

# **Residual intersymbol interference**

(comment R1-28)

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# Introduction

- Residual intersymbol interference (ISI) in the transmitter output waveform is constrained by the ISI\_RES specification
- Per 163.9.2.6, ISI\_RES related to the linear fit error computed for a linear fit pulse length  $N_p = 11$
- Signal-to-noise-and-distortion ratio (SNDR) includes a linear fit error term computed using  $N_p = 200$
- This term is primarily associated with distortion ( $N_p = 200$  was chosen to reduce the influence of residual ISI on SNDR)
- ISI\_RES therefore combines residual ISI and distortion
- The model used determine the ISI\_RES limit (see [dudek\\_3ck\\_01\\_0721](#)) was linear hence the SNDR linear fit error term was likely close to 0

# Problem statement #1

- ISI\_RES combines residual ISI and distortion
- Since SNDR controls distortion, this is double-counting
- ISI\_RES limit was derived for transmitters whose SNDR was dominated by uncorrelated noise

Parameter	Case 1	Case 2	Case 3
RMS uncorrelated noise	2.37%	1.5%	0%
RMS linear fit error for $N_p = 200$	0%	1.84%	2.37%
RMS residual ISI	2.82%	2.82%	2.82%
RMS linear fit error for $N_p = 11$	2.82%	3.37%	3.68%
SNDR, dB	32.5	32.5	32.5
ISI_RES, dB	-31	-29.5	-28.7

ISI\_RES limit violated despite having an “acceptable” level of residual ISI

## Problem statement #2

- ISI\_RES is measured with  $N_p = 11$  and  $D_p = 4$  so it includes all errors after post-cursor 6
- A dispersive channel (package, host, test fixture) can generate an ISI tail that extends beyond post-cursor 6
- A receiver can generally be expected to deal with such a tail – reflections are the primary concern
- ISI\_RES degraded by inconsequential ISI
- Transmitter equalization has been suggested as a means to reduce the impact of the tail (see [ran\\_3ck\\_adhoc\\_01\\_032322](#))
- A low-frequency pole/zero pair is a more efficient tool for tail reduction

# Inconsistency

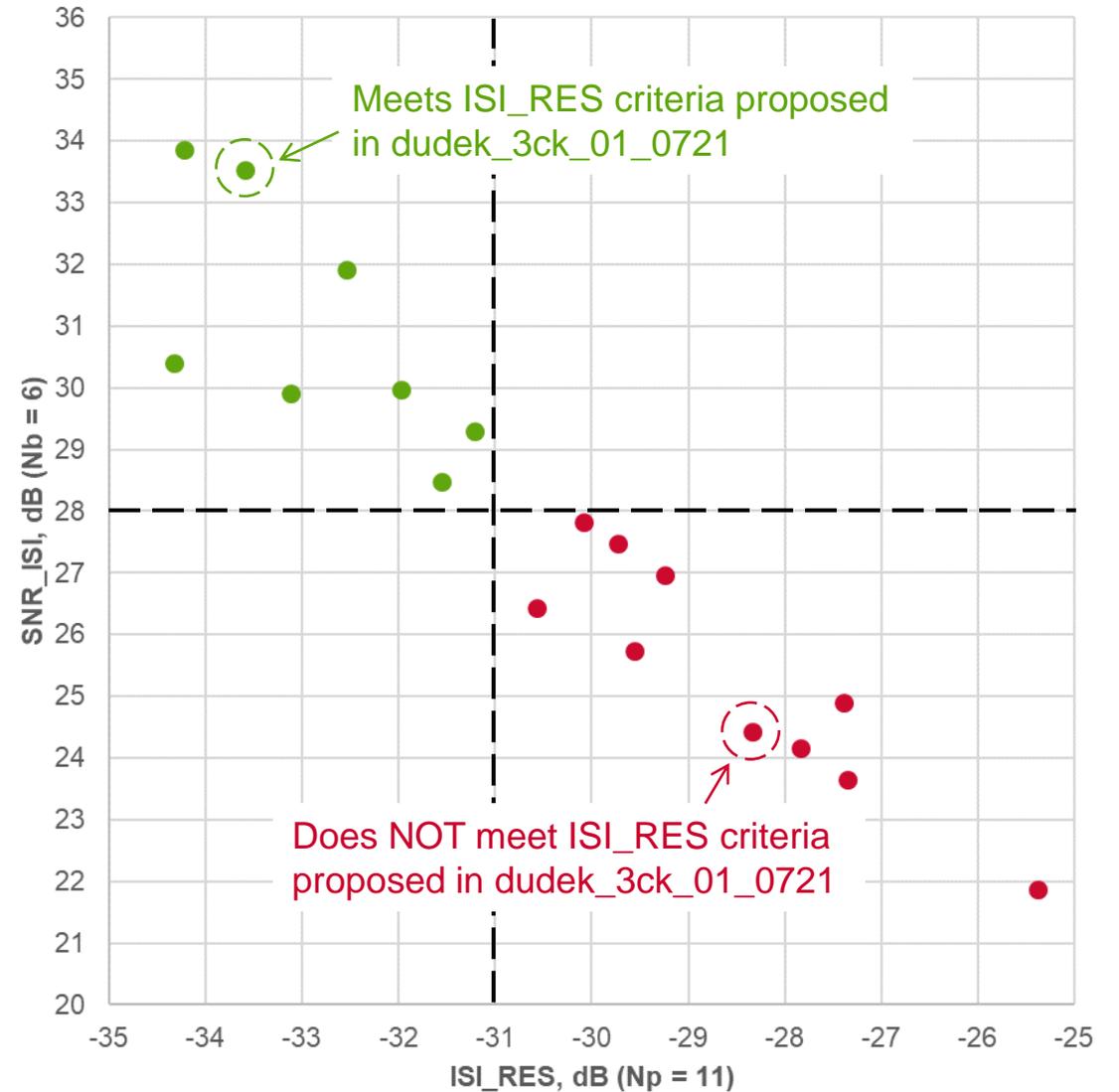
- Effective return loss (ERL) considers the alignment of reflections at the sampling point
- ERL uses the sampling phase that maximizes the error
- In contrast, ISI\_RES combines all residual errors irrespective of phase
- It would be better for reflections to be treated consistently between ERL and ISI\_RES

# Proposed solution

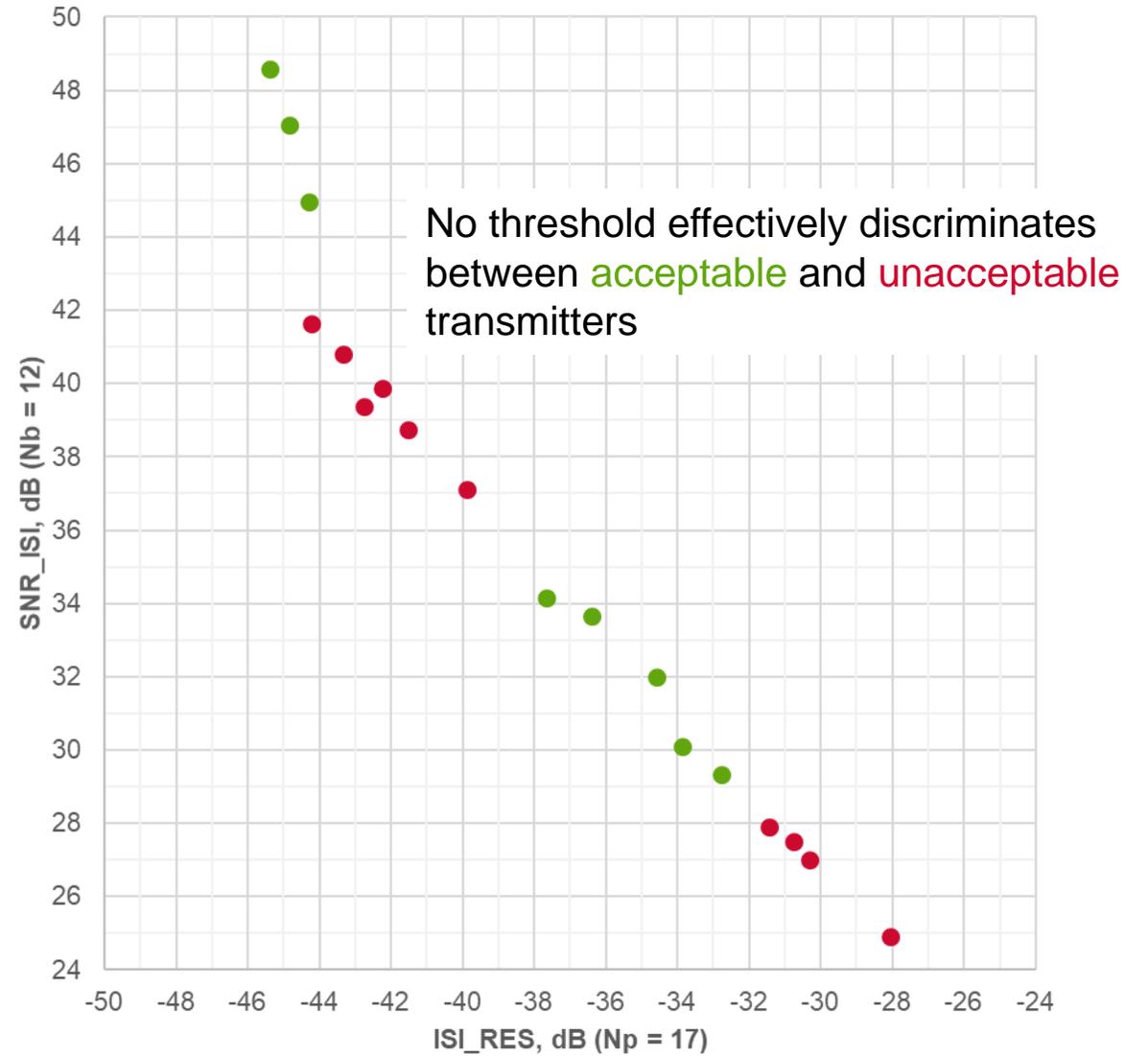
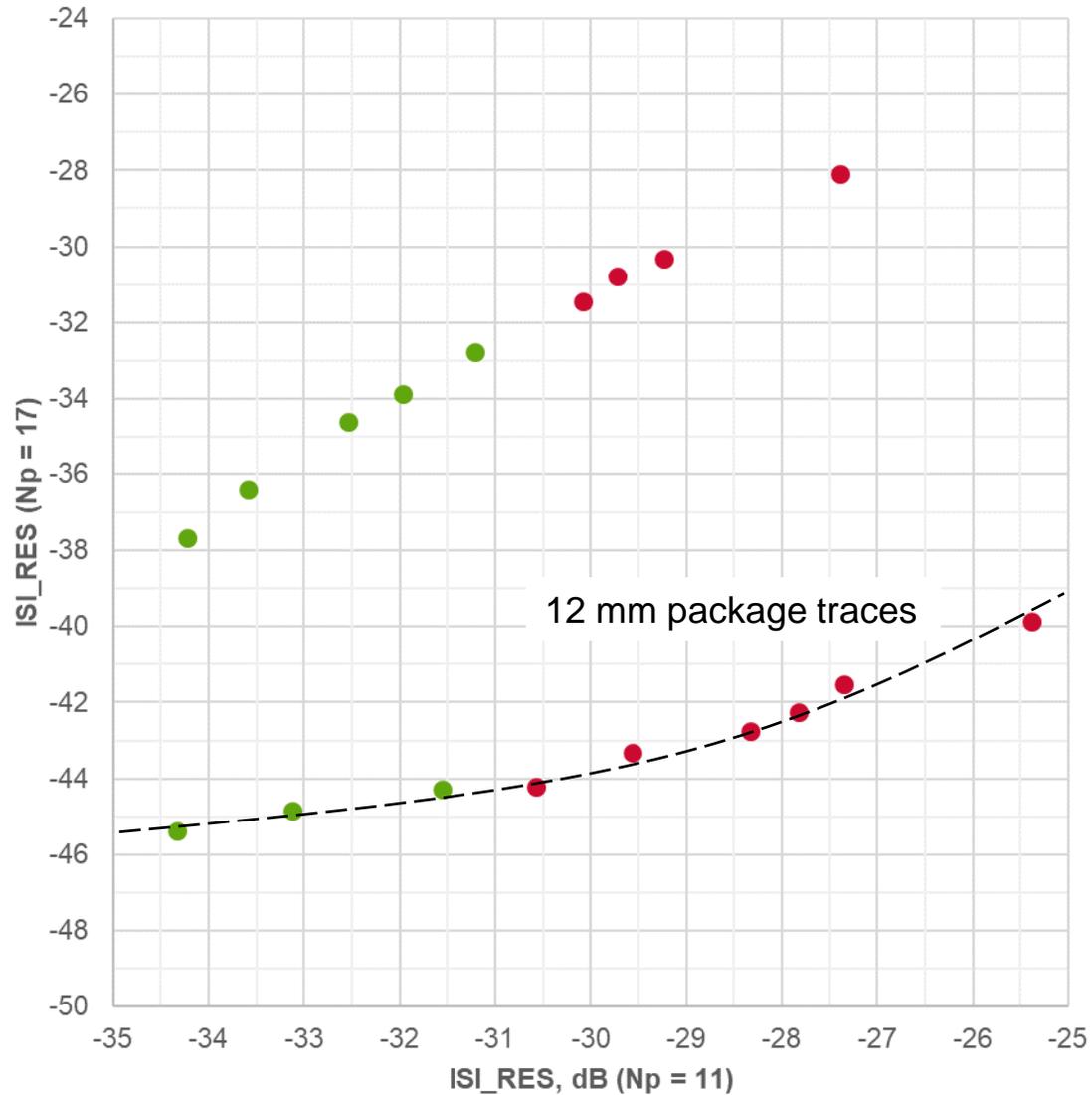
- Replace ISI\_RES with SNR\_ISI as defined in 120D.3.1.7 except ...
- ... use the continuous time filter parameters in Table 163–11 and ...
- ... for calculation of  $ISI_{cursors}$ , sweep phase  $\pm 0.5$  UI around  $t_p$  and choose the phase that minimizes SNR\_ISI
  
- SNR\_ISI does not include SNDR linear fit error
- SNR\_ISI includes a reference equalizer to reduce the dispersive tail and focus on reflections
- SNR\_ISI accounts for the alignment of reflections at the sampling point (similar to ERL)
- SNR\_ISI is already part of the base standard – there is no need to add a new residual ISI metric

# Correlation of SNR\_ISI to ISI\_RES at TP0v

- 18 transmitter models from slide 9 of [dudek\\_3ck\\_01\\_0721](#)
- 4 dB test fixture
- $N_b = 6$  (agrees with  $N_p = 11$ )
- Assume transmitters that meet the ISI\_RES requirement also yield acceptable COM (and vice versa)

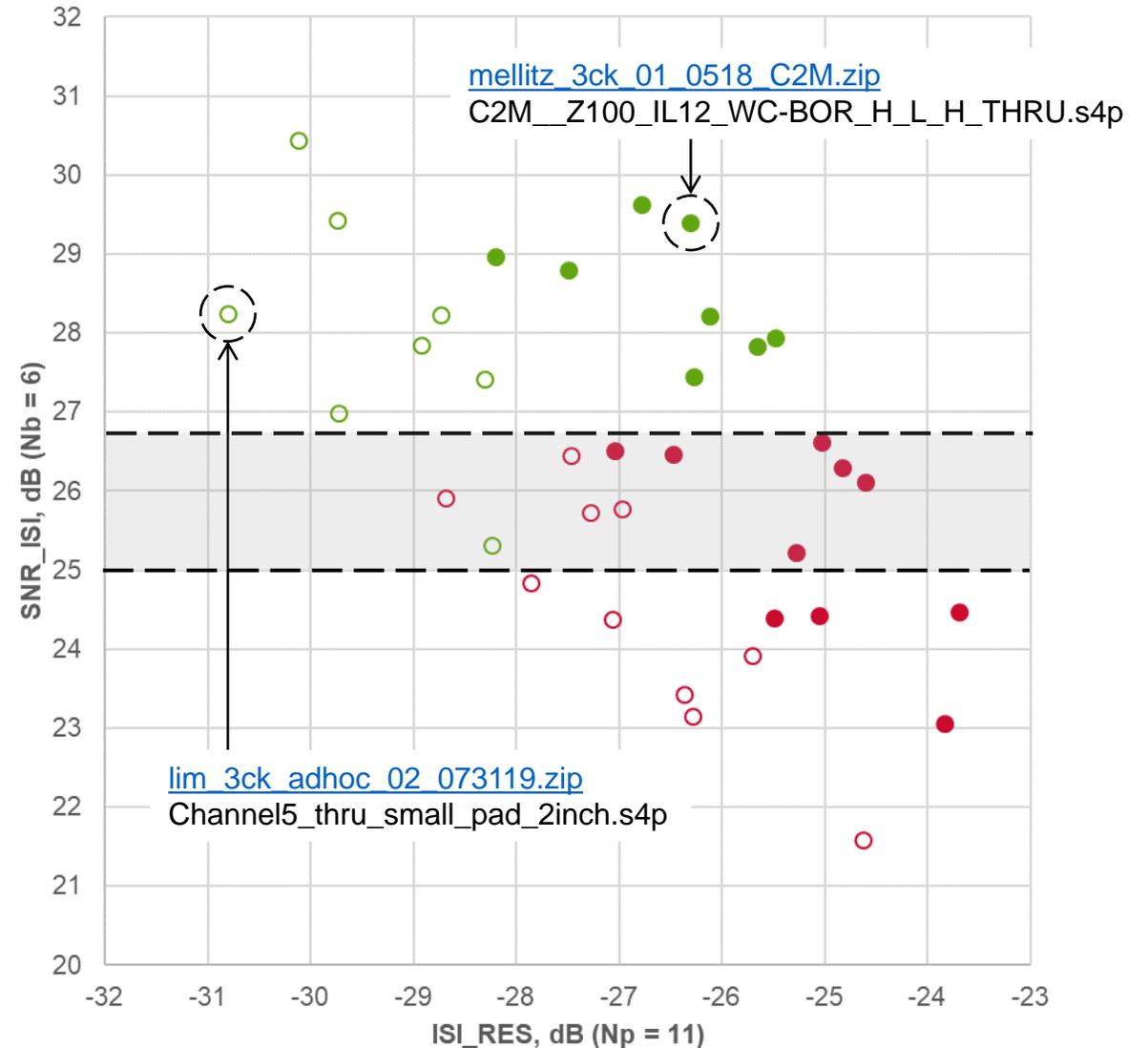


# What if $N_b = 12$ ? (TP0v results)

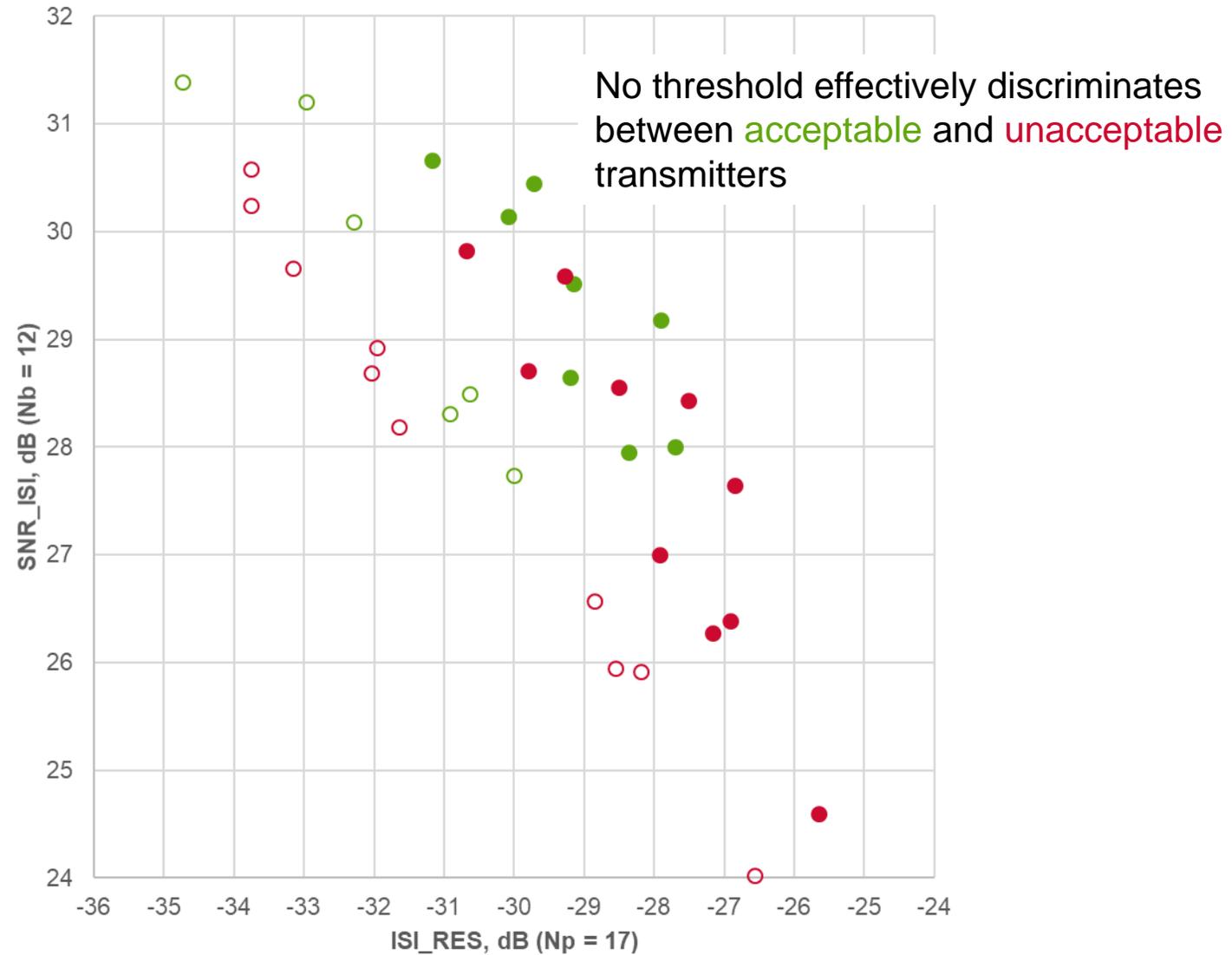


# Correlation of SNR\_ISI to ISI\_RES at TP2

- 18 transmitter models from slide 9 of [dudek\\_3ck\\_01\\_0721](#)
- Different host models
- $N_b = 6$  (agrees with  $N_p = 11$ )



# What if $N_b = 12$ ? (TP2 results)



# Proposed limits

- Set  $N_b$  to 6
- For Clause 163 and Annex 120F, set SNR\_ISI (min.) to 28 dB
- For Clause 162, set SNR\_ISI (min.) to 26.7 dB
- Requirements need only be met for one transmitter equalizer setting e.g., the one that maximizes SNR\_ISI