosstalk signals during calibration of the stressed signal are asynchronous with target amplitude of TBD mV peak-to-peak differential and 20% to 80% target transition time of TBD ps as measured at TP1a (without the use of a reference receiver)." Set amplitude to the host output maximum value and set the transition time to the host output minimum value.

SuggestedRemedy
 Change the sentence to the following:
 "The counter propagating crosstalk signals during calibration of the stressed signal are asynchronous with target amplitude of 870 mV peak-to-peak differential and 20% to 80% target transition time of 7.5 ps as measured at TP1a (without the use of a reference receiver)."

Proposed Response Response Status O

CI 120G SC 120G.3.4 P 235 L 11 # 104

Brown, Matt Huawei
 Comment Type T Comment Status X

The module input ERL value is TBD.

SuggestedRemedy
 Replace TBD with an appropriate value.

Proposed Response Response Status O

CI 120G SC 120G.3.4.1 P 231 L 35 # 105

Brown, Matt Huawei
 Comment Type T Comment Status X

In Table 120G-9 for module input stressed signal the value for eye width is TBD.

SuggestedRemedy
 Replace TBD with an appropriate value.

Proposed Response Response Status O

CI 120G SC 120G.3.3.2 P 232 L 18 # 106

Brown, Matt Huawei
 Comment Type T Comment Status X

In Table 120G-9 for host input stressed signal there are specifications for both far-end eye symmetry mask width (ESMW) and eye width (EW). ESMW is not mentioned in the stressed input procedure nor does it seem relevant.

SuggestedRemedy
 Delete ESMW row in Table 120G-6.

Proposed Response Response Status O

CI 120G SC 120G.3.4.1.1 P 236 L 15 # 107

Brown, Matt Huawei
 Comment Type T Comment Status X

For the module input stressed eye, the pattern generator transition time value is TBD as follows:
 "The target pattern generator 20% to 80% transition time at the input to the test channel in the module stressed input test is TBD ps."

SuggestedRemedy
 Replace TBD with 7.5 ps.

Proposed Response Response Status O

IEEE P802.3ck D1.3 100/200/400 Gb/s Electrical Interfaces Task Force 4th Task Force review comments

CI 120G SC 120G.3.4.1.1 P 236 L 47 # 108

Brown, Matt Huawei
 Comment Type T Comment Status X

The parameter values for the module input eye opening crosstalk source are TBD as follows:
 "The counter propagating crosstalk signals during calibration of the stressed signal are asynchronous with target amplitude of TBD mV peak-to-peak differential and target slew time between -TBD mV and TBD mV of TBD ps as measured at TP4 (without the use of a reference equalizer)."
 Use the maximum peak to peak value from Table 120G-3, range of 20% to 80%, and minimum transition time from Table 120G-3 (value proposed in another comment).

SuggestedRemedy

Replace with the following:
 The crosstalk generator is calibrated at TP4 (without the use of a reference receiver) with target differential peak-to-peak amplitude of 900 mV and slew time of 7.5 ps between -270 V and +270 V.

Proposed Response Response Status O

CI 120G SC 120G.3.4.1.1 P 237 L 14 # 109

Brown, Matt Huawei
 Comment Type T Comment Status X

For the module input stressed eye high-loss case the criteria to have CTLE setting greater than a certain value is not relevant because: (a) there are two gain parameters and (b) the reference receiver includes a DFE. Regardless, the minimum CTLE setting value is TBD.

SuggestedRemedy

Either:
 (a) delete the following text:
 "This CTLE setting has to be greater than or equal to TBD dB." on line 13, and
 "except that the restriction that the CTLE setting has to be greater than or equal to TBD dB does not apply" on line 18
 OR
 (b) provide an alternate relevant criteria.

Proposed Response Response Status O

CI 162 SC 162.11 P 156 L 37 # 110

Champion, Bruce TE Connectivity
 Comment Type T Comment Status X

Cable Assembly ERL listed as TBD in Table 162-16

SuggestedRemedy

TBD to be changed to 7.4 dB. See presentation

Proposed Response Response Status O

CI 162 SC 162.11.5 P 157 L 52 # 111

Champion, Bruce TE Connectivity
 Comment Type T Comment Status X

Cable assembly differential to common-mode conversion loss requirements are listed as TBD

SuggestedRemedy

A limit should be specified by an equation. It is recommended to use the following equation for this limit:

$$\begin{aligned} \text{SCD21}(f)\text{-SDD21}(f) &\geq 10 \text{ for } 0.05 \leq f < 12.89 \\ \text{SCD21}(f)\text{-SDD21}(f) &\geq 14 - 0.3108 * f \text{ for } 12.89 \leq f \leq 40 \text{ GHz} \end{aligned}$$

f is frequency in GHz
 SCD21(f) is the cable assembly differential to common-mode conversion loss
 SDD21 (f) is the cable assembly insertion loss

This limit is based on 5ps of skew (see presentation)

Proposed Response Response Status O

CI 162 SC 162.11.4 P 157 L 48 # 112

Champion, Bruce TE Connectivity
 Comment Type T Comment Status X

Cable assembly differential to common-mode return loss requirements are listed as TBD

SuggestedRemedy

A limit should be specified by an equation. It is recommended to use the equation for this parameter as shown on page 5 of diminico_3ck_02e_0720.pdf

Proposed Response Response Status O

IEEE P802.3ck D1.3 100/200/400 Gb/s Electrical Interfaces Task Force 4th Task Force review comments

Cl 162 SC 162.11.3 P 158 L 9 # 113
 Kocsis, Sam Amphenol
 Comment Type **TR** Comment Status **X**
 CR ERL parameter N is "3500"
 SuggestedRemedy
 Change to "5100", see background/consensus presentation
 Proposed Response Response Status **O**

Cl 162B SC 162B.1.3.6 P 260 L 28 # 116
 Kocsis, Sam Amphenol
 Comment Type **ER** Comment Status **X**
 Is the reference to "110B.1.3.7" valid? 802.3-2018
 SuggestedRemedy
 Change to "110B.1.3.6"
 Proposed Response Response Status **O**

Cl 162 SC 162.11 P 156 L 37 # 114
 Kocsis, Sam Amphenol
 Comment Type **TR** Comment Status **X**
 Minimum cable assembly ERL = TBD
 SuggestedRemedy
 Change to "7.4dB", see background/consensus presentation
 Proposed Response Response Status **O**

Cl 162B SC 162B.1.3.6 P 260 L 32 # 117
 Kocsis, Sam Amphenol
 Comment Type **TR** Comment Status **X**
 No definition of start and stop frequencies
 SuggestedRemedy
 Add defintion for fstart=50MHz, fstop=40GHz
 Proposed Response Response Status **O**

Cl 162B SC 162B.1.3.1 P 256 L 26 # 115
 Kocsis, Sam Amphenol
 Comment Type **TR** Comment Status **X**
 MTF "FOM_ILD shall be less than (TBD) dB"
 SuggestedRemedy
 Change to "is recommended to be less than 0.18dB, and ILD(f) shall meet the values determined using the equation below."
 ILD(f)<1|dB for f<26.56GHz
 ILD(f)<3|dB for 26.56<f<40GHz,
 see background/consensus presentation
 Proposed Response Response Status **O**

Cl 162B SC 162B.1.3.6 P 260 L 52 # 118
 Kocsis, Sam Amphenol
 Comment Type **ER** Comment Status **X**
 Assumed methodology reference is 92.11.3.6.3?
 SuggestedRemedy
 Add explicit reference, since specific parameters will be change for 3ck
 Proposed Response Response Status **O**

Cl 162B SC 162B.1.3.6 P 261 L 1 # 119
 Kocsis, Sam Amphenol
 Comment Type **TR** Comment Status **X**
 No definition of start and stop frequencies
 SuggestedRemedy
 Add defintion for fstart=50MHz, fstop=40GHz
 Proposed Response Response Status **O**

IEEE P802.3ck D1.3 100/200/400 Gb/s Electrical Interfaces Task Force 4th Task Force review comments

Cl 162 SC 162.5 P 137 L 19 # 120
 Kocsis, Sam Amphenol
 Comment Type **TR** Comment Status **X**
 one-way delay no more than "14ns"
 SuggestedRemedy
 one-way delay no more than "16ns", for consistency with ERL parameter values
 Proposed Response Response Status **O**

Cl 162 SC 162.11.7 P 158 L 35 # 121
 Kocsis, Sam Amphenol
 Comment Type **TR** Comment Status **X**
 T_r is "7.5ps"
 SuggestedRemedy
 Change to "6.5ps", see background/consensus presentation
 Proposed Response Response Status **O**

Cl 162B SC 162B.1.3.2 P 256 L 41 # 122
 Kocsis, Sam Amphenol
 Comment Type **TR** Comment Status **X**
 text says test fixture "shall meet" Eq 162B-6
 SuggestedRemedy
 Change to "is recommended to meet and shall meet an ERL of 8dB, see background/consensus presentation
 Proposed Response Response Status **O**

Cl 162B SC 162B.1.3.2 P 256 L 41 # 123
 Kocsis, Sam Amphenol
 Comment Type **TR** Comment Status **X**
 Add definition of ERL for MTF
 SuggestedRemedy
 Copy Table120G-4, change Tfx to "0", use as reference for MTF ERL
 Proposed Response Response Status **O**

Cl 162 SC 162.9.3.1.2 P 149 L 6 # 124
 Hidaka, Yasuo Credo Semiconductor
 Comment Type **T** Comment Status **X**
 The definition of steady-state voltage vf in clause 136.9.3.1.2 uses the linear fit pulse p(k). The linear fit pulse p(k) is calculated with Dp=3 in clause 136, whereas it is calculated with Dp=4 in clause 162. It is not clear which procedure is used to calculate the linear fit pulse p(k).
 SuggestedRemedy
 Change "The steady-state voltage vf is defined in 136.9.3.1.2, and is determined using Nv=200."
 to
 "The steady-state voltage vf is defined in 136.9.3.1.2, and is determined using Nv=200 and linear fitted pulse p(k) calculated by the procedure in 162.9.3.1.1."
 Proposed Response Response Status **O**

Cl 162 SC 162.11.7.1.1 P 161 L 20 # 125
 Hidaka, Yasuo Credo Semiconductor
 Comment Type **E** Comment Status **X**
 The transmitter PCB signal path is denoted as S^(HOSPT).
 SuggestedRemedy
 Change "S^(HOSTxP)" to "S^(HOSPT)".
 Proposed Response Response Status **O**

IEEE P802.3ck D1.3 100/200/400 Gb/s Electrical Interfaces Task Force 4th Task Force review comments

Cl 162 SC 162.11.7.1.2 P161 L 50 # 126

Hidaka, Yasuo Credo Semiconductor

Comment Type E Comment Status X

The comment #127 for D1.2 was not correctly implemented.

The aggressor transmitter host PCB path was denoted as S^(HOTxSP) in clause 136.11.7.1.2, not S^(HOSTxP).

As written in editor's note, the comment #128 for D1.2 had a conflict in the variable name in Equation (162-13) due to this implementation error.

I recommend to implement #127 and #128 for D1.2 and denote the aggressor transmitter host PCB path as S^(HOTxSP) for consistency with clause 136.11.7.1.2.

SuggestedRemedy

Change "S^(HOSTxP)" to "S^(HOTxSP)" in the following locations:

- P161, line 50
- P162, line 5, Equation (162-13)
- P162, line 11
- P162, line 16, Equation (162-14)
- P162, line 22

Remove Editor's note.

Proposed Response Response Status O

Cl 120F SC 120F.3.1.3 P 210 L 43 # 127

Hidaka, Yasuo Credo Semiconductor

Comment Type T Comment Status X

As Rob presented and we discussed at ad hoc on 9/16/2020, EOJ methodology defined in 120D.3.1.8.2 does not correctly measure EOJ due to length of PRBS13Q and 4MHz bandwidth of clock recovery.

To prevent CDR from tacking two cycles of test pattern, the best solution may be to use a test pattern shorter than PRBS13Q.

SuggestedRemedy

Define PRBS9Q test pattern in clause 120.5.11.2, similar to PRBS13Q in 120.5.11.2.1, but using PRBS9 defined in Table 68-6.

Choose 12 edges in PRBS9Q test pattern, and add a table similar to Table 120D-4.

Add a sub clause how to measure EOJ using PRBS9Q, similar to 120D.3.1.8.2.

Proposed Response Response Status O

Cl 163A SC 163A.2 P 281 L 3 # 128

Hidaka, Yasuo Credo Semiconductor

Comment Type T Comment Status X

TP0 is the interface between Transmitter package ball and PCB as shown in Figure 163-3. TP0 is not stable for measurement, because TP0 is highly non-TEM mode. A replica test fixture may have a test point corresponding to TP0, but this cannot be exactly same as TP0 due to the difficulty of measurement at TP0. In order to remind this difference, we should make the label of the test point for replica test fixture different from TP0.

We should not assume replica test fixture is same as actual test fixture.

Also for clarification, I suppose we should differentiate the label of TP0v between the test fixture attached to DUT and the replica test fixture.

SuggestedRemedy

Use TP0r and TP0vr as the labels for the test points where the replica test fixture may be used.

Proposed Response Response Status O

IEEE P802.3ck D1.3 100/200/400 Gb/s Electrical Interfaces Task Force 4th Task Force review comments

Cl 162 SC 162.11 P 156 L 18 # 129
 Ghiasi, Ali Ghiasi Quantum/Inphi
 Comment Type **TR** Comment Status **X**
 802.3cd standards specified 50 kHz AC coupling but this standard is operating 2x the Baudrate
 SuggestedRemedy
 Replace 50 KHz with 100 kHz
 Proposed Response Response Status **O**

Cl 162 SC 162.11.3 P 157 L 43 # 132
 Ghiasi, Ali Ghiasi Quantum/Inphi
 Comment Type **ER** Comment Status **X**
 ..shall be meet ..
 SuggestedRemedy
 should be ...shall meet....
 Proposed Response Response Status **O**

Cl 162 SC 162.11 P 156 L 19 # 130
 Ghiasi, Ali Ghiasi Quantum/Inphi
 Comment Type **TR** Comment Status **X**
 If the AC coupling needs to be 50 KHz or 100 KHz why are we defining capacitor value, actually 100 nF results in 32 KHz cut off
 SuggestedRemedy
 Remove recommended AC coupling value
 Proposed Response Response Status **O**

Cl 162 SC 162.11.3 P 157 L 44 # 133
 Ghiasi, Ali Ghiasi Quantum/Inphi
 Comment Type **TR** Comment Status **X**
 Given that for low loss cable the loss is controlled to 1 dB, we should do the same for high loss cable
 SuggestedRemedy
 The intention of this statement is not clear! Does it mean that if COM >=4 dB then no need to meet ERL?
 Proposed Response Response Status **O**

Cl 162 SC 162.9.4.3 P 152 L 32 # 131
 Ghiasi, Ali Ghiasi Quantum/Inphi
 Comment Type **TR** Comment Status **X**
 Given that for low loss cable the loss is controlled to 1 dB, we should do the same for high loss cable
 SuggestedRemedy
 Increase the cable assembly test case min loss from 17.75 to 18.75 dB
 Proposed Response Response Status **O**

Cl 162 SC 162.11.7.2 P 163 L 6 # 134
 Ghiasi, Ali Ghiasi Quantum/Inphi
 Comment Type **TR** Comment Status **X**
 Some explanation is necessary for table 162-20
 SuggestedRemedy
 "A description would be helpful such as ""cable assemblies are constructed with identical MDI at each end of cable or could be constructed with different MDI for cable A vs B ends, see table ..""
 In the table add A end and B end"
 Proposed Response Response Status **O**

IEEE P802.3ck D1.3 100/200/400 Gb/s Electrical Interfaces Task Force 4th Task Force review comments

Cl 163 SC 163.9.2 P 176 L 30 # 135

Ghiasi, Ali Ghiasi Quantum/Inphi

Comment Type TR Comment Status X

Transmit parameters must be measurable and well defined physical test point, the current TP0v test point methodology is not proven yet and is not uncommon when one inverts the channel spurious response to result. We have put into the draft unproven test method when the solution was trivial!

SuggestedRemedy

Just as we have done for the MCB and HCB losses, we need to increase the loss from the TP0 to TP0a a loss of 2.2 dB to 2.6 dB with nominal 2.4 dB loss is inline with MCB loss and allow construction of DUT boards with 2.5-3" long traces. Such traces combined with 2x8 or 2x12 2.5 mm pogo pins connectors allow breakout of high large 256 lanes switches. Make TP0a normative and make TP0v the method to de-embed when DUT PCB loss deviate from nominal range.

Proposed Response Response Status O

Cl 163 SC 163.9.2.2 P 178 L 33 # 136

Ghiasi, Ali Ghiasi Quantum/Inphi

Comment Type TR Comment Status X

Increase the loss from 1.2 dB and 1.6 dB

SuggestedRemedy

to 2.2 and 2.6 dB and update equation 163-1 to $=0.0062 + 0.1753*\sqrt{f}+0.0561*f$ the equation nominal loss is 2.4 dB

Proposed Response Response Status O

Cl 163 SC 163.9.3.2 P 181 L 18 # 137

Ghiasi, Ali Ghiasi Quantum/Inphi

Comment Type TR Comment Status X

Increase the loss from 1.2 dB and 1.6 dB

SuggestedRemedy

to 2.2 and 2.6 dB

Proposed Response Response Status O

Cl 163 SC 163.10.5 P 186 L 48 # 138

Ghiasi, Ali Ghiasi Quantum/Inphi

Comment Type TR Comment Status X

802.3cd standards specified 50 kHz AC coupling but this standard is operating 2x the Baudrate

SuggestedRemedy

Replace 50 KHz with 100 kHz

Proposed Response Response Status O

Cl 163 SC 163.A.3.1 P 281 L 25 # 139

Ghiasi, Ali Ghiasi Quantum/Inphi

Comment Type TR Comment Status X

Why is the cascaded reference package with test fixture called virtual reference channel, shouldn't this be the DUT reference channel? When testing a real device the package will be DUT package, using reference is confusing as it could imply IEEE COM reference package.

SuggestedRemedy

Repalce virtual with DUT, and replace reference package with DUT package

Proposed Response Response Status O

Cl 120F SC 120.F.3.1 P 208 L 1 # 140

Ghiasi, Ali Ghiasi Quantum/Inphi

Comment Type T Comment Status X

Until it is proven TP0v with real measurement the electrical characteristics should be at TP0a, there is no need create all this confusion and complexity by introducing TP0v when the solution is trivial just increase the DUT board loss to 2.4 dB as we have done for MCB and HCB!

SuggestedRemedy

Change TP0v to TP0a

Proposed Response Response Status O

IEEE P802.3ck D1.3 100/200/400 Gb/s Electrical Interfaces Task Force 4th Task Force review comments

CI 120F SC 120.F.3.1 P 208 L 13 # 141
 Ghiasi, Ali Ghiasi Quantum/Inphi
 Comment Type **TR** Comment Status **X**
 30 mV AC common mode results in 1+ dB of COM penalty, there is no technical bases for using such large amount of AC common mode
 SuggestedRemedy
 Reduce TX AC common mode from 30 mV to 15 mV RMS
 Proposed Response Response Status **O**

CI 120F SC 120F.3.2.3 P 213 L 18 # 142
 Ghiasi, Ali Ghiasi Quantum/Inphi
 Comment Type **TR** Comment Status **X**
 Inteference tolerance must include AC common mode
 SuggestedRemedy
 Add step k to the list: Adjust stressor P/N skew if necessary to achive 17.5 mV AC RMS.
 Proposed Response Response Status **O**

CI 120G SC 120G.3.1.3 P 227 L 46 # 143
 Ghiasi, Ali Ghiasi Quantum/Inphi
 Comment Type **TR** Comment Status **X**
 Rx of 0.618 implies permitted reflection of -4.2 dB which can be problematic for C2M receiver with just 4T DFE, at 50G we have Rx of 0.19. Extensive analysis was performed by Mr. Mellitz but C2M measurement points are at TP1a and TP4 not an end-end link using COM
https://www.ieee802.org/3/ck/public/adhoc/jun10_20/mellitz_3ck_adhoc_01a_061020.pdf
 SuggestedRemedy
 Recommend changing back to the original Rx=0.19 which equates to -14.4 dB unless it can be proven that -4.2 dB would work on a link where compliance is not at the slicer.
 Proposed Response Response Status **O**

CI 120G SC 120G.3.2.1 P 229 L 48 # 144
 Ghiasi, Ali Ghiasi Quantum/Inphi
 Comment Type **TR** Comment Status **X**
 It is stated that module has two setting one settting for short and one setting for long, not clear what short and long are nor clear if the link must work between short and long!
 SuggestedRemedy
 Define short channel as following: Any host channel with loss up to 11 dB.
 Define long channel as following: Any host channel with loss >11 dB.
 Proposed Response Response Status **O**

CI 120G SC 120G.3.2.3 P 231 L 16 # 145
 Ghiasi, Ali Ghiasi Quantum/Inphi
 Comment Type **TR** Comment Status **X**
 Rx of 0.618 implies permitted reflection of -4.2 dB which can be problematic for C2M receiver with just 4T DFE, at 50G we have Rx of 0.19. Extensive analysis was performed by Mr. Mellitz but C2M measurement points are at TP1a and TP4 not an end-end link using COM
https://www.ieee802.org/3/ck/public/adhoc/jun10_20/mellitz_3ck_adhoc_01a_061020.pdf
 SuggestedRemedy
 Recommend changing back to the original Rx=0.19 which equates to -14.4 dB unless it can be proven that -4.2 dB would work on a link where compliance is not at the slicer.
 Proposed Response Response Status **O**

CI 120G SC 120G.3.3 P 231 L 47 # 146
 Ghiasi, Ali Ghiasi Quantum/Inphi
 Comment Type **TR** Comment Status **X**
 KR/CR chips are defiend with common mode of 0.2 V to 1.0 V, there is no reason to define the same host with such high common mode
 SuggestedRemedy
 Reduce common mode min to 0.2 V and common mode max to 1.0 V
 Proposed Response Response Status **O**

IEEE P802.3ck D1.3 100/200/400 Gb/s Electrical Interfaces Task Force 4th Task Force review comments

CI 120G SC 120G.3.2 P 229 L 34 # 147

Ghiasi, Ali Ghiasi Quantum/Inphi

Comment Type **TR** Comment Status **X**

KR/CR chips are defiend with common mode of 0.2 V to 1.0 V, there is no reason to define the same host with such high common mode.

If the CDR in the module is BiCMOS and uses 3.3 V then one will use the right voltage rating but if the CDR in the module is CMOS then one doesn't need to use 3.3V+ DC blocks.

SuggestedRemedy

Reduce common mode min to 0.2 V and common mode max to 1.0 V

Proposed Response Response Status **O**

CI 120G SC 120G.3.1 P 224 L 9 # 148

Ghiasi, Ali Ghiasi Quantum/Inphi

Comment Type **TR** Comment Status **X**

KR/CR chips are defiend with common mode of 0.2 V to 1.0 V, there is no reason to define the same host to have such large output common mode voltage. If the CDR in the module is BiCMOS and uses 3.3 V then one will use the right voltage rating but if the CDR in the module is CMOS then one doesn't need to use 3.3V+ DC blocks.

SuggestedRemedy

Reduce common mode min to 0.2 V and common mode max to 1.0 V

Proposed Response Response Status **O**

CI 120G SC 120G.3.4 P 235 L 18 # 149

Ghiasi, Ali Ghiasi Quantum/Inphi

Comment Type **TR** Comment Status **X**

KR/CR chips are defiend with common mode of 0.2 V to 1.0 V, there is no reason to define the same host to have such large output common mode voltage. If the CDR in the module is BiCMOS and uses 3.3 V then one will use the right voltage rating but if the CDR in the module is CMOS then one doesn't need to use 3.3V+ DC blocks.

SuggestedRemedy

Reduce common mode min to 0.2 V and common mode max to 1.0 V

Proposed Response Response Status **O**

CI 120G SC 120G.5.3 P 241 L 31 # 150

Ghiasi, Ali Ghiasi Quantum/Inphi

Comment Type **TR** Comment Status **X**

Pre-cursor ISI was added in 802.3bs when we did not have VEC, several people have questioned if pre-cursor ISI is need. No has shown why we need to keep pre-cursor ISI, just it might be usefull.

SuggestedRemedy

Given than no one has shown pre-cursor ISI needed then we should remove

Proposed Response Response Status **O**

CI 162 SC 162.9.3 P 146 L 24 # 151

Ghiasi, Ali Ghiasi Quantum/Inphi

Comment Type **TR** Comment Status **X**

30 mV AC common mode results in 1+ dB of COM penalty, there is no technical bases for using such large amount of AC common mode

SuggestedRemedy

Reduce TX AC common mode from 30 mV to 15 mV RMS

Proposed Response Response Status **O**

CI 162 SC 162.9.4 P 151 L 37 # 152

Ghiasi, Ali Ghiasi Quantum/Inphi

Comment Type **TR** Comment Status **X**

Receiver specifications at TP3 must include max AC common mode

SuggestedRemedy

Add max AC commonm mode 17.5 mV to the table

Proposed Response Response Status **O**

IEEE P802.3ck D1.3 100/200/400 Gb/s Electrical Interfaces Task Force 4th Task Force review comments

CI 163 SC 163.9.2 P 176 L 43 # 153

Ghiasi, Ali Ghiasi Quantum/Inphi

Comment Type **TR** Comment Status **X**

30 mV AC common mode results in 1+ dB of COM penalty, there is no technical bases for using such large amount of AC common mode

SuggestedRemedy

Reduce TX AC common mode from 30 mV to 15 mV RMS

Proposed Response Response Status **O**

CI 163 SC 163.9.3 P 180 L 25 # 154

Ghiasi, Ali Ghiasi Quantum/Inphi

Comment Type **TR** Comment Status **X**

Receiver specifications at TP5a must include max AC common mode

SuggestedRemedy

Add max AC common mode 17.5 mV to the table

Proposed Response Response Status **O**

CI 163 SC 163.9.3.3 P 182 L 20 # 155

Ghiasi, Ali Ghiasi Quantum/Inphi

Comment Type **TR** Comment Status **X**

Inteference tolerance must include AC common mode

SuggestedRemedy

Add step k to the list: Adjust stressor P/N skew if necessary to achive 17.5 mV AC RMS.

Proposed Response Response Status **O**

CI 162 SC 162.9.3.5 P 150 L 50 # 156

Dudek, Mike Marvell.

Comment Type **T** Comment Status **X**

The description here is not helpful. This is the common-mode to common mode return loss of the Tx. Also a value of 2dB hardly "limits" this affect it just helps and if it were really "required" it would need to be a much larger value.

SuggestedRemedy

Change the paragraph "Common-mode signal can be generated in the channel by conversion of a differential signal. Any commonmode signal returned into the channel can be converted back to a differential signal and result in differential noise into the receiver. To limit this effect, a minimum common-mode to common-mode return loss is required." to "Common-mode signals can be returned to the transmitter by differential to common mode reflections of the cable or receiver. Any commonmode signal reflected back into the channel by the transmitter can be converted to a differential signal and result in differential noise into the receiver. To reduce this effect a minimum common-mode to common-mode return loss is specified."

Proposed Response Response Status **O**

CI 162 SC 162.9.3.4 P 151 L 16 # 157

Dudek, Mike Marvell.

Comment Type **E** Comment Status **X**

The wording in the footnote doesn't properly describe what is being mitigated. In particular what is "the test point and transmission line". A test point doesn't have a return loss.

SuggestedRemedy

Change " which sufficiently mitigates the test point and transmission line return loss." to "which sufficiently mitigates the effect of reflections from the test connector and test fixture transmission line". Also on the footnote to table 162-17 on page 157 line 15

Proposed Response Response Status **O**

CI 162 SC 162.9.4.5 P 155 L 37 # 158

Dudek, Mike Marvell.

Comment Type **E** Comment Status **X**

Erroneous "be"

SuggestedRemedy

Change "shall be meet the" to "shall meet the" Also on page 157 line 43.

Proposed Response Response Status **O**

IEEE P802.3ck D1.3 100/200/400 Gb/s Electrical Interfaces Task Force 4th Task Force review comments

Cl 162 SC 162.11.3 P 157 L 40 # 159
 Dudek, Mike Marvell.
 Comment Type E Comment Status X
 mixture of singular "ERL" with plural "are"
 SuggestedRemedy
 Change "are" to "is"
 Proposed Response Response Status O

Cl 162 SC 162.11.7.1.1 P 161 L 19 # 160
 Dudek, Mike Marvell.
 Comment Type T Comment Status X
 The wrong name is used and the equation reference is wrong.
 SuggestedRemedy
 Change "HOSTxP" to "HOSPT" Change Equation 162-12 on line 21 to Equation 162-10
 Proposed Response Response Status O

Cl 163 SC 163.9.2.1.2 P 178 L 5 # 161
 Dudek, Mike Marvell.
 Comment Type T Comment Status X
 There is no specification for the ERL of the test fixture
 SuggestedRemedy
 Insert a Paragraph "The ERL of the test fixture shall be greater than TBD dB"
 Proposed Response Response Status O

Cl 163 SC 163.9.2.2 P 178 L 33 # 162
 Dudek, Mike Marvell.
 Comment Type TR Comment Status X
 The insertion loss of this example test fixture is un-realistically low. This applies to the Rx test fixture as well.

SuggestedRemedy
 Change the loss to "between 2.4 and 3.2dB" and double the co-efficients in equation 163-1 and change Figure 163-4 to match. Note that the Rx test fixture refers to this equation and figure as well. Change the loss of the Rx test fixture to "between 2.4 and 3.2dB" on page 181 line 19.
 Proposed Response Response Status O

Cl 163 SC 163.9.3.1 P 180 L 37 # 163
 Dudek, Mike Marvell.
 Comment Type TR Comment Status X
 The use of the trace replica in 93A.2 already enables the use of a variable loss Rx test fixture for the interference tolerance test fixture. It would be better to enable this for the ERL test as well as has been done for the Transmitter.

SuggestedRemedy
 Change the specification in Table 163-9 and section 163.9.3.1 from ERL to dERL using the methodology of Annex 163A with suitable exceptions
 Proposed Response Response Status O

Cl 163 SC 163.9.3.1 P 180 L 34 # 164
 Dudek, Mike Marvell.
 Comment Type E Comment Status X
 It is strange to have the ERL section that needs the Rx Test fixture ahead of the description of the test fixture.

SuggestedRemedy
 Reverse the order of the Rx ERL and Receiver test fixture sections to match the Tx order.
 Proposed Response Response Status O

IEEE P802.3ck D1.3 100/200/400 Gb/s Electrical Interfaces Task Force 4th Task Force review comments

CI 163 SC 163.9.3.2 P 181 L 26 # 165

Dudek, Mike Marvell.

Comment Type TR Comment Status X

Equation 163-2 and figure 163-6 are nothing to do with return loss. Also it would be better to use ERLas the parameter.

SuggestedRemedy

Change to match the Tx test fixture Replace the sentence referring to return loss with "The Receiver test fixture shall meet the specification for ERL in 163.9.2.1.2"

Proposed Response Response Status O

CI 163 SC 163.9.3.3 P 181 L 42 # 166

Dudek, Mike Marvell.

Comment Type TR Comment Status X

Equation 163-2 is nothing to do with return loss. Also it would be better to use ERLas the parameter.

SuggestedRemedy

Change to "The ERL of the test setup in Figure 93C-4 measured at TP5 replica towards TPt meets the requirements for ERL in 163.9.2.1.2 with the exception that the length of the reflection signal N is 3500 UI"

Proposed Response Response Status O

CI 163 SC 163.9.3.3 P 181 L 51 # 167

Dudek, Mike Marvell.

Comment Type TR Comment Status X

TP0v is not used in Annex 93C which describes this test method.

SuggestedRemedy

Either add a bullet at the beginning of the considerations. "In this clause TP0v replaces TP0a in annex 93C". Or Replace "TP0v" with "TP0a". Do the same in section 163.9.3.4

Proposed Response Response Status O

CI 163 SC 163.9.3.3 P 181 L 50 # 168

Dudek, Mike Marvell.

Comment Type TR Comment Status X

The relationship between Tr of the transmitter and the Trm measurement will be a function of the loss between TP0 and TP0v and the Nyquist frequency. The equation used was only valide for the loss of the test fixture of 1.4dB with a Nyquist frequency of approx 12.5GHz.

SuggestedRemedy

Replace the equation with TBD.

Proposed Response Response Status O

CI 120F SC 120F.3.1.1 P 209 L 26 # 169

Dudek, Mike Marvell.

Comment Type E Comment Status X

using the symbol for delta is a pain for normal typing and general report writing etc. d is used in table 120F-1 but the delta symbol is used in other places.

SuggestedRemedy

Replace the symbol delta with d throughout Ammex 120F. Additional places I noticed were

Proposed Response Response Status O

CI 120F SC 120F.3.2.3 P 212 L 42 # 170

Dudek, Mike Marvell.

Comment Type T Comment Status X

There isn't a return loss spec in 163.9.2.1

SuggestedRemedy

Change "return loss" to "effective return loss"

Proposed Response Response Status O

IEEE P802.3ck D1.3 100/200/400 Gb/s Electrical Interfaces Task Force 4th Task Force review comments

CI 120F SC 120F.3.1.1 P 209 L 26 # 171

Dudek, Mike Marvell.

Comment Type E Comment Status X

using the symbol for delta is a pain for normal typing and general report writing etc. d is used in table 120F-1 but the delta symbol is used in other places.

SuggestedRemedy

Replace the symbol delta with d throughout Ammex 120F. Additional places I noticed were

Proposed Response Response Status O

CI 120F SC 120F.3.2.3 P 212 L 42 # 172

Dudek, Mike Marvell.

Comment Type T Comment Status X

There isn't a return loss spec in 163.9.2.1

SuggestedRemedy

Change "return loss" to "effective return loss"

Proposed Response Response Status O

CI 162 SC 162.11.2 P 157 L 8 # 173

Haser, Alex Molex

Comment Type TR Comment Status X

The minimum IL is too strict to allow 0.5m 30awg cables (see support slide); need to relax min IL limit

SuggestedRemedy

More work needed to determine what the mask should be

Proposed Response Response Status O

CI 162 SC 162.11.2 P 157 L 10 # 174

Haser, Alex Molex

Comment Type TR Comment Status X

Fill in TBD. Low frequency cable loss can't vary wildly if the cable works at higher frequencies; no need to over-spec

SuggestedRemedy

Replace TBD with 0.05GHz

Proposed Response Response Status O

CI 162 SC 162.11.3 P 158 L 12 # 175

Haser, Alex Molex

Comment Type T Comment Status X

Setting a single value for fixture delay is not flexible enough to account for variation between test fixtures

SuggestedRemedy

Specify a range for fixture delay (e.g., 2ns +/- 10%)

Proposed Response Response Status O

CI 162 SC 162.11.3 P 158 L 15 # 176

Haser, Alex Molex

Comment Type ER Comment Status X

The note about fixture delay is misleading. The specified delay does not represent twice the transmission line delay. Only the coax is being removed from the fixture.

SuggestedRemedy

Change footnote to: "The specified Tfx value significantly mitigates the test point and transmission line return loss by removing the coax connector and via from the measurement." or something along those lines

Proposed Response Response Status O

IEEE P802.3ck D1.3 100/200/400 Gb/s Electrical Interfaces Task Force 4th Task Force review comments

Cl 162B SC 162B.1.3.1 P 256 L 25 # 177

Haser, Alex Molex

Comment Type TR Comment Status X

Start frequency has minimal impact on FOM_ILD values (see haser_3ck_adhoc_01c_062420, slide 8); a start frequency of 50 MHz is more practical than a start frequency of 10 MHz due to current commonly available VNA capabilities

SuggestedRemedy

Change fmin for FOM_ILD calculation from 10 MHz to 50 MHz

Proposed Response Response Status O

Cl 162B SC 162B.1.3.2 P 256 L 40 # 178

Haser, Alex Molex

Comment Type TR Comment Status X

Current RL mask doesn't accurately capture necessary RL performance

SuggestedRemedy

Remove RL mask and replace with ERL ; input values and ERL limit TBD

Proposed Response Response Status O

Cl 162B SC 162B.1.3.6 P 260 L 28 # 179

Haser, Alex Molex

Comment Type ER Comment Status X

Section 110B.1.3.7 does not exist

SuggestedRemedy

Change reference to 110B.1.3.6

Proposed Response Response Status O

Cl 162B SC 162B.1.3.6 P 260 L 29 # 180

Haser, Alex Molex

Comment Type TR Comment Status X

Start and stop frequencies are not defined for ICN calculation. This section points to (should point to) 110B.1.3.6, which specifies 50 MHz to 19 GHz; this range is insufficient for this data rate

SuggestedRemedy

Somehow specify ICN calculations should be done 50 MHz to 40 GHz with a 10 MHz step size, either by adding text or adding values to Table 162B-1

Proposed Response Response Status O

Cl 162B SC 162B.1.3.6 P 260 L 54 # 181

Haser, Alex Molex

Comment Type TR Comment Status X

Start and stop frequencies are not defined for ICN calculations

SuggestedRemedy

Add "Integrated crosstalk RMS noise voltages are measured over N uniformly-spaced frequencies f_n spanning the frequency range 50 MHz to 40 GHz with a minimum spacing of 10 MHz." to the end of this section or add values to Table 162B1-3

Proposed Response Response Status O

IEEE P802.3ck D1.3 100/200/400 Gb/s Electrical Interfaces Task Force 4th Task Force review comments

Cl 120G SC 120G.3.2.1 P 229 L 51 # 182

Maki, Jeffery Juniper Networks

Comment Type T Comment Status X

For host management of module equalization, it would be aligned with modern management interface specifications (e.g., CMIS with use of SFF-8024 Table 4-5 Host Electrical Interface Codes) to designate a nomenclature for the configuration that the module advertises it supports and the host selects. Since there are only two states to choose between, short and long, this is a very practical approach.

SuggestedRemedy

Add immediately after first occurrence of tx_eq_state the text, "also designated as 100GAUI-1-S or 100GAUI-1-L for 100GAUI-1 C2M, 200GAUI-2-S or 200GAUI-2-L for 200GAUI-2 C2M and 400GAUI-4-S or 400GAUI-4-L for 400GAUI-4 C2M." For the second occurrence of tx_eq_state, insert immediately after "tx_eq_state is 0" the text "or 100GAUI-1-S is selected for 100GAUI-1 C2M, or 200GAUI-2-S is selected for 200GAUI-2 C2M or 400GAUI-4-S is selected for 400GAUI-4 C2M." For the third occurrence of tx_eq_state, insert immediately after "tx_eq_state is 1" the text "or 100GAUI-1-L is selected for 100GAUI-1 C2M, or 200GAUI-2-L is selected for 200GAUI-2 C2M or 400GAUI-4-L is selected for 400GAUI-4 C2M." For the fourth occurrence of tx_eq_state, insert immediately after "tx_eq_state" the text "or the use of 100GAUI-1-S or 100GAUI-1-L for 100GAUI-1 C2M, 200GAUI-2-S or 200GAUI-2-L for 200GAUI-2 C2M and 400GAUI-4-S or 400GAUI-4-L for 400GAUI-4 C2M." Note this is very similar to BiDi optics that designate a base PMD name and an extended name for the "down" and "up" PMD. See for example Clause 58.1 for 100BASE-BX10, where it is written "100BASE-BX10-D PMD at one end and a 100BASE-BX10-U PMD at the other." Here we use the extended AUI name to indicate choice of equalization, short or long.

Proposed Response Response Status O

Cl 120G SC 120G.3.2.2 P 230 L 6 # 183

Maki, Jeffery Juniper Networks

Comment Type T Comment Status X

For host management of module equalization, it would be aligned with modern management interface specifications (e.g., CMIS with use of SFF-8024 Table 4-5 Host Electrical Interface Codes) to designate a nomenclature for the configuration that the module advertises it supports and the host selects. Since there are only two states to choose between, short and long, this is a very practical approach.

SuggestedRemedy

Insert immediately after "tx_eq_state set to 0" the text "or 100GAUI-1-S is selected for 100GAUI-1 C2M, or 200GAUI-2-S is selected for 200GAUI-2 C2M or 400GAUI-4-S is selected for 400GAUI-4 C2M." Insert immediately after "tx_eq_state set to 1" the text "or 100GAUI-1-L is selected for 100GAUI-1 C2M, or 200GAUI-2-L is selected for 200GAUI-2 C2M or 400GAUI-4-L is selected for 400GAUI-4 C2M."

Proposed Response Response Status O

Cl 120G SC 120G.6.3 P 243 L 30 # 184

Maki, Jeffery Juniper Networks

Comment Type T Comment Status X

Major capability/option for the module is missing.

SuggestedRemedy

Add one row to the table. (1) with Item = EQ; Feature = (100GAUI-1-S and 100GAUI-1-L) or (200GAUI-2-S and 200GAUI-2-L) or (400GAUI-4-S and 400GAUI-4-L); Subclause = 120G.3.2.1; Value/Comment = See 120G.3.2.1; Status = M; Support = Yes [].

Proposed Response Response Status O

Cl 120G SC 120G.6.3 P 243 L 29 # 185

Maki, Jeffery Juniper Networks

Comment Type T Comment Status X

Major capability/option for the host is missing that is already listed for the module.

SuggestedRemedy

Add row to table with Item = ADE-H; Feature = Adaptive Equalization; Subclause = 120G.3.3; Value/Comment = See 120G.3.3; Status = M; Support = Yes [].

Proposed Response Response Status O

IEEE P802.3ck D1.3 100/200/400 Gb/s Electrical Interfaces Task Force 4th Task Force review comments

CI 162 SC 162.9.3 P 146 L 48 # 186

Calvin, John Keysight Technologies

Comment Type T Comment Status X

The spec limit for Even-Odd jitter is only 358 femtoseconds, which is too low to be accurately measured with current state of the art test equipment.

SuggestedRemedy

Increase the spec limit from 0.019 UI to 0.025 UI

Proposed Response Response Status O

CI 163 SC 163.9.2 P 177 L 16 # 187

Calvin, John Keysight Technologies

Comment Type T Comment Status X

The spec limit for Even-Odd jitter is only 358 femtoseconds, which is too low to be accurately measured with current state of the art test equipment.

SuggestedRemedy

Increase the spec limit from 0.019 UI to 0.025 UI

Proposed Response Response Status O

CI 120F SC 120F.3.1 P 208 L 39 # 188

Calvin, John Keysight Technologies

Comment Type T Comment Status X

The spec limit for Even-Odd jitter is only 358 femtoseconds, which is too low to be accurately measured with current state of the art test equipment.

SuggestedRemedy

Increase the spec limit from 0.019 UI to 0.025 UI

Proposed Response Response Status O

CI 162 SC 162.9.3.3 P 150 L 39 # 189

Calvin, John Keysight Technologies

Comment Type T Comment Status X

Based on Sleigh/Calvin/LeCheminant presentation
https://grouper.ieee.org/groups/802/3/ck/public/adhoc/sept16_20/calvin_3ck_adhoc_01_091620.pdf it has been shown that the EOJ measurement is susceptible to a systematic error based on the test pattern length and baud rate. This is easily resolved by allowing the CDR loop BW to be reduced below 4 MHz

SuggestedRemedy

Update the text of page 150 line 39 to read Even-odd jitter is calculated using the measurement method specified in 120D.3.1.8.2. with the exception that EOJ may be measured with a clock recovery unit (CRU) with a corner frequency of <= 4 MHz and a slope of 20 dB/decade

Proposed Response Response Status O

CI 120F SC 120F.3.1.3 P 210 L 43 # 190

Calvin, John Keysight Technologies

Comment Type T Comment Status X

Based on Sleigh/Calvin/LeCheminant presentation
https://grouper.ieee.org/groups/802/3/ck/public/adhoc/sept16_20/calvin_3ck_adhoc_01_091620.pdf it has been shown that the EOJ measurement is susceptible to a systematic error based on the test pattern length and baud rate. This is easily resolved by allowing the CDR loop BW to be reduced below 4 MHz

SuggestedRemedy

Update the text of page 210 line 43 to read Even-odd jitter is calculated using the measurement method specified in 120D.3.1.8.2. with the exception that EOJ may be measured with a clock recovery unit (CRU) with a corner frequency of <= 4 MHz and a slope of 20 dB/decade

Proposed Response Response Status O

IEEE P802.3ck D1.3 100/200/400 Gb/s Electrical Interfaces Task Force 4th Task Force review comments

CI 120G SC 120G.3.3.2 P 232 L 23 # 191

Calvin, John Keysight Technologies

Comment Type T Comment Status X

Based on Hadrien/Garg/Calvin presentation
https://www.ieee802.org/3/ck/public/adhoc/sept23_20/louchet_3ck_adhoc_01a_092320.pdf
 it is illustrated that the Host stressed Far-end vertical eye closure of 7.5dB, cannot be realized with contemporary instrumentation. The current choice of MTF channel losses and sinusoidal impairments records a VEC on the order of 9.5dB.

SuggestedRemedy

Update the target Far-end vertical eye closure VEC in Table 120G-6 from 7.5dB to 9.5dB. Alternately asserting this 7.5dB VEC target without typical margining (SJ) impairments is allowable to reach a VEC of 7.5dB.

Proposed Response Response Status O

CI 120G SC 120G.3.4.1 P 235 L 40 # 192

Calvin, John Keysight Technologies

Comment Type T Comment Status X

Based on Hadrien/Garg/Calvin presentation
https://www.ieee802.org/3/ck/public/adhoc/sept23_20/louchet_3ck_adhoc_01a_092320.pdf
 it is illustrated that the Module stressed input test VEC (max) value of 9.5dB, cannot be realized with contemporary instrumentation. The current choice of MTF channel losses and sinusoidal impairments records a VEC on the order of 13dB.

SuggestedRemedy

Update the target VEC max in Table 120G-9 from 9.5dB to 13dB. Alternately asserting this 9.5dB target VEC should be attainable with either a lower loss C2M test channel, or without typical margining (SJ) impairments is allowable to reach a VEC of 9.5dB.

Proposed Response Response Status O

CI 163 SC 163.9.3.2 P 181 L 26 # 193

Wu, Mau-Lin MediaTek

Comment Type T Comment Status X

The sentence here is to define the "differential return loss" of the test fixture (TP5a) and refer to Equation (163-2) & Figure 163-6. However, the referred equation and figure are not correct.

The reason is that the original equation (Equation 163-2) & figure (Figure 163-4) in D1p2 had been removed from D1p3

SuggestedRemedy

Copy Equation 163-2 & Figure 163-4 in D1p2 & related description to D1p3. Put them in the appropriate location & correct the referred Equation ID & Figure ID.

Proposed Response Response Status O

CI 163 SC 163.9.3.3 P 181 L 42 # 194

Wu, Mau-Lin MediaTek

Comment Type T Comment Status X

The reference equation, Equation (163-2), is not correct. It shall be the original equation (equation 163-2) in D1p2 and be removed from D1p3.

SuggestedRemedy

Copy Equation 163-2 in D1p2 & related description to D1p3. Put them in the appropriate location & correct the referred Equation ID.

Proposed Response Response Status O

CI 120F SC 120F.3.1.1 P 209 L 6 # 195

Wu, Mau-Lin MediaTek

Comment Type E Comment Status X

The symbol "dERL (min)" here doesn't consist with "dERL (min)" in Table 120F-1.

SuggestedRemedy

Align with "dERL (min)" in Table 120F-1.

Proposed Response Response Status O

IEEE P802.3ck D1.3 100/200/400 Gb/s Electrical Interfaces Task Force 4th Task Force review comments

Cl 120F SC 120F.3.1.1 P 209 L 26 # 196
 Wu, Mau-Lin MediaTek
 Comment Type E Comment Status X
 The symbol "dERL (min)" here doesn't consist with "dERL (min)" in Table 120F-1.
 SuggestedRemedy
 Align with "dERL (min)" in Table 120F-1.
 Proposed Response Response Status O

Cl 163A SC 163A.3.1.1 P 282 L 19 # 199
 Wu, Mau-Lin MediaTek
 Comment Type T Comment Status X
 The parameter of "N_v" in the equation (163A-3) had been mistakenly set as "n_v".
 SuggestedRemedy
 Correct "n_v" as "N_v" in the equation (163A-3)
 Proposed Response Response Status O

Cl 163 SC 163.9.2 P 176 L 43 # 197
 Wu, Mau-Lin MediaTek
 Comment Type T Comment Status X
 By adopting "TP0v" variable test fixture methodology, the value of "AC common-mode RMS voltage (max)" will be also strongly dependent on IL of TP0v. We need to fix this.
 SuggestedRemedy
 We shall define "Difference between measured and reference AC common-mode RMS voltage (max)" here. We shall define the AC common-mode RMS voltage (max) at TP0 and adopt one scaling factor which is related to IL of TP0v to derive the reference AC common-mode RMS voltage (max) at TP0v. Define the difference among measured one and reference one. Some information had been provided in wu_3ck_adhoc_01_090920.pdf. Plan to provide one contribution, wu_3ck_01_1120.pdf, for
 Proposed Response Response Status O

Cl 163 SC 163.9.3.4 P 183 L 41 # 200
 Wu, Mau-Lin MediaTek
 Comment Type T Comment Status X
 The "Case E from Table 162-15" here is not correct. The original one in D1p2 is "Case E from Table Table 163-9", where Case E is the case with Jitter frequency 40 MHz. However, the "Case E from Table 162-15" in D1p3 is the case with Jitter frequency 12 MHz. There is one similar errors in step c) in 120F.3.2.4 at page 214.
 SuggestedRemedy
 Change "Case E from Table 162-15" to "Case F from Table 162.15" both in step c) in 163.9.3.4 at page 183 & step c) in 120F.3.2.4 at page 214.
 Proposed Response Response Status O

Cl 163A SC 163A.1 P 280 L 28 # 198
 Wu, Mau-Lin MediaTek
 Comment Type E Comment Status X
 It seems that the term "for" in the following sentence is redundant.
 "c) The difference between measured and reference values for are computed using the methods defined in 163A.3.2."
 SuggestedRemedy
 Change the sentence of c) into "c) The difference between measured and reference values are computed using the methods defined in 163A.3.2."
 Proposed Response Response Status O

Cl 120F SC 120F.3.2.4 P 214 L 16 # 201
 Wu, Mau-Lin MediaTek
 Comment Type T Comment Status X
 It mentions that "The receiver under test shall meet the FEC symbol error ratio requirement for each case in Table 162-15". However, the FEC symbol error ratio requirement is 1e-3 in Table 162-15, which is for KR & CR. For C2C application, the FEC symbol error ratio requirement shall be 1e-4.
 SuggestedRemedy
 Change the sentence to "The receiver under test shall meet 1e-4 FEC symbol error ratio requirement for each case in Table 162-15."
 Proposed Response Response Status O

IEEE P802.3ck D1.3 100/200/400 Gb/s Electrical Interfaces Task Force 4th Task Force review comments

CI 163 SC 163.9.2 P 176 L 44 # 202

Wu, Mau-Lin MediaTek

Comment Type T Comment Status X

dERL is still TBD

SuggestedRemedy

Suggest to set as some negative values. I had shared some information in wu_3ck_adhoc_01_092320.pdf. I plan to prepare one contribution, wu_3ck_02_1120.pdf, for this comment.

Proposed Response Response Status O

CI 120F SC 120F.3.1 P 207 L 14 # 203

Wu, Mau-Lin MediaTek

Comment Type T Comment Status X

dERL is still TBD

SuggestedRemedy

Suggest to set as some negative values. I had shared some information in wu_3ck_adhoc_01_092320.pdf. I plan to prepare one contribution, wu_3ck_02_1120.pdf, for this comment.

Proposed Response Response Status O

CI 163 SC 163.9.2.2 P 178 L 33 # 204

Wu, Mau-Lin MediaTek

Comment Type T Comment Status X

The IL and ILD specs here are too challenging to achieve. In this case, I see no points to provide this kind of "example TX test fixture". Based on that, I proposed to relax the IL and ILD specs of this example TX test fixture (TP0a). Detailed information had been included in wu_3ck_adhoc_01_092320.pdf. I plan to prepare one contribution, wu_3ck_02_1120.pdf, for this comment.

SuggestedRemedy

Change IL and ILD specs of the example TX test fixture (TP0a) to "between 2.0 dB and 2.8 dB at 26.56 GHz". ILD is less than or equal to 0.2 dB from 0.05 to 26.56 GHz
Remove the Equation (163-1), Figure 163-4, and related paragraphs since TP0a is just an example and informative

Proposed Response Response Status O

CI 163A SC 163A.1 P 280 L 47 # 205

Wu, Mau-Lin MediaTek

Comment Type T Comment Status X

By adopting "TP0v" test fixture methodology, not only ERL, vf, vpeak, but also AC common-mode RMS voltage shall be scaled by IL of TP0v test fixture.

SuggestedRemedy

If we take the V_ACCM as the notation for "AC common-mode RMS voltage", propose to change the blocks of "Measured ERL, V_f, V_peak" & "Reference ERL, V_f, V_peak" in Figure 163A-1 to "Measured ERL, V_f, V_peak, V_ACCM" & "Reference ERL, V_f, V_peak, V_ACCM".

The paragraphs in Annex 163 related to this change shall be modified accordingly. Some new paragraphs may need if necessary.

Plan to provide one contribution, wu_3ck_01_1120.pdf, for more details.

Proposed Response Response Status O

CI 120G SC 120G.5.2 P 241 L 10 # 206

Ran, Adeo Intel

Comment Type T Comment Status X

In item c the linear fit is performed "with parameter M the same as for step a)" - but in step a there is no mention of M.

If M corresponds to "a minimum of 3 samples per symbol" then this is too low for calculation of a linear fit and especially for obtaining t_s.

In the PMD clauses, for linear fit, M is required to be at least 32, and interpolation can be used. The third paragraph of 162.9.3.1.1 (which is referenced here) states this clearly, so no explicit statement is required.

SuggestedRemedy

Delete "with parameter M the same as for step a)".

Proposed Response Response Status O

IEEE P802.3ck D1.3 100/200/400 Gb/s Electrical Interfaces Task Force 4th Task Force review comments

Cl 120G SC 120G.5.1 P 238 L 51 # 207
 Ran, Adeo Intel
 Comment Type E Comment Status X
 Cross reference to 120E.3.1 is inaccurate
 SuggestedRemedy
 Change to 120E.3.1.2
 Proposed Response Response Status O

Cl 120G SC 120G.3.1 P 226 L 17 # 208
 Ran, Adeo Intel
 Comment Type T Comment Status X
 ESMW is TBD.
 The importance of ESMW is not clear and there has been no proposal for a value for this parameter.
 It is suggested to remove EMSW, at least until evidence of the need for it (in addition to the existing EH and VEC limits) and a robust measurement method are presented, and a value for limit is proposed.
 SuggestedRemedy
 Remove the EMSW row from this table (120G-1), and also from Table 120G-3 (twice), Table 120G-6, and Table 120G-9.
 Proposed Response Response Status O

Cl 120G SC 120G.3.1 P 226 L 17 # 209
 Ran, Adeo Intel
 Comment Type T Comment Status X
 The reference for ESMW is subclause 120G.3.1.6 which does not address ESMW at all.
 Note: In another comment, ESMW is proposed to be removed.
 SuggestedRemedy
 If ESMW is not removed, change the reference from 120G.3.1.6 to 120G.5.2 in Table 120G-1 and in Table 120G-3.
 Proposed Response Response Status O

Cl 120G SC 120G.5.2 P 241 L 14 # 210
 Ran, Adeo Intel
 Comment Type T Comment Status X
 "Compute the receiver input signal $y_{rx}(k)$ by applying the effect of the DFE to $y_2(k)$ using the sampling phase t_s and tap weights $b(n)$ determined in the previous step"
 It is not specified fully how the effect of the DFE is applied. Different methods can result in different eye shape. Although EH and VEC are not affected, if EW or ESMW spec are retained they will depend on the DFE application, so it needs to be specified unambiguously.
 SuggestedRemedy
 If ESMW and EW specifications are not removed, Change the quoted statement to
 "Compute the receiver input signal $y_{rx}(k)$ by adding the output of a DFE with tap weights $b(n)$ determined in the previous step to $y_2(k)$. The DFE output is a piecewise-constant signal with transitions occurring at $t_s + UI/2$ ".
 Proposed Response Response Status O

Cl 120G SC 120G.3.3.2 P 232 L 18 # 211
 Ran, Adeo Intel
 Comment Type T Comment Status X
 Eye width is only a parameter of host stressed input specification (Table 120G-6). There is no corresponding parameter in the module output signal.
 Similarly in module stressed input (Table 120G-9).
 Creating a special condition for the stress signal is burdensome for the test setup, and is not justified if there is no such specification for output signal.
 SuggestedRemedy
 Delete the eye width rows in tables 120G-6 and 120G-9.
 Proposed Response Response Status O

IEEE P802.3ck D1.3 100/200/400 Gb/s Electrical Interfaces Task Force 4th Task Force review comments

Cl 1 SC 1.4.87 P 32 L 33 # 212
 Dawe, Piers Nvidia
 Comment Type **TR** Comment Status **X**
 This says that there is one version of 200GAUI-2 when in fact there are two incompatible ones. Notice that 116.1 and 120.5.1 say "Annex 120F *or* Annex 120G".
SuggestedRemedy
 Change "and a two-lane version (200GAUI-2)" to "and two two-lane versions (200GAUI-2)".
 Change ", or Annex 120F and Annex 120G for 200GAUI-2." to ", or Annex 120F or Annex 120G for 200GAUI-2".
 Proposed Response Response Status **O**

Cl 1 SC 1.4.111 P 33 L 6 # 213
 Dawe, Piers Nvidia
 Comment Type **TR** Comment Status **X**
 This says that there is one version of 400GAUI-4 when in fact there are two incompatible ones. Notice that 116.1 and 120.5.1 say "Annex 120D, Annex 120E, Annex 120F, *or* Annex 120G".
SuggestedRemedy
 Change "and a four-lane version (400GAUI-4)" to "and two four-lane versions (400GAUI-4)".
 Change ", or Annex 120F and Annex 120G for 400GAUI-4." to ", or Annex 120F or Annex 120G for 400GAUI-4".
 Proposed Response Response Status **O**

Cl 73 SC 73.6 P 66 L 15 # 214
 Dawe, Piers Nvidia
 Comment Type **E** Comment Status **X**
 It's hard to tell what's going on here.
SuggestedRemedy
 Please show or tell the reviewers and the staff editor how this figure differs from the existing figure.
 Proposed Response Response Status **O**

Cl 135 SC 135.5.1 P 106 L 45 # 215
 Dawe, Piers Nvidia
 Comment Type **TR** Comment Status **X**
 These AUI specifications are alternatives
SuggestedRemedy
 Change "and" to "or". Also in the next paragraph.
 Proposed Response Response Status **O**

Cl 162 SC 162.7 P 138 L 41 # 216
 Dawe, Piers Nvidia
 Comment Type **E** Comment Status **X**
 Blank line(s)
SuggestedRemedy
 Remove. Also before tables 162-6 and 7.
 Proposed Response Response Status **O**

Cl 162 SC 162.9.3.4 P 151 L 12 # 217
 Dawe, Piers Nvidia
 Comment Type **T** Comment Status **X**
 Both the parameter description and the note are incorrect: "Twice the propagation delay associated with the test fixture", "The specified Tfx value represents twice the transmission line delay which sufficiently mitigates the test point and transmission line return loss."
 And the terminology doesn't match: propagation delay, transmission line delay - are they the same thing or what?
SuggestedRemedy
 Tfx is windowing time that is larger than twice the delay associated with the test point connector but less than twice the delay from the test point connector to the other end of the test fixture's transmission line.
 Also Tfx needs to appear in 93A.5, which is where the explanation should go, not here.
 Make similar changes in each ERL section in the draft.
 Proposed Response Response Status **O**

IEEE P802.3ck D1.3 100/200/400 Gb/s Electrical Interfaces Task Force 4th Task Force review comments

CI 162 SC 162.9.3.5 P 150 L 50 # 218

Dawe, Piers Nvidia

Comment Type TR Comment Status X

1. This paragraph complains about issues from mixed-mode conversion then claims that "a minimum common-mode to common-mode return loss is required". It's misinformation.
2. This is a standard, not an attempt at a textbook. We don't give any justifications for most other specs; there is no reason that this one should be different.
3. For those interested: this 2 dB CM LR spec is there to contain a gross build-up of CM voltage. It's ineffective in the context of mixed-mode where the specs are around 10-20 dB. But we don't need to discuss it in the draft.

SuggestedRemedy

Delete the paragraph

Proposed Response Response Status O

CI 162 SC 162.9.4.3.5 P 154 L 38 # 219

Dawe, Piers Nvidia

Comment Type E Comment Status X

The FEC symbol error ratio requirement assumes errors are

SuggestedRemedy

The FEC symbol error ratio requirement assumes that errors are

Proposed Response Response Status O

CI 162 SC 162.9.4.4.2 P 155 L 6 # 220

Dawe, Piers Nvidia

Comment Type E Comment Status X

Table 120D-7

SuggestedRemedy

Table 162-15

Proposed Response Response Status O

CI 162 SC 162.11.2 P 157 L 26 # 221

Dawe, Piers Nvidia

Comment Type TR Comment Status X

This minimum loss curve bends the wrong way at high frequencies

SuggestedRemedy

Change the limit (Eq 162-10) so it becomes flatter at high frequencies

Proposed Response Response Status O

CI 162 SC 162.11.6 P 158 L 23 # 222

Dawe, Piers Nvidia

Comment Type E Comment Status X

This is a simple number; dressing it up as equation is a waste of time, and not how it's done in 163.

SuggestedRemedy

Similar to 162.9.3.5 and Table 163-5: change the contents of this subclause to: The common-mode to common-mode return of the cable assembly shall be within the limit given in Table 162-18 at all frequencies between 50 MHz and 40 GHz.

In Table 162-18, put "(min)" after "Common-mode to common-mode return loss" and replace "Equation (162-11)" with "2".

Proposed Response Response Status O

CI 162 SC 162.11.7.1 P 160 L 52 # 223

Dawe, Piers Nvidia

Comment Type E Comment Status X

93A.1.2.1 is in this draft now.

SuggestedRemedy

Reference to 93A.1.2.1 should be a hotlink to this draft.

Proposed Response Response Status O

IEEE P802.3ck D1.3 100/200/400 Gb/s Electrical Interfaces Task Force 4th Task Force review comments

CI 162 SC 162.11.7.1.1 P161 L 23 # 224
 Dawe, Piers Nvidia
 Comment Type E Comment Status X
 =110.3
 SuggestedRemedy
 = 110.3 (insert space) as in 162.11.7.1.2, or use a word: "of" or "equals"?

Proposed Response Response Status O

CI 163 SC 163.1 P171 L 1 # 225
 Dawe, Piers Nvidia
 Comment Type E Comment Status X
 Layout
 SuggestedRemedy
 Remove blank lines at 1 and 25, make the first three tables wider so the notes take 2 lines not 3
 Proposed Response Response Status O

CI 163 SC 163.9.2 P177 L 12 # 226
 Dawe, Piers Nvidia
 Comment Type E Comment Status X
 It's surprising that the only definition of SNDR is table footnote c. The reader could miss the deviation from 120D.3.1.6.
 SuggestedRemedy
 At least put 162.9.3.1.1 in the Reference column with 120D.3.1.6
 Proposed Response Response Status O

CI 163 SC 163.9.2.1.1 P177 L 47 # 227
 Dawe, Piers Nvidia
 Comment Type T Comment Status X
 Try to exclude unexplored / unnecessary areas of inaccuracy or poor reproducibility in measurement.
 SuggestedRemedy
 Set a minimum insertion loss for this test fixture as well as a maximum. It could be as low as 1.2 dB which we had before for TP0a, or it could be higher.
 Proposed Response Response Status O

CI 163 SC 163.9.2.1.3 P178 L 26 # 228
 Dawe, Piers Nvidia
 Comment Type T Comment Status X
 It doesn't make sense to have an RL spec for the test fixture only to 26.56 GHz, while the spec for the item under test extends to 40 GHz (see 162.9.3.5, referenced from Table 163-5: is that the right cross-reference?)
 SuggestedRemedy
 Provide a CM RL spec for the test fixture up to the same frequency as the product spec.
 Proposed Response Response Status O

CI 163 SC 163.9.2.2 P178 L 33 # 229
 Dawe, Piers Nvidia
 Comment Type T Comment Status X
 An example with a range is more complicated than it need be.
 SuggestedRemedy
 Pick a single example IL, e.g. 3.5 or 4 dB. Make this and the IL equation 163-3 consistent. Give the reference ERL, steady-state voltage and so on for the example.
 Proposed Response Response Status O

IEEE P802.3ck D1.3 100/200/400 Gb/s Electrical Interfaces Task Force 4th Task Force review comments

Cl 163 SC 163.9.3.2 P 181 L 19 # 230
 Dawe, Piers Nvidia
 Comment Type T Comment Status X
 We agreed that a test fixture test fixture between 1.2 dB and 1.6 dB is not practical.
 SuggestedRemedy
 Make the receiver test fixture like the transmitter test fixture.
 Proposed Response Response Status O

Cl 93A SC 93A.1.2.1 P 198 L 3 # 233
 Dawe, Piers Nvidia
 Comment Type T Comment Status X
 Do we need to consider cascading 4-port networks?
 SuggestedRemedy
 Proposed Response Response Status O

Cl 163 SC 163.9.3.3 P 181 L 35 # 231
 Dawe, Piers Nvidia
 Comment Type T Comment Status X
 This isn't right: "transmitter equalization is configured by management (see 120D.3.2.3) to the settings that provide the lowest FEC symbol error ratio". It's the receiver's responsibility to choose an adequate transmitter equalization setting. Further, the transmitter could be a test instrument that doesn't do 802.3 management. What has 120D.3.2.3 got to do with it? Was this text copied from a C2C clause?
 SuggestedRemedy
 Correct the text. The transmitter equalization is what the receiver asks for after it's had a chance to train, or a default if it doesn't ask for anything in particular.
 Same for 163.9.3.4 Receiver jitter tolerance.
 Proposed Response Response Status O

Cl 93A SC 93A.1.2.1 P 198 L 10 # 234
 Dawe, Piers Nvidia
 Comment Type T Comment Status X
 It may be helpful to the reader (particularly someone programming this function) to know that cascade() is associative.
 SuggestedRemedy
 Add a sentence:
 cascade is associative: $\text{cascade}(S(w), \text{cascade}(S(x), S(y))) = \text{cascade}(\text{cascade}(S(w), S(x)), S(y))$.
 Proposed Response Response Status O

Cl 163 SC 163.10.2 P 186 L 28 # 232
 Dawe, Piers Nvidia
 Comment Type T Comment Status X
 A -60 dB response at 45 GHz, 32 dB below the response at Nyquist, can't matter, but a respectable channel could fail this limit.
 SuggestedRemedy
 Replace the straight part of the limit with one that curves down.
 Proposed Response Response Status O

Cl 93A SC 93A.1.2.2 P 198 L 14 # 235
 Dawe, Piers Nvidia
 Comment Type E Comment Status X
 Network
 SuggestedRemedy
 network (as in the published base document). Also in 93A.1.2.3
 Proposed Response Response Status O

IEEE P802.3ck D1.3 100/200/400 Gb/s Electrical Interfaces Task Force 4th Task Force review comments

Cl 93A SC 93A.5 P 202 L 26 # 236
 Dawe, Piers Nvidia
 Comment Type E Comment Status X
 New ERL parameters
 SuggestedRemedy
 Add rows for Tfx and Tukey window flag in Table 93A-4, ERL parameters
 Proposed Response Response Status O

Cl 93A SC 93A.5.1 P 202 L 39 # 237
 Dawe, Piers Nvidia
 Comment Type TR Comment Status X
 Unexplained notation of up and down: v ^
 SuggestedRemedy
 Remove it. Just say "and" "or" or whatever you mean. Or, don't cram with-Tukey and without-Tukey into one equation; you can easily say if Tw is zero, Htw is 1, and if it's one, the equation (somewhat simpler) applies.
 Proposed Response Response Status O

Cl 93A SC 93A.5.1 P 202 L 41 # 238
 Dawe, Piers Nvidia
 Comment Type T Comment Status X
 This way of writing the middle row of the equation is unnecessarily complicated.
 SuggestedRemedy
 Simplify it, remembering that $\cos(x)=\cos(-x)=-\cos(x+\pi)$. Notice that f < fb in this case and fper is +ve, with fb before fr in the formula.
 Something like $0.5(1-\cos(2\pi(fb-f)/fper))$
 Proposed Response Response Status O

Cl 120G SC 120G.2 P 225 L 29 # 239
 Dawe, Piers Nvidia
 Comment Type T Comment Status X
 Terminology should align better with that agreed after debate in P802.3ba or bs, and with the text.
 SuggestedRemedy
 In Figure 120G-4, Module compliance points, change "Receiver" to "Electrical input", and change "Transmitter" to "Electrical output".
 Proposed Response Response Status O

Cl 120G SC 120G.3.1 P 226 L 17 # 240
 Dawe, Piers Nvidia
 Comment Type TR Comment Status X
 We need an ESMW limit because in C2M, the effects of driver jitter and part-channel are limited in combination not separately. Eye width measurement works with or without a DFE in the reference receiver; examples in louchet_3ck_adhoc_01a_092320.pdf .
 If the VEC values in this draft and Annex 120E, and the ESMW in Annex 120E is right, ESMW should be between 0.22 and 0.3 UI.
 SuggestedRemedy
 Write down a range of candidate limits in the next draft, or a single limit if we have enough information to choose one.
 Proposed Response Response Status O

Cl 120G SC 120G.3.1.1 P 226 L 41 # 241
 Dawe, Piers Nvidia
 Comment Type E Comment Status X
 Font size of 53.125
 SuggestedRemedy
 Fix
 Proposed Response Response Status O

IEEE P802.3ck D1.3 100/200/400 Gb/s Electrical Interfaces Task Force 4th Task Force review comments

Cl **120G** SC **120G.3.1.1** P **226** L **41** # **242**
 Dawe, Piers Nvidia
 Comment Type **T** Comment Status **X**
 per lane
 SuggestedRemedy
 for each lane
 Proposed Response Response Status **O**

Cl **120G** SC **120G.3.2** P **229** L **17** # **243**
 Dawe, Piers Nvidia
 Comment Type **TR** Comment Status **X**
 We need ESMW limits because in C2M, the effects of driver jitter and part-channel are limited in combination not separately. Eye width measurement works with or without a DFE in the reference receiver; examples in louchet_3ck_adhoc_01a_092320.pdf . Annex 120E has NE ESMW 0.265 UI. Here we expect worse reflections but a more capable equaliser. If we stay with the two-settings method, ESMW should be somewhere in the range 0.2 to 0.265 UI

SuggestedRemedy
 Write down a range of candidate limits in the next draft, or a single limit if we have enough information to choose one.
 Proposed Response Response Status **O**

Cl **120G** SC **120G.3.2** P **229** L **19** # **244**
 Dawe, Piers Nvidia
 Comment Type **TR** Comment Status **X**
 For a reasonably clean module (or test equipment in a host stressed eye test), the driver swing has to be aggressively reduced to deliver only 24 mV. If the module is set to the "near" setting, and the host receiver isn't that near, the eye it is offered is smaller than 24 mV because of loss, and out of tune as well. 120E has 70 mV.

SuggestedRemedy
 Change the NEEH from 24 mV to 50 mV.
 Proposed Response Response Status **O**

Cl **120G** SC **120G.3.2** P **229** L **22** # **245**
 Dawe, Piers Nvidia
 Comment Type **T** Comment Status **X**
 We need ESMW limits because in C2M, the effects of driver jitter and part-channel are limited in combination not separately. Eye width measurement works with or without a DFE in the reference receiver; examples in louchet_3ck_adhoc_01a_092320.pdf . Annex 120E has FE ESMW 0.2 UI, no explicit VEC limit, and EH 30 mV. Here we expect worse reflections but a more capable equaliser. If we stay with the two-settings method, ESMW should be somewhere in the range 0.16 to 0.2 UI. But 0.16 seems too small.

SuggestedRemedy
 Write down a range of candidate limits in the next draft, or a single limit if we have enough information to choose one.
 Proposed Response Response Status **O**

Cl **120G** SC **120G.3.2** P **229** L **26** # **246**
 Dawe, Piers Nvidia
 Comment Type **T** Comment Status **X**
 We don't know what to do with far-end pre-cursor ISI ratio. It was copied in from a spec with a very different reference receiver. In this scenario, we don't know what it's for, what a limit should be, or why.
 I believe that the ordinary EH, EW and VEC specs with this reference receiver will defend receivers from the same threats that far-end pre-cursor ISI ratio in 120E was intended to guard against, except possibly for some drivers with exemplary noise, jitter and distortion but not so well tuned which can be received anyway.

SuggestedRemedy
 We could leave this TBD hanging around in case someone finds a use for it, or clean it up for now while no-one has. We can bring it back later if justified.
 Proposed Response Response Status **O**

IEEE P802.3ck D1.3 100/200/400 Gb/s Electrical Interfaces Task Force 4th Task Force review comments

CI 120G SC 120G.3.2.1 P 229 L 46 # 247

Dawe, Piers Nvidia

Comment Type TR Comment Status X

As already discussed, the 2-settings method with only two compliance losses doesn't work. If the module is set to the short setting, and the host receiver isn't that near, the eye it is offered is smaller than 24 mV because of loss, and out of tune as well. If the module is set to the long setting and the host isn't that long, the eye is also out of tune. There's no guarantee that either setting is usable.

SuggestedRemedy

We need four compliance losses forming two overlapping ranges, or go back to the one-setting method which is much preferable for avoiding complexity, firmware and interop issues.

Proposed Response Response Status O

CI 120G SC 120G.3.2.2.1 P 230 L 47 # 248

Dawe, Piers Nvidia

Comment Type E Comment Status X

-9.6dB

SuggestedRemedy

approximately 9.6 space dB

Proposed Response Response Status O

CI 120G SC 120G.3.2.2.1 P 230 L 49 # 249

Dawe, Piers Nvidia

Comment Type E Comment Status X

with an exception to use zp = 244.7 mm, and C0 and C1 are both 0 nF

SuggestedRemedy

with the exceptions that zp is 244.7 mm, and C0 and C1 are both 0 nF

Proposed Response Response Status O

CI 120G SC 120G.3.3.2 P 232 L 17 # 250

Dawe, Piers Nvidia

Comment Type TR Comment Status X

The module NE and FE minimum EH should not be the same (see another comment). If we stay with the 2-settings module specification, even if corrected with a 4-loss specification method, this should be reflected in this table, which should include near-end parameters anyway.

SuggestedRemedy

Add the rows for the near-end parameters.

Proposed Response Response Status O

CI 120G SC 120G.3.3.2.1 P 232 L 33 # 251

Dawe, Piers Nvidia

Comment Type T Comment Status X

This sentence refers to the SJ table but doesn't tell the reader what to do. Other clauses and annexes with similar tables say that the entries are used one at a time (you don't apply all the SJ tones at once).

SuggestedRemedy

Please make this explicit.

Proposed Response Response Status O

CI 120G SC 120G.3.3.2.1 P 233 L 43 # 252

Dawe, Piers Nvidia

Comment Type T Comment Status X

"Meeting the BER requirements at only one of the methods is sufficient": not quite. The host needs to choose right as well.

SuggestedRemedy

If the 2-settings method is kept, say that meeting the BER requirements at the one of the two methods that the host selects is sufficient.

Proposed Response Response Status O

IEEE P802.3ck D1.3 100/200/400 Gb/s Electrical Interfaces Task Force 4th Task Force review comments

CI 120G SC 120G.3.3.2.1 P 233 L 49 # 253

Dawe, Piers Nvidia

Comment Type T Comment Status X

120E.3.2.1.2

SuggestedRemedy

120G.5.3, if it remains - or delete the sentence. I believe the other specs mean that the following sentence "Pre-emphasis capability is likely to be required in the pattern generator to meet this requirement." would still apply.

Proposed Response Response Status O

CI 120G SC 120G.3.4.1.1 P 237 L 14 # 254

Dawe, Piers Nvidia

Comment Type T Comment Status X

"This CTLE setting has to be greater than or equal to TBD dB": with a compound CTLE, it's not as simple as that.

The limits should be close to that for TP4 FE in Table 120G-14, but might not be identical.

SuggestedRemedy

Proposed Response Response Status O

CI 120G SC 120G.4.1 P 238 L 34 # 255

Dawe, Piers Nvidia

Comment Type T Comment Status X

I'm sure there could be an acceptable channel that failed this mask at 45 GHz

SuggestedRemedy

Make the straight section curve down and/or truncate it at 50 GHz

Proposed Response Response Status O

CI 120G SC 120G.5.2 P 240 L 10 # 256

Dawe, Piers Nvidia

Comment Type T Comment Status X

By allowing stronger gDC with stronger gDC2, we can have up to 12 dB of peaking for gCD2 = -1 but up to 16 dB for gDC2 = -3 - yet we don't expect the maximum channel loss to vary like that.

SuggestedRemedy

I think we should be allowing stronger gDC with weaker gDC2, for TP1a and for TP4 far end.

Proposed Response Response Status O

CI 120G SC 120G.5.2 P 241 L 27 # 257

Dawe, Piers Nvidia

Comment Type TR Comment Status X

We can't pass the signal when it passes EH but fails EW / ESMW, but it might be OK at another setting. Note this does not require optimising for EW, only rejecting candidate solutions that fail EW (constraint not goal). We did this in 120E, nothing new here. Pre-cursor ISI ratio would be a constraint too if it remains.

SuggestedRemedy

Change:
where eye height also complies with the specification for eye height (min) as specified for the interface.

to:
where the eye also complies with the specifications for eye height, ESMW, and eye width if applicable, as specified for the interface.

Proposed Response Response Status O

CI 120G SC 120G.5.3 P 241 L 34 # 258

Dawe, Piers Nvidia

Comment Type TR Comment Status X

The valid setting would have to satisfy eye width / ESMW too.

SuggestedRemedy

Modify the definition of valid setting or delete the subclause.

Proposed Response Response Status O

IEEE P802.3ck D1.3 100/200/400 Gb/s Electrical Interfaces Task Force 4th Task Force review comments

CI **120G** SC **120G.5.3** P **241** L **37** # **259**
 Dawe, Piers Nvidia
 Comment Type **T** Comment Status **X**
 The pulse peak is not at the same time as the DFE sampling phase ts determined in step d of 120G.5.2, but it's close. No need for both.
SuggestedRemedy
 Change from pmax to the pulse at the DFE sampling phase ts, or delete the subclause.
 Proposed Response Response Status **O**

CI **FM** SC **FM** P **20** L **16** # **262**
 Dawe, Piers Nvidia
 Comment Type **E** Comment Status **X**
 Italics
SuggestedRemedy
 Should be upright as usual?
 Proposed Response Response Status **O**

CI **FM** SC **FM** P **1** L **8** # **260**
 Dawe, Piers Nvidia
 Comment Type **E** Comment Status **X**
 Draft Standard for Ethernet Amendment: Standard for Ethernet Amendment: repetition?
SuggestedRemedy
 Draft standard for Ethernet Amendment: or Standard for Ethernet Draft amendment: Also on page 29.
 Proposed Response Response Status **O**

CI **1** SC **1.1.3.2** P **30** L **21** # **263**
 Dawe, Piers Nvidia
 Comment Type **TR** Comment Status **X**
 These paragraphs about 100GAUI-n, 200GAUI-n and 400GAUI-n are written as if each is a single interface, as in "conformance with implementation of **this interface** ... is recommended, since it allows maximum flexibility" when there are multiple variants, which are not interoperable. Some of these errors should be fixed in maintenance but this project should not be adding new ones.
SuggestedRemedy
 Change "and a one-lane version (100GAUI-1)" to "and two one-lane versions (100GAUI-1),".
 Change "and a two-lane version (200GAUI-2)" to "and two two-lane versions (200GAUI-2),".
 Change "and a four-lane version (400GAUI-4)" to "and two four-lane versions (400GAUI-4),".
 Proposed Response Response Status **O**

CI **FM** SC **FM** P **10** L **1** # **261**
 Dawe, Piers Nvidia
 Comment Type **E** Comment Status **X**
 XX Month 201X
SuggestedRemedy
 XX Month 202X
 Proposed Response Response Status **O**

CI **1** SC **1.3** P **31** L **14** # **264**
 Dawe, Piers Nvidia
 Comment Type **E** Comment Status **X**
 The base document subclause 1.3 already has an entry for SFF-8665, Rev 1.9, June 29, 2015
SuggestedRemedy
 Delete this duplicate
 Proposed Response Response Status **O**

IEEE P802.3ck D1.3 100/200/400 Gb/s Electrical Interfaces Task Force 4th Task Force review comments

Cl 1 SC 1.4.36 P 32 L 1 # 265
 Dawe, Piers Nvidia
 Comment Type E Comment Status X
 1.4.36 isn't inserted by 802.3cd, it's in the base document
 SuggestedRemedy
 Change "as inserted" to "as modified"
 Proposed Response Response Status O

Cl 1 SC 1.4.36 P 32 L 6 # 266
 Dawe, Piers Nvidia
 Comment Type TR Comment Status X
 This says that there is one version of 100GAUI-1 when in fact there are two incompatible ones.
 SuggestedRemedy
 Change "and a single-lane version (100GAUI-1)" to "and two single-lane versions (100GAUI-1)".
 Change "Clause 135, Annex 120F, and Annex 120G for 100GAUI-1." to "Clause 135 and Annex 120F or Annex 120G for 100GAUI-1".
 The (See this for this, that for that...) section is becoming unwieldy: it could be better as separate sentences: For 100GAUI-1, see Clause 135 and Annex 120F or Annex 120G.
 Proposed Response Response Status O

Cl 1 SC 1.4.36 P 32 L 8 # 267
 Dawe, Piers Nvidia
 Comment Type E Comment Status X
 Why is PMA clause 135 listed but not 83 or 120 in similar text?
 SuggestedRemedy
 ?
 Proposed Response Response Status O

Cl 162B SC 162B.1.1.1 P 253 L 32 # 268
 Dawe, Piers Nvidia
 Comment Type T Comment Status X
 I read "reference TP2 or TP3 test fixture insertion loss" as the insertion loss of a reference TP2 or TP3 test fixture. But I think it is the reference insertion loss of a TP2 or TP3 test fixture (similar to line 19).
 SuggestedRemedy
 It might be clearer to re-order "reference TP2 or TP3 test fixture insertion loss" to "TP2 or TP3 test fixture reference insertion loss", putting "reference" immediately before "insertion loss" as appropriate throughout 162B.
 Proposed Response Response Status O

Cl 162B SC 162B.1.3.1 P 256 L 12 # 269
 Dawe, Piers Nvidia
 Comment Type E Comment Status X
 Figure 162B-3, Mated test fixtures insertion loss, shows the maximum and minimum IL but not the reference IL.
 SuggestedRemedy
 Please show the reference insertion loss of the mated test fixture also, on the same graph.
 Proposed Response Response Status O

Cl 162C SC 162C.1 P 264 L 52 # 270
 Dawe, Piers Nvidia
 Comment Type E Comment Status X
 I could not easily find what DL and SL mean
 SuggestedRemedy
 Add cross-reference to 162.8.1
 Proposed Response Response Status O

IEEE P802.3ck D1.3 100/200/400 Gb/s Electrical Interfaces Task Force 4th Task Force review comments

CI 162C SC 162C.2.1 P 268 L 6 # 271

Dawe, Piers

Nvidia

Comment Type E Comment Status X

"SFP+ supports one lane", "QSFP+ supports up to four lanes" and so on

SuggestedRemedy

Would it be clearer to say "SFP+ supports one lane in each direction" and similarly for the other connector types?

Proposed Response Response Status O

CI 162C SC 162C.2.2 P 268 L 46 # 272

Dawe, Piers

Nvidia

Comment Type T Comment Status X

SFP-DD supports up to four lanes

SuggestedRemedy

SFP-DD supports up to four lanes [in each direction]
Similarly for DSFP.

Proposed Response Response Status O

CI 162C SC 162C.3.3 P 275 L 22 # 273

Dawe, Piers

Nvidia

Comment Type E Comment Status X

Order of this table doesn't match the clause

SuggestedRemedy

Please re-order the entries in this table to align with the clause, renumbering the items.
Also, there is no MDI3 so some of them should be renumbered anyway.
Similarly for the table in 162C.3.4.1 Contact Mapping.

Proposed Response Response Status O

CI 162D SC 162D.1 P 277 L 14 # 274

Dawe, Piers

Nvidia

Comment Type E Comment Status X

"Hosts have six specified MDI connectors "receptacles"": I read this as describing a 6-port host.

SuggestedRemedy

Suggest "There are six types of MDI connectors "receptacles" specified for hosts"

Proposed Response Response Status O

CI 162D SC 162D.1 P 277 L 32 # 275

Dawe, Piers

Nvidia

Comment Type T Comment Status X

This is the only time "host interface type" is used, and one would expect the phrase to mean PMD or PHY type on a host. We can wordsmith round this because six things were mentioned just above.

SuggestedRemedy

Change "This creates six host interface types and multiple cable..." to "Therefore, there are multiple cable..."

Proposed Response Response Status O

CI 163A SC 163A.1 P 280 L 28 # 276

Dawe, Piers

Nvidia

Comment Type E Comment Status X

for are

SuggestedRemedy

Delete for?

Proposed Response Response Status O

IEEE P802.3ck D1.3 100/200/400 Gb/s Electrical Interfaces Task Force 4th Task Force review comments

Cl 163A SC 163A.3.1 P 281 L 22 # 277

Dawe, Piers Nvidia

Comment Type T Comment Status X

I don't like the term "virtual reference channel". It's no more unreal than the other blocks in this figure. I didn't find any other "reference channel" in this draft.

SuggestedRemedy

Change its name to "reference channel" or "reference test channel" throughout.

Proposed Response Response Status O

Cl 163A SC 163A.3.1 P 281 L 31 # 278

Dawe, Piers Nvidia

Comment Type T Comment Status X

The material in the NOTE needs to be normative.

SuggestedRemedy

Move it to regular text at line 42

Proposed Response Response Status O