



# Outline

- COM and channels used in this analysis
- Non-Monotonic COM performance by increasing FFE tap number
- Root cause and ways to improve
- Discussion & next step
- Summary

# COM Tool Adopted

- COM 2.41
  - Adopted COM ver2.41 ([Link](#)) released by Richard Mellitz
  - Adopted the following parameters proposed by Richard for “100 G KR PAM4 DFE1 FFE(3,1,24)”
    - T1config\_com\_ieee8023\_93a=100GEL-KR\_DFE1\_RxFFE3-24.xls
    - T1config\_com\_ieee8023\_93a=100GEL-KR\_DFE1\_RxFFE3-20.xls
    - T1config\_com\_ieee8023\_93a=100GEL-KR\_DFE1\_RxFFE3-16.xls
    - T1config\_com\_ieee8023\_93a=100GEL-KR\_DFE1\_RxFFE3-12.xls
  - PKG length = 30 mm
- COM 2.41a
  - Modified from COM 2.41 by extending the dimension of FV by 2
  - Details in latter pages

# Channels in this Simulation

Ch. ID	Description
A	Mellitz, Ideal Transmission Lines for Backplane* <sub>1</sub> ( <a href="#">Link</a> )
B	Mellitz, Initial BP – Best case Tachyon BP, 3’’ IL15to16 ( <a href="#">Link</a> )
C	Mellitz, Initial BP – Best case Tachyon BP, 13’’ IL25to26 ( <a href="#">Link</a> )
D	Mellitz, Cabled BP & PCB Design Impact Using 112G Ready Connectors, Opt1_24dB* <sub>2</sub> ( <a href="#">Link</a> )
E	Mellitz, Cabled BP & PCB Design Impact Using 112G Ready Connectors, Opt1_28dB* <sub>3</sub> ( <a href="#">Link</a> )

\*1. Adopt the “Backplane channel” for analysis

\*2. Adopt the channel of “CaBP\_BGAVia\_Opt1\_24dB.zip”

\*3. Adopt the channel of “CaBP\_BGAVia\_Opt1\_28dB.zip”

# Expectation – COM increases when FFE tap increases

- It's intuitive that COM values increases when FFE tap increases
- However, we found it's NOT true for COM 2.41
- Take Channel A as an example to do analysis

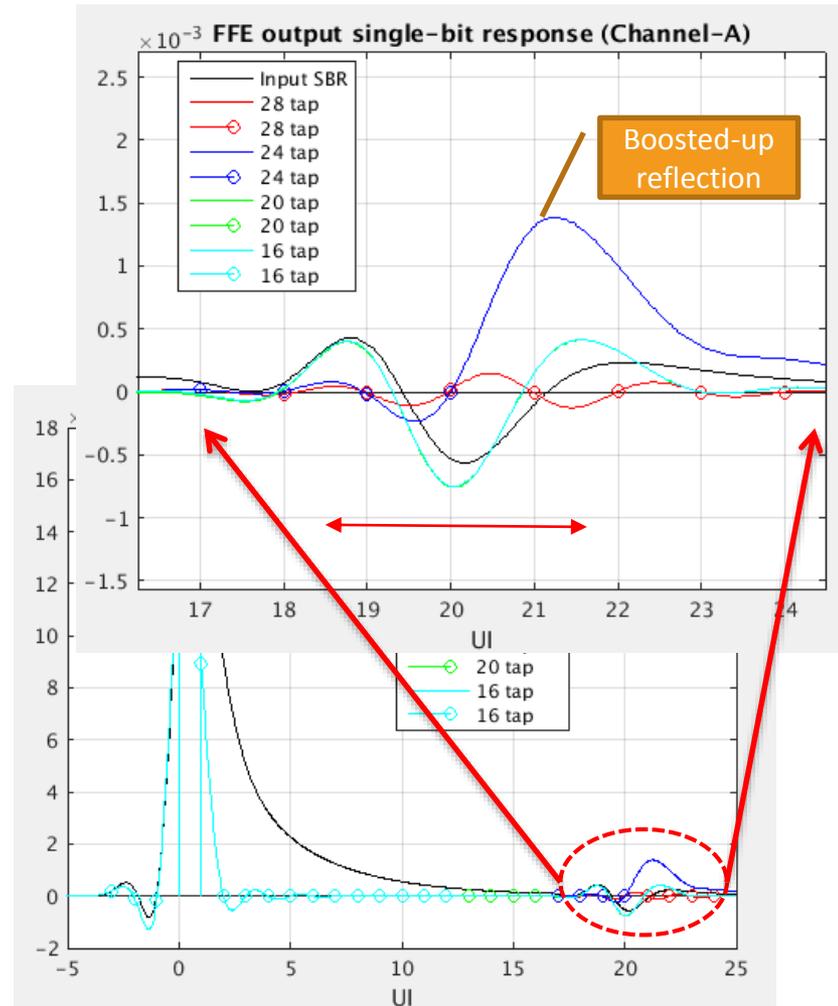
COM Values by ver. 2.41

Channel	16-tap FFE	20-tap FFE	24-tap FFE	28-tap FFE
A	2.65 dB	2.66 dB	<b>2.26 dB</b>	5.55 dB
B	-0.38 dB	-0.29 dB	0.10 dB	0.59 dB
C	-1.92 dB	-1.94 dB	<b>-1.83 dB</b>	-1.47 dB
D	2.51 dB	2.51 dB	3.26 dB	5.11 dB
E	2.08 dB	2.08 dB	<b>1.79 dB</b>	4.38 dB

# Non-Monotonic Behavior of COM

## 2.41 – Varying FFE Tap #

- Apply same TxFFE & CTLE for all cases
  - TxFFE = [0 0.05 -0.2 0.75 0], gdc = -10, gdc2 = -2
- From 'Input SBR', there is reflection during 19 ~ 21 UIs after main cursor
- For 16-tap & 20-tap cases
  - Not cover 'reflection': COM  $\approx$  2.7 dB
- For 28-tap cases
  - Overall 'reflection' is covered: COM  $\approx$  5.6 dB
- For 24-tap cases
  - Due to some 'reflection' is NOT covered in the 'FV' \*<sub>1</sub>, it's boosted up by FFE
  - COM value degrades to  $\approx$  -0.45 dB < 2.7 dB (20-tap)
- Question: is this the true behavior of Receiver?

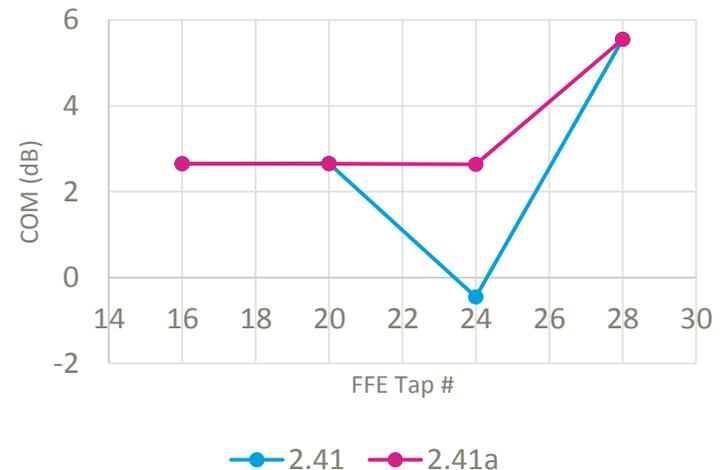


\*1. Refers to Page 7 of "[Mellitz 3ck 01 0718.pdf](#)" for details of the 'forcing vector (FV)'

# Solution (2.41a) – Modifications from COM 2.41

- Apply same TxFFE & CTLE for all cases
  - TxFFE = [0 0.05 -0.2 0.75 0], gdc = -10, gdc2 = -2
- In order to avoid 'non-monotonic behavior', we tried COM 2.41a
  - Take FFE with 24 taps as an example
  - Range of coefficients to be calculated [Pre, Main, Post] = [3, 1, 20]
  - Range of forcing vector (FV) is extended from [3, 1, 20] to [3, 1, 20+2], on purpose of considering overall reflections when calculating FFE/DFE coefficients
- Results
  - We can find COM value monotonic increases by increasing FFE tap number for Channel A
  - However, it can't apply generally to solve issues for other channels

COM Comparisons for Channel A



Link: [SBR of 2.41a](#)

# COM 2.41a Results

COM Values by ver. 2.41a

Channel	16-tap FFE	20-tap FFE	24-tap FFE	28-tap FFE
A	2.65 dB	2.65 dB	2.90 dB	5.55 dB
B	-1.56 dB	-0.21 dB	0.18 dB	<b>-0.26 dB</b>
C	-2.72 dB	-2.65 dB	-2.51 dB	-2.40 dB
D	1.57 dB	<b>1.46 dB</b>	2.90 dB	5.16 dB
E	2.67 dB	<b>2.57 dB</b>	<b>2.30 dB</b>	3.26 dB

- By 'zero-forcing' approach adopted in COM 2.41 (& 2.41a as well)
  - Crosstalk and noise not count in calculating FFE & DFE coefficients
  - May not result in 'optimal' FFE/DFE coefficients
- Question: any alternative approaches?

# Discussion & Next Step

- What alternative ways are feasible for FFE/DFE calculation?
- Exhausted search
  - Not feasible!
  - 24-tap FFE with maximum absolute value of 0.2 and resolution of 0.05 requires  $(2*0.2/0.05+1)^{24} \approx 1e23$  candidates to be calculated
- Some adaptation to reduce the complexity
  - Maybe too implementation-specific & difficult to reach consensus
- Some closed-form solution is suggested
  - Such as “Salz SNR” used by Broadcom\*<sub>1</sub>
    - Need to modify it to finite-tap version
  - Maybe MMSE-DFE\*<sub>2</sub>

\*1. Page 3 of [“healey\\_100GEL\\_01\\_0318.pdf”](#)

\*2. Reference: Book by John M. Cioffi

# Summary

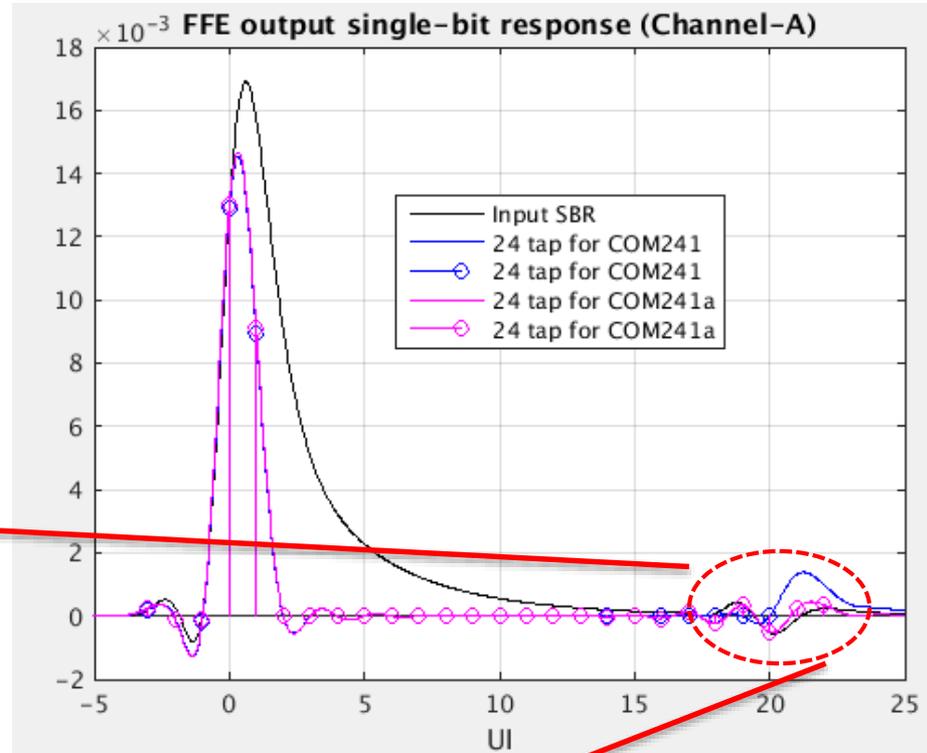
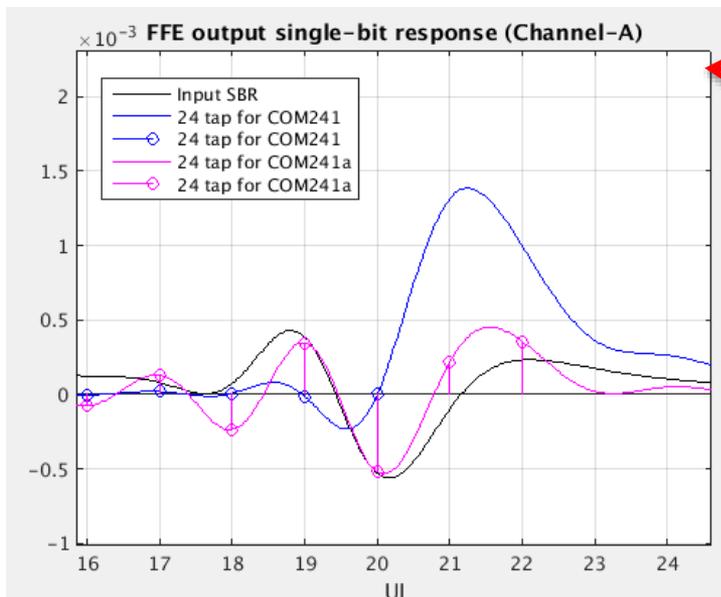
- By adopting ‘zero-forcing’ approach to calculate FFE/DFE coefficients in COM 2.41, we found
  - COM performance doesn’t monotonic increase when FFE tap increases
  - Can’t solve this issue even by extending forcing vector (FV) dimension
- Suggest to consider alternative approach to calculate FFE/DFE coefficients
  - Some closed-form preferred, such as Salz SNR, MMSE-DFE



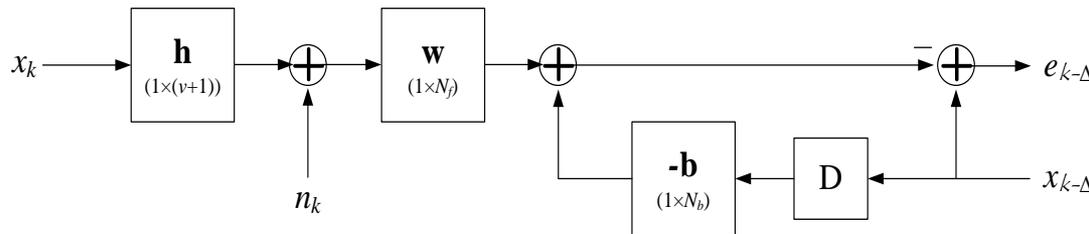
*everyday genius*

# Extending FV length by 2 – The Effects

- By same TxFFE & CTLE
- By extending 2 taps for FV range, the SBR after FFE shows smaller residue ISI comparing to COM 2.41



# Formula of MMSE solution for FFE/DFE



$$\mathbf{w} = \mathbf{1}_\Delta^* \mathbf{P}^* \left( \mathbf{P} \mathbf{P}^* - \mathbf{P} \mathbf{J}_\Delta \mathbf{J}_\Delta^* \mathbf{P}^* + \frac{1}{\varepsilon_x} \mathbf{R}_{nn} \right)$$

$$\mathbf{b} = \mathbf{w} \mathbf{P} \mathbf{J}_\Delta \quad \sigma_e^2 = \varepsilon_x (1 - \mathbf{w} \mathbf{P} \mathbf{1}_\Delta)$$

$$SNR_{biased\ MMSE\text{-}DFE} = \frac{\varepsilon_x}{\sigma_e^2} = \frac{1}{1 - \mathbf{w} \mathbf{P} \mathbf{1}_\Delta}$$

## References

- Book by John M. Cioffi
  - <https://web.stanford.edu/group/cioffi/book/>
- Details in Chapter 3.7.4  
FIR MMSE-DFE
- We may try to adopt MMSE approach to calculate
  - FFE and DFE coefficients