

# Exploration of SCMR Limits in 802.3ck D2.3

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For IEEE 802.3ck

# Outlines

- Background
- Performance impact analysis of CM noise
- SCMR values under different scenarios
- Summary & Proposal

## Background – New SCMR (min) in 802.3ck D2.3

- Due to the new adopted TP0v method for 100GEL C2C/KR clauses
  - The original 30 mV, AC common-mode RMS (max), spec is not valid – the value depends on TP0v IL, which is variant
  - Signal to AC common-mode noise ratio, SCMR (min), was adopted in D2.3
    - However, there is no validations yet for 16 dB limit
- Try to analyze what's the appropriate SCMR (min) limit
  - 16 dB is too large, propose 13 dB instead

# Recap of SCMR (min) Spec

## 163.9.2.7 Signal to AC common-mode noise ratio

Signal to AC common-mode noise ratio is calculated using Equation (163–2). The procedure in 162.9.3.1.1 is used to determine the differential-mode linear fit pulse response  $p(k)$ . The peak-to-peak AC common-mode voltage is defined as the AC common-mode voltage (see 93.8.1.3) range measured at TP0v that includes all except  $10^{-4}$  of the measured distribution, from 0.00005 to 0.99995 of the cumulative distribution. The signal to AC common-mode noise ratio shall meet the specification for SCMR (min) in Table 163–11.

$$SCMR = 20 \log_{10} \left( \frac{P_{max}}{V_{CMPP}} \right) \quad (163-2)$$

where

- $SCMR$  is the signal to AC common-mode ratio in dB
- $P_{max}$  is the maximum value of the differential-mode linear fit pulse response  $p(k)$
- $V_{CMPP}$  is the peak-to-peak AC common-mode voltage

- Purpose – explore SCMR values with different scenarios to come out reasonable SCMR limit

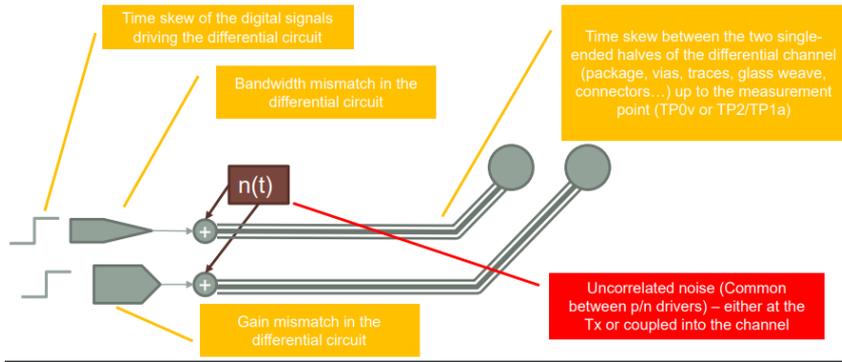
- Differential peak signal is compared with pk-to-pk AC common-mode voltage (at prob. of  $1e-4$ )
  - $V_{CMPP}$  strongly depends on components of CM noise – whether it's Gaussian or not?

### 5—Summary of transmitter specifications at TP0v

meter	Reference	Value	Units
Signaling rate, each lane (range)		53.125 ± 50 ppm <sup>a</sup>	GBd
Differential pk-pk voltage (max) <sup>b</sup>	93.8.1.3	30	mV
Transmitter disabled Transmitter enabled		1200	mV
DC common-mode voltage (max) <sup>b</sup>	93.8.1.3	1	V
DC common-mode voltage (min) <sup>b</sup>	93.8.1.3	0.2	V
Signal to AC common-mode noise ratio, SCMR (min)	163.9.2.7	16	dB

# Identify AC CM noise sources

- Sources of common mode AC output had been discussed & separated into the following parts in [ran 3ck 04 1020](#)

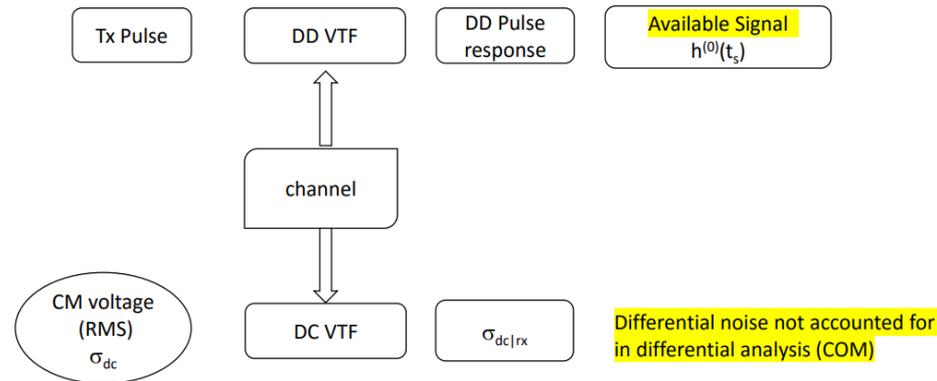


- CM noise (uncorrelated with the desired signal) (**CM1**)
  - High-freq component (**CM1a**), such “supply noise”, typically below  $\sim 1$  MHz ([ran 3ck adhoc 01 063021](#))
    - Let’s model it as dual dirac with pk2pk value as  $2 * A_{DD1}$
  - Wideband components (**CM1b**), let’s model it as Gaussian noise with  $\sigma_{CM}$
- CM signal (correlated with desired signal) (**CM2**)
  - Assumed it can be compensated by RX ([ran 3ck 04 1020](#))
  - Let’s model it as dual dirac with pk2pk value as  $2 * A_{DD2}$

# Performance Impact of CM1 – $SNR_{TX}$

- Uncorrelated CM noise (**CM1** with  $\sigma_{ucm}$  by combining  $A_{DD1}$  &  $\sigma_{CM}$ )
  - $\sigma_{ucm}^2 = (A_{DD1}^2 + \sigma_{CM}^2)$
- Adopted the modified COM code in [mellitz 3ck adhoc 01 061720](#)
  - CM voltage (RMS) at TPO -  
 $\sigma_{dc} = \sigma_{ucm}$
  - Converting by common-mode to differential mode conversion loss of channel (sdc21)
  - Evaluate the impact by  $SNR_{TX}$  degradation

## Simple First Estimate



# Performance Impact of CM1 – $SNR_{TX}$ loss < 0.1 dB

File	AC CM ( $\sigma_{ucm}$ ) (mV)	New $SNR_{Tx}$ (dB)					sdc21_Peak (dB)
		30	17.5	15	10	1	
Kateri/Bch2_b7p5_7_		32.0	32.3	32.4	<b>32.4</b>	32.5	-38.9931
Kateri/Bch2_b6_7_t		31.9	32.3	32.3	<b>32.4</b>	32.5	-38.5647
Kateri/CAch2_a2p5_t		30.4	31.7	31.9	32.2	32.5	<b>-32.8423</b>
Heck/Cable_BKP_28dB_0p575m_more_isi_thru1		31.5	32.1	32.2	<b>32.5</b>	32.5	-38.3842
Mellitz/CaBP_BGAVia_Opt2_28dB_THRU		32.4	32.5	32.5	<b>32.5</b>	32.5	-51.1657
Zambell/Thru_Link_910_C1_Pr_14_to_Pr_5		31.7	32.2	32.3	<b>32.4</b>	32.5	-40.547
Gore/C2C_PCB/SYSVIA_20dB_thru		31.3	32.1	32.2	<b>32.4</b>	32.5	-35.5721
Palkert/THRU_VL5_OD-BP-Channel_16inch_16inch		25.7	28.9	29.6	31.0	32.5	<b>-30.0389</b>

- IEEE 8x baseline KR channels analyzed
- Original  $SNR_{TX}$  is 32.5 dB
- By sdc21\_Peak <= -35 dB &  $SNR_{TX}$  >= 32.4 dB → AC CM ( $\sigma_{ucm}$ ) <= **10 mV**

# Limited Values of Components of CM Voltage

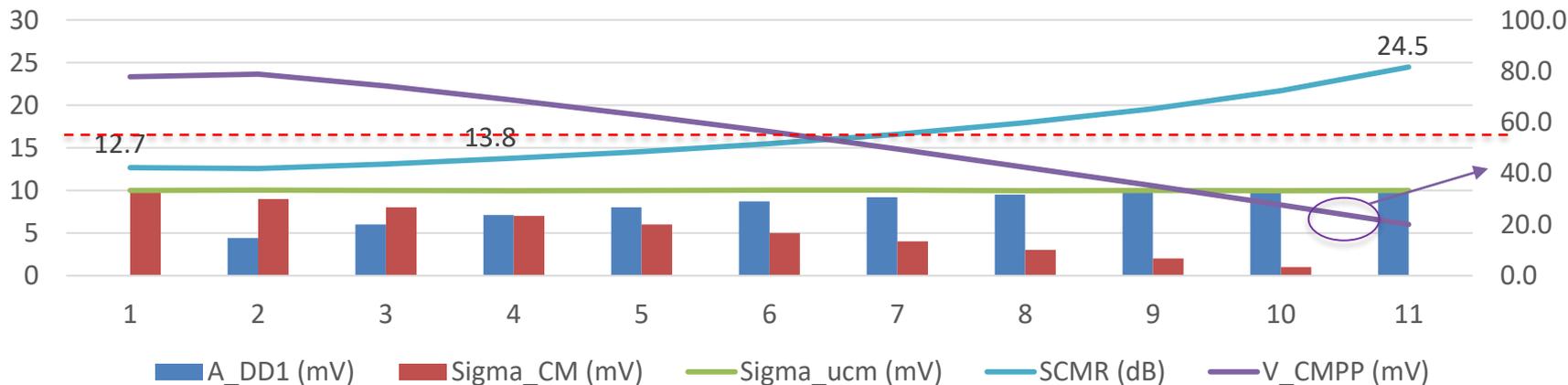
Component	Symbol	Performance impact	Limited value (mV)	Notes
CM1a: Uncorrelated CM noise – high freq.	$A_{DD1}$	Impact is limited by 0.1 dB $SNR_{TX}$ loss	$\sigma_{ucm} \leq 10,$ $\sigma_{ucm}^2 = (A_{DD1}^2 + \sigma_{CM}^2)$	<ul style="list-style-type: none"> <li>SCMR strongly depends on ratio of <math>A_{DD1}</math> &amp; <math>\sigma_{CM}</math></li> <li>10 mV <math>\sigma_{ucm}</math> results in <b>SCMR = 13.8 dB (failed 16 dB spec) with <math>A_{DD1} = \sigma_{CM}</math></b></li> </ul>
CM1b: Uncorrelated CM noise – wideband	$\sigma_{CM}$			
CM2: Correlated CM signal	$A_{DD2}$	Assumed no impact	5~10 (50 in <a href="#">mellitz 3ck 01 0921</a> )	Will easily fail SCMR 16 dB spec limit → need to exclude this from SCMR calculation

- ❑  $\sigma_{ucm} = 10$  mV aligned with [mellitz 3ck 01 0921](#)
- ❑ Large value of  $A_{DD2}$  doesn't impact RX, but will fail SCMR spec → two options
  - ❖ Option 1 – reduce SCMR limit by considering  $A_{DD2}$  component
  - ❖ Option 2 – define CM specs for correlated & uncorrelated ([mellitz 3ck 01 0921](#))

# SCMR with $\sigma_{ucm} = 10$ mV

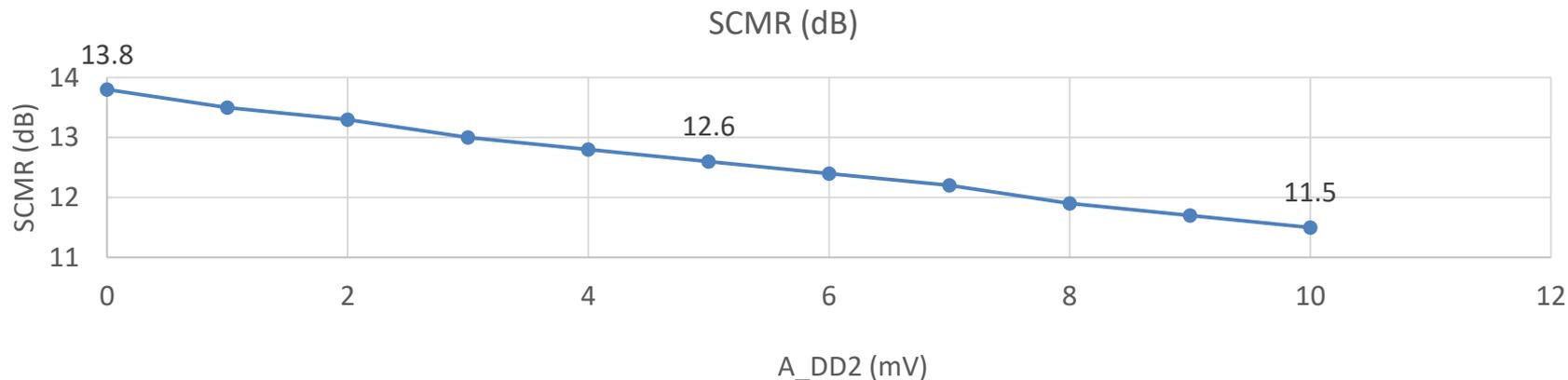
## sweeping ratio of $A_{DD1}$ & $\sigma_{CM}$ , with $A_{DD2} = 0$ mV

$P_{max} = 335$  mV



- ❑  $P_{max} = 335$  mV is derived from referenced TP0v test fixture (163B.3) & scaled up to TP0 ([append.](#))
- ❑ Larger  $\sigma_{CM}$  induces larger  $V_{CMPP}$ , and therefore smaller SCMR
  - ❖ You need to limit  $\sigma_{CM} \leq 4.5$  mV to meet 16 dB SCMR, even  $A_{DD2}$  doesn't count in yet
  - ❖ By equal partition in  $A_{DD1}$  &  $\sigma_{CM}$ , the appropriate SCMR spec is 13.8 dB

SCMR with  $\sigma_{ucm} = 10$  mV,  
 $A_{DD1} = \sigma_{CM}$ , by sweeping  $A_{DD2} = 0 \sim 10$  mV



- ❑ Although  $A_{DD2}$  doesn't have big impact to RX, but contributes a lot to reduce SCMR value
  - ❖ Reduces SCMR with 0.8 ~ 1.7 dB for  $A_{DD2}$  in 5 ~ 10 mV
- ❑ It may change too much to D2.3 if excluding  $A_{DD2}$  in SCMR or defining CM specs for correlated & uncorrelated ([mellitz 3ck 01 0921](#))
  - ❖ Propose to further reduce SCMR spec limit to reflect this issue, to say 13 dB

# Summary and Proposal

- The simulation & analysis of AC CM noise shows
  - $\sigma_{ucm} \leq 10$  at TP0 is the appropriate spec to limit impact to RX
- The SCMR values are calculated by considering
  - Uncorrelated CM noise (high freq. + wideband)
  - Correlated CM signal
- SCMR values strongly depends on ratio of high freq. & wideband components of uncorrelated CM noise
  - Take equal partition, 16 dB is too much a value
- Correlated CM signal further reduces SCMR values, although it only has little impact to RX
  - Need further margin for it
- Propose to change SCMR spec limit from 16 dB to 13 dB
  - Apply both of C2C & C163

Thank You



# Information to derive $P_{max} = 335$ mV at TP0

## 163B.3 Reference Values

For this test fixture, the reference values determined according to the methodology in 163A.3 using the parameters supplied in Clause 163 are listed in Table 163B-1.

Table 163B-1—Summary of transmitter reference values at TP0v

Parameter	Reference	Value	Units
Effective return loss, $ERL^{(ref)}$	163A.3.1.2	12.95	dB
Transmitter steady-state voltage, $v_f^{(ref)}$	163A.3.1.1	0.409	V
Transmitter linear fit pulse peak, $v_{peak}^{(ref)}$	163A.3.1.1	0.237	V
Transmitter pulse peak ratio, $R_{peak}^{(ref)}$	163A.3.2.1	0.580	-

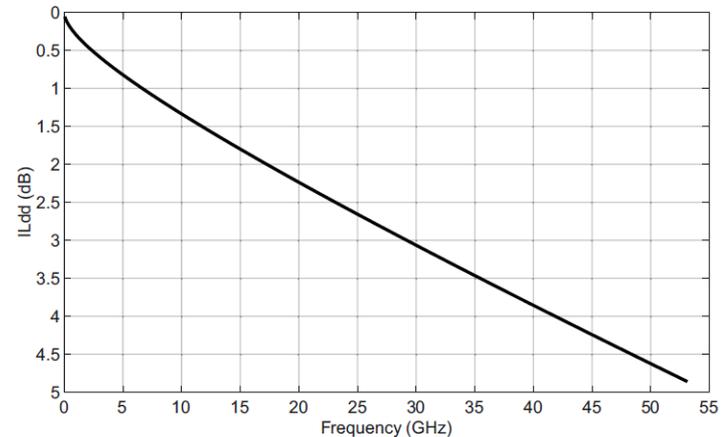


Figure 163B-1—Example test fixture differential-mode to differential-mode insertion loss

□ 237 mV (@ TP0v with ~3 dB IL), simply scaled up by 3 dB (approximately), results in 335 mV @ TP0