

# CTLE for the C2M reference receiver

(supporting comment 127)

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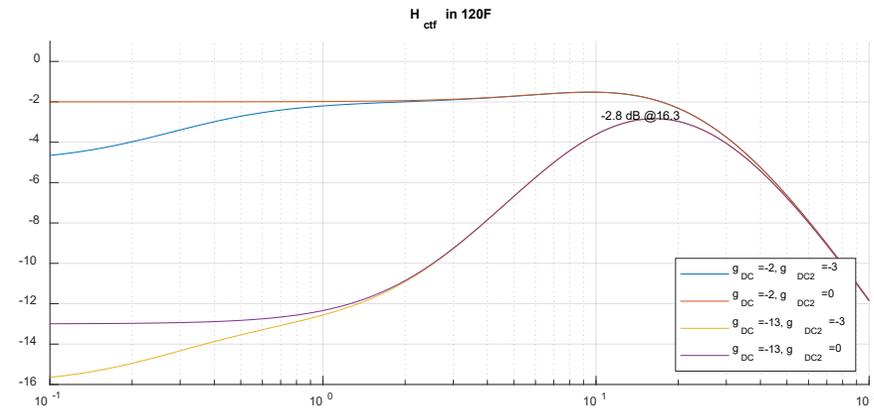
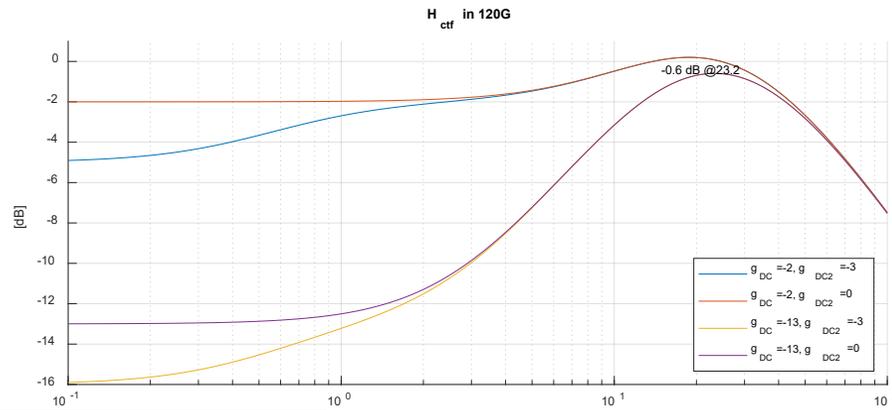
# Outline

- Examine the reference CTLE model in 120G (C2C)
- Compare to 120F (C2C)
- Compare to 120E (50G PAM4 C2M) and 83E (25G NRZ C2M)
- Consider differences, and why should we care
- Proposal for change, with some results

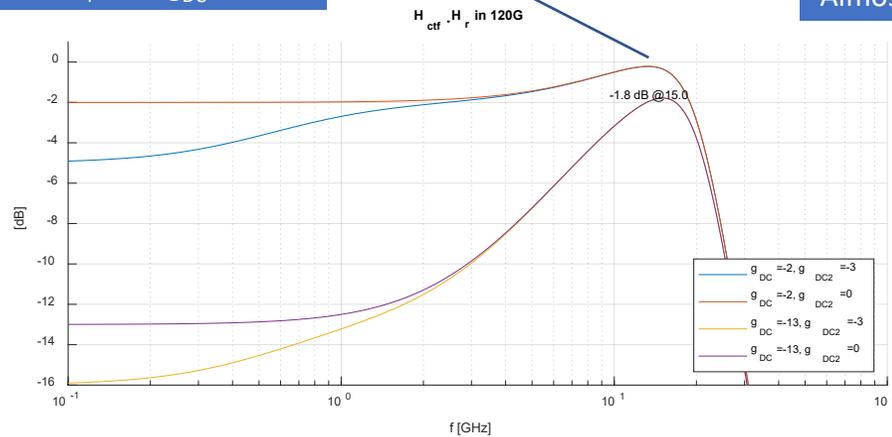
# A look at Annex 120G CTLE

- CTLE transfer functions in annex 120G are based on Annex 93A (COM) equations, but with unusual parameters
  - In other places where these equations are used, we have  $f_{p1}=f_z$ , and  $f_{p2}=f_b$
  - In 120G, these four parameters are different from each other
- The resulting CTLE is not passive (peak > 0 dB) for some values of  $g_{DC}$  (e.g. 0 dB)
  - With  $g_{DC} = -2$  dB, after the specified  $H_r$  transfer function, the peak close to 0 dB (but not exactly)
  - But with lower values of  $g_{DC}$  the peak drops below 0 dB (down to -1.8 dB)
- The reason for this choice of parameters is unclear
  - Limiting max  $g_{DC}$  to -2 dB seems to be an attempt to hit 0 dB – it has been changed across drafts (not stated explicitly)
  - It is not claimed to be optimal or to match reasonable implementations
- All resulting settings have some peaking and negative DC gain
  - Unlike other places that use COM equations

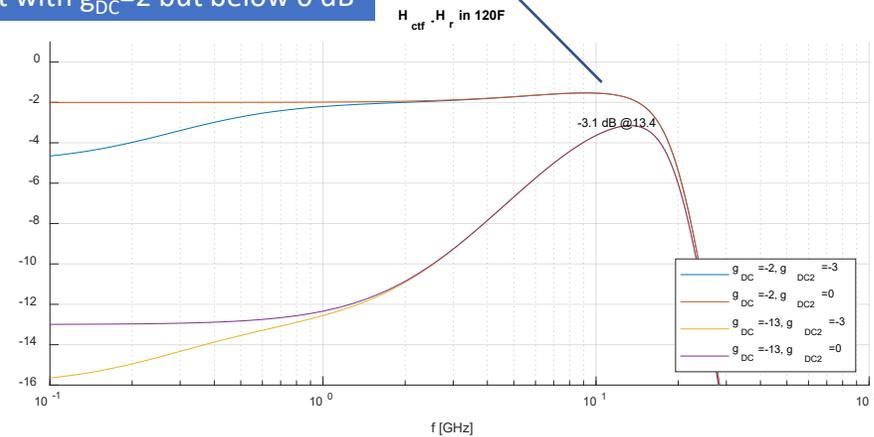
# CTLE curves in 120G (host output) vs. 120F



Up to 0 dB after H<sub>r</sub> with  $g_{DC} = 2$



Almost flat with  $g_{DC} = 2$  but below 0 dB



Note that for minimum  $g_{DC}$ , the peaking frequencies in 120F and 120G are very close, but the peaks are different

# CTLE curves in previous C2M annexes

120E used equations which create zeros/poles equivalent to typical COM CTLEs, but with a gain factor  $G$  to make all curves touch 0 dB

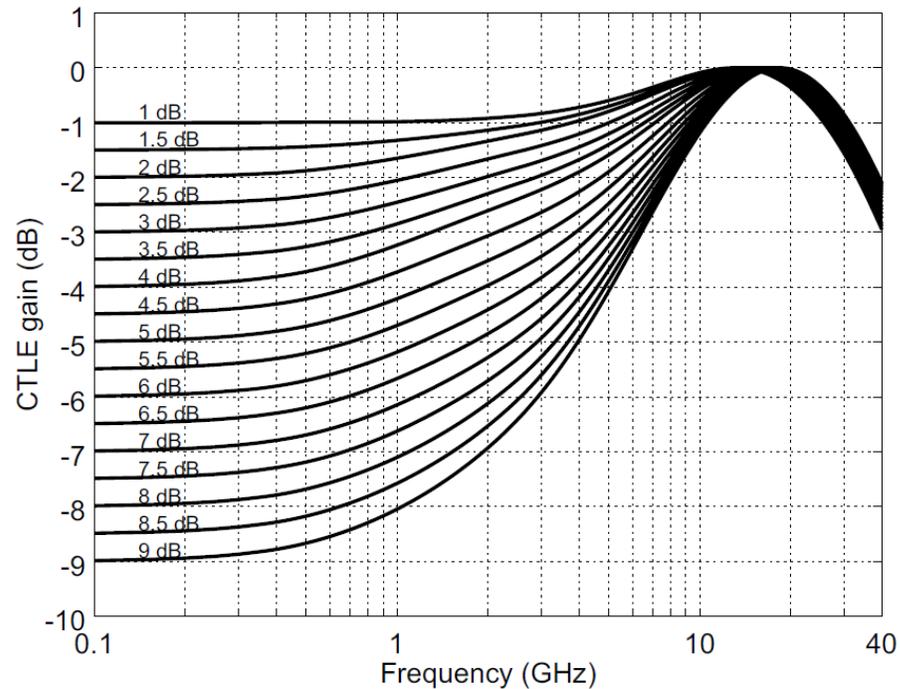


Figure 120E-9—Reference continuous time linear equalizer (CTLE) characteristic

83E used somewhat different poles and zeros but also made all curves touch 0

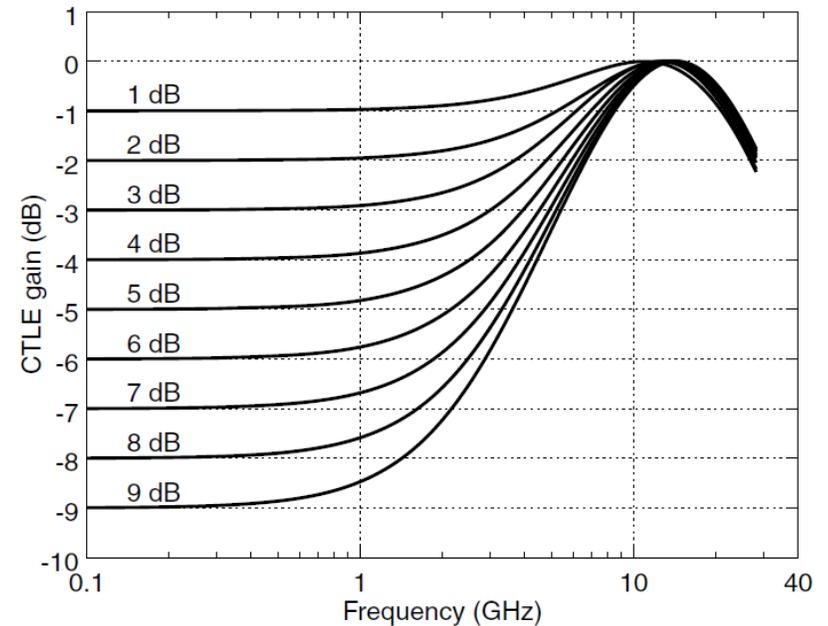


Figure 83E-10—Selectable continuous time linear equalizer (CTLE) characteristic

Note that in both cases there is no “flat” setting (and the reference receiver has no DFE – may be related)

# 120G is a new beast

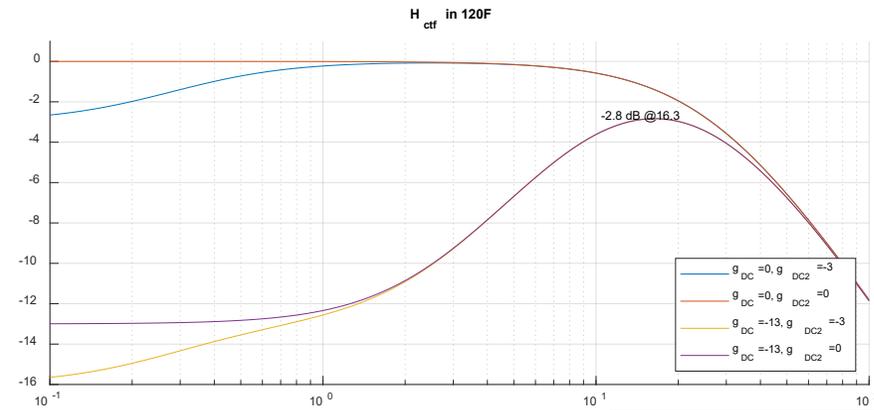
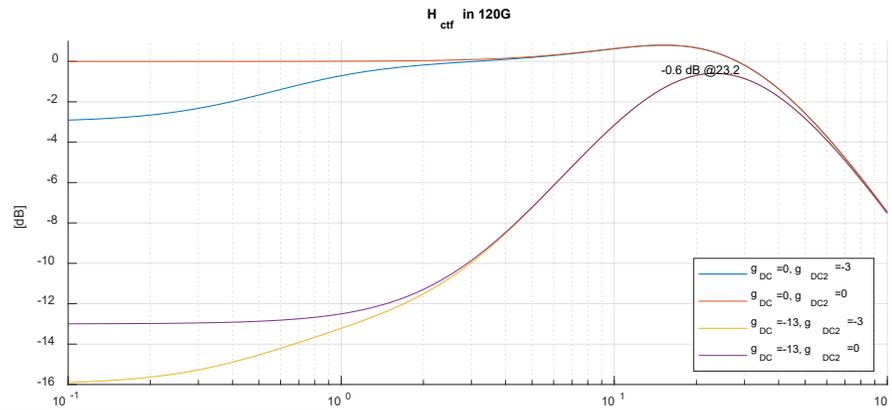
- The reference receiver includes a DFE, and a bandwidth limiting filter  $H_r$ , like C2C reference receiver (and unlike previous C2M)
  - The DFE has  $c(1)$  with minimum value of 0.1
- It requires limitations on values of  $g_{DC}$  to prevent positive gain
- CTLE Transfer functions do not touch 0 dB in all cases
  - No normalization factor
  - This means the definition of EH has changed from what it was in 120E/83E – where normalization factor was always applied

# Why should we care?

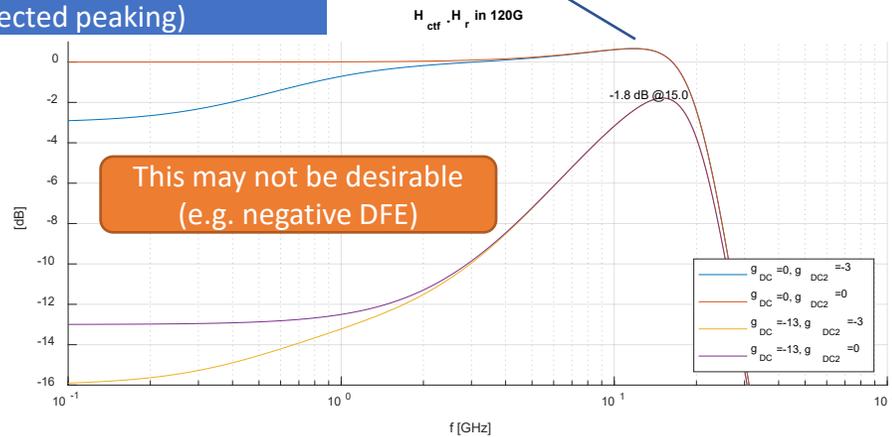
- Uniformity is better in a standard
- It is likely a better match to module and host capabilities (e.g. it is hard to avoid having some settings with no peaking)
- There may be cases (like hosts with very short traces) that with nonzero peaking create very small, or negative DFE taps, but these are not allowed.
  - These hosts might need negative pre-emphasis to pass the test (not a typical design)
  - But modules probably don't need this "tweak"
- It is expected to improve EH results and enable reducing max  $V_{diff-pTp}$  to 600 mV.

# What if we just use $g_{DC}=0$ for host output?

This is not proposed – just showing the effect on the two models

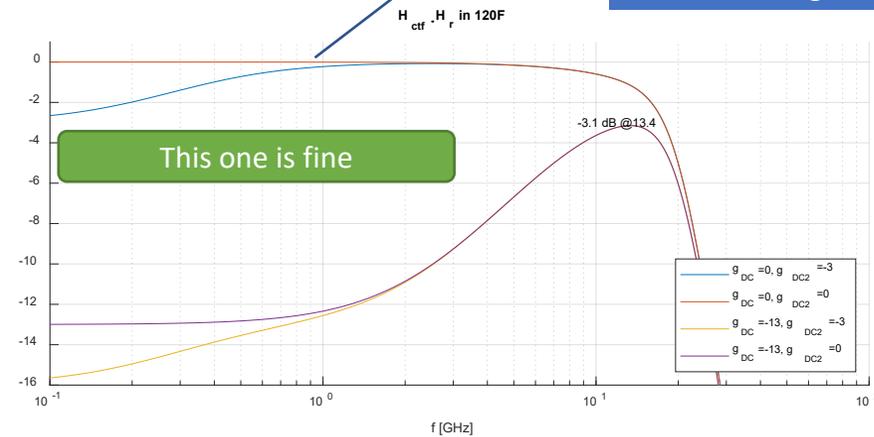


Goes above 0 dB even after  $H_r$   
(unexpected peaking)



This may not be desirable  
(e.g. negative DFE)

Flat, starting at 0 dB



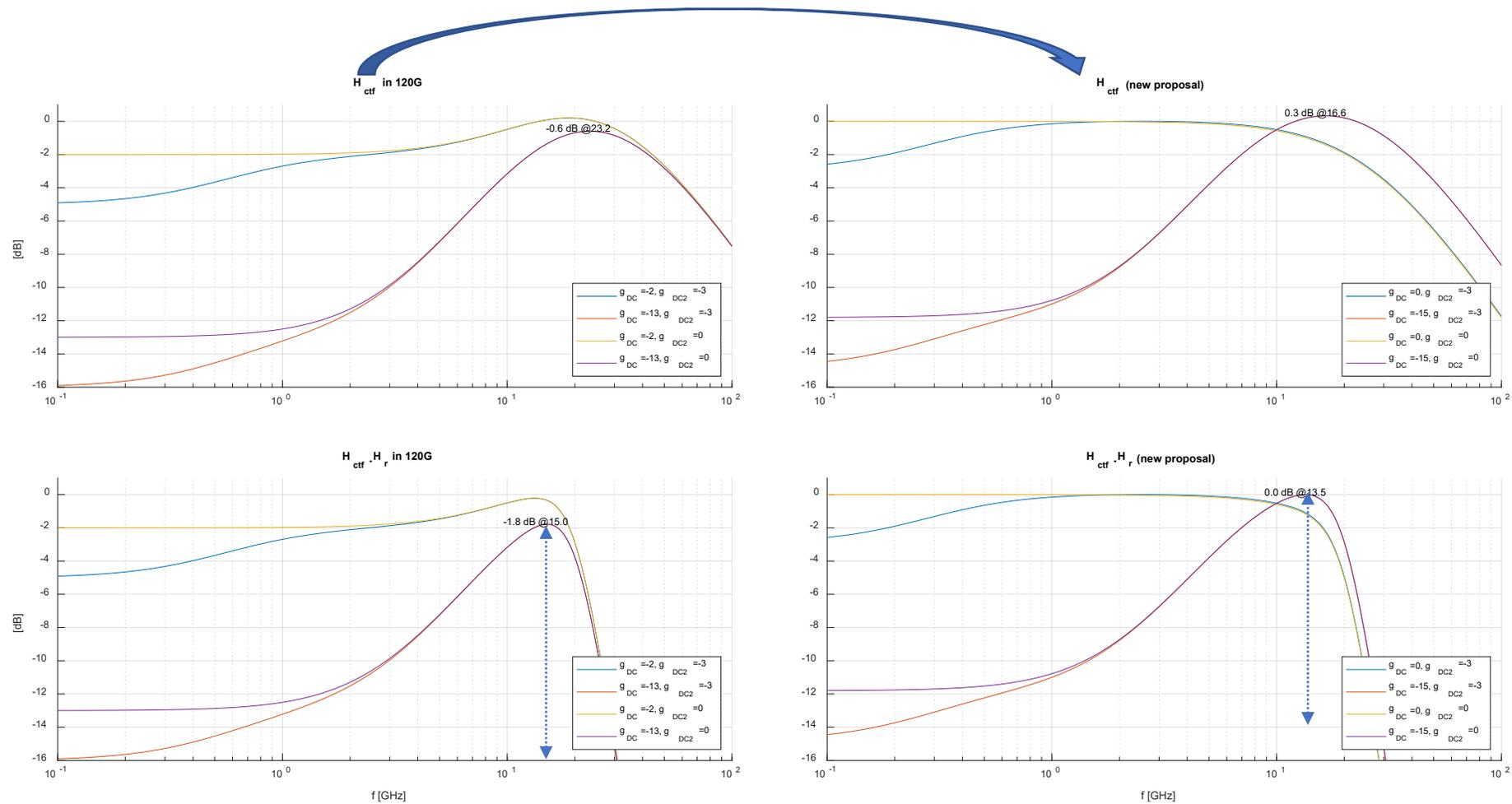
This one is fine

# Outline of proposal

- Change the CTLE parameters to be equal to the ones defined in 120F (C2C)
- Modify  $g_{DC}$  ranges:
  - Enable  $g_{DC}$  up to 0 dB to ensure negative DFE will not be needed
  - Keep maximum boost requirements as they are. This requires reducing the minimum  $g_{DC}$  by 2 dB.
  - Keep the dependence of  $g_{DC}$  range on  $g_{DC2}$  (to reduce the number of combinations)
- Additionally, add a normalization factor to make all curves touch 0 dB (as in 120E, 83E)
  - This will apply positive gain in all cases where  $g_{DC} < 0$
  - And will likely somewhat improve EH results

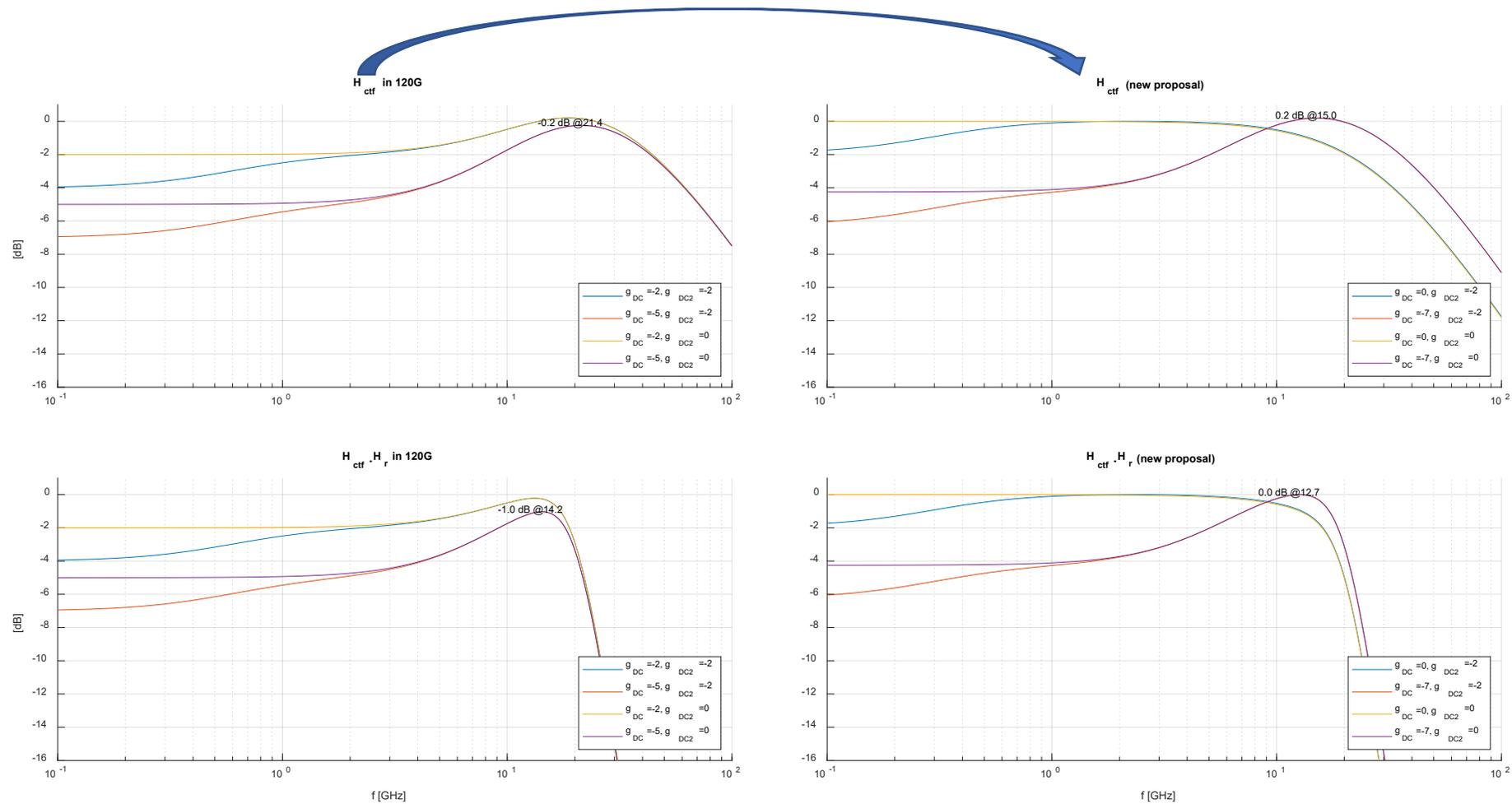
# Some results of the proposed change

# Host output (TP1a)

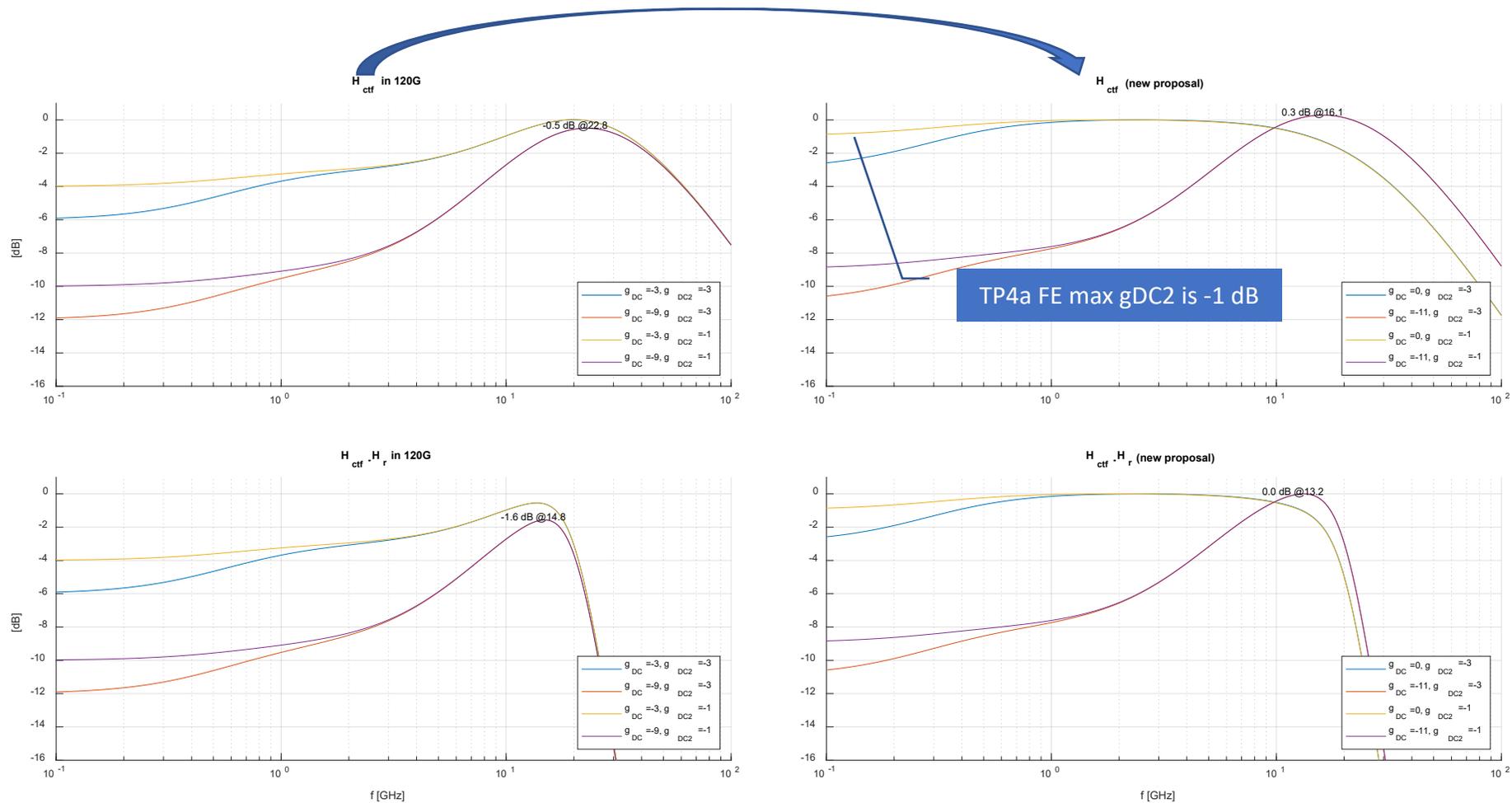


Maximum boost (peak gain minus DC gain) is about the same

# Module output (TP4 near-end)



# Module output (TP4 far-end)



It may not be necessary to allow  $g_{DC}=0$  in this case

# Proposal details

- Bring 93A.1.4.3 (Receiver equalizer) into the draft, and change Equation 93A–22 to include an additional factor  $G$ :

$$H_{ctf}(f) = G \frac{\left(10^{\frac{g_{DC}}{20}} + j\frac{f}{f_z}\right)\left(10^{\frac{g_{DC2}}{20}} + j\frac{f}{f_{LF}}\right)}{\left(1 + j\frac{f}{f_{p1}}\right)\left(1 + j\frac{f}{f_{p2}}\right)\left(1 + j\frac{f}{f_{LF}}\right)} \quad (93A - 22)$$

- Add text after the equation:

“Where  $G$  is a gain factor, whose value depends on the variable `norm_ctle` as follows:

- If `norm_ctle` is 1,  $G$  is set based on `g_DC`, `f_z`, `g_DC2`, `f_LF`, `f_p1`, and `fp2`, such that the maximum of  $H_{ctf}(f) \cdot H_r(f)$  across  $f$  is equal to 1.
  - If `norm_ctle` is 0 or is not provided by the clause that invokes this method,  $G$  is set to 1.”
- In Annex 120G:
    - Apply changes to Table 120G–12 parameters as shown in the next slide.
    - Add the parameter `norm_ctle` with value 1 (in the table or in the text of 120G.5.2).

# Table 120G – 12 changes

Table 120G–12—Eye opening reference receiver parameter values

Parameter	Symbol	Value	Units
Receiver 3 dB bandwidth	$f_r$	$0.75 \times f_b$	GHz
Continuous time filter, DC gain for TP1a Range for $g_{DC2} = 0$ Range for $-1 \leq g_{DC2} < 0$ Range for $-2 \leq g_{DC2} < -1$ Range for $-3 \leq g_{DC2} < -2$ Step size	$g_{DC}$	<del>-2 to -9</del> -2 to -12 <del>-4 to -12</del> <del>-6 to -13</del> 1.0	dB
Continuous time filter, DC gain 2 for TP1a Minimum value Maximum value Step size	$g_{DC2}$	-3 0 0.5	dB
Continuous time filter, DC gain for TP4 near-end Minimum value Maximum value Step size	$g_{DC}$	<del>-5</del> -7 <del>-2</del> 0 1.0	dB
Continuous time filter, DC gain 2 for TP4 near-end Minimum value Maximum value Step size	$g_{DC2}$	-2 0 0.5	dB
Continuous time filter, DC gain for TP4 far-end Minimum value Maximum value Step size	$g_{DC}$	<del>-9</del> -11 -3 1.0	dB
Continuous time filter, DC gain 2 for TP4 far-end Minimum value Maximum value Step size	$g_{DC2}$	-3 -1 0.5	dB
Continuous time filter, zero frequency for $g_{DC} = 0$	$f_z$	<del>12.58</del>	GHz
Continuous time filter, pole frequencies	$f_{p1}$ $f_{p2}$	<del>20</del> <del>28</del> $f_b$	GHz GHz
Continuous time filter, low-frequency pole/zero	$f_{LF}$	$f_b / 40$ 80	GHz

# Planned next steps

- Run EH/VEC simulations on candidate channels with/without the proposed change, and provide results
  - Pointing out candidate channels would be appreciated
  - If anyone has an automated test suite for this, help would be appreciated

# Straw poll

- For the reference CTLE of Annex 120G:
  - A. I would support the proposed change if it does not degrade VEC/EH compared to the current parameters.
  - B. I would support the proposed change if it improves VEC/EH compared to the current parameters, and change the max VEC / min EH accordingly.
  - C. I am interested in the proposed change but some modifications are required.
  - D. I would not support any change.
  - E. I need more information.
  - F. I don't have an opinion.
- (choose one)