C/ 45 SC 45.2.1.6 P21 L10 C/ 167 SC 167.5.7 P49 Dawe, Piers Nvidia Bruckman, Leon Huawei Comment Status X Comment Status D Comment Type Ε Comment Type E PMD global transmit disable disables all lane's transmitters. Rubric needs revising for basis of 802.3dc SuggestedRemedy SuggestedRemedy In bullet b) Replace: "turning off the optical transmitter in each lane.", with: "turning off the Per comment optical transmitter in all lanes." Proposed Response Response Status O Proposed Response Response Status W PROPOSED ACCEPT IN PRINCIPLE. CI 78 SC 78.1.4 P25 L22 # 42 C/ 167 SC 167.7.1 P51 Dawe, Piers Nvidia Swanson, Steven Corning Incorporated Comment Type E Comment Status D Comment Type TR Comment Status R Here, the order of 100GBASE-SRn PHY types is 4 2 10 1. In Table 80-1, it's 10 2 4 1. In There has been no contributions that prove that the inclusion of 940nm VCSELs will Table 80-4, 10 4 and Table 80-5, 1 2. This seems inconsistent. increase market potential and leverage the high volume manufacturing infrastructure SugaestedRemedy currently supplying 3D sensing applications. The VCSELs used for 3D sensing are not Consider what the order should be, bearing in mind that "100 m" doesn't mean exactly the suitable for the IEEE 802.3db application and the added complexity of the receiver does not same thing for the different PHYs, make changes to the order if appropriate. warrant the inclusion of another wavelength. Proposed Response Response Status W SuggestedRemedy PROPOSED ACCEPT IN PRINCIPLE. Change the center wavelength specification from 842-948 to 844-863. Review these tables in light of latest 802.3dc draft and reorder as appropriate. Response Response Status C

REJECT.

Reviewed the accompanying presentation. swanson 3db 01 090921.pdf.

The center wavelength (range) was discussed in the comment resolution against D1.1. The decision, after weighing the pros and cons, was to set the center wavelength range to 842 -948 nm for VR.

C/ 167

SC 167.7.1

L9

L15

# 45

# 68

Based on a straw poll, decision is to leave the center wavelength range for VR links as 842 - 948 nm.

SORT ORDER: Clause, Subclause, page, line

CI 167 SC 167.7.1 P51 L15 # 1
Abbott, John Corning Incorporated

Comment Type TR Comment Status D

In Table 167-7 Transmit Characteristics the goal for the VR option is to be a low cost option for connections to the server. This was fully summarized in the original CFI for the project. In order to optimize VR for this new market opportunity using existing OM3 and OM4 fiber (optimized for performance at 850nm) we need to balance all options. It makes sense to broaden the wavelength range for VR from 842 to 865 (wider than SR) to make the VR transmitters as low cost as possible, but it is not at all clear that using transmitters at 940nm which need to match a lower fiber BW can match those at 850nm. This comment agrees with basic point of comment 70 of D1.1 that the VR wavelength range should be centered around 850nm (the design wavelength for the fiber).

#### SuggestedRemedy

Change 842 to 948 to 824 to 865 (2nm wider than SR on both sides)

#### Proposed Response Response Status W

Review the accompanying presentation, swanson\_3db\_01\_090921.pdf.

#### PROPOSED REJECT.

The center wavelength (range) was discussed in the comment resolution against D1.1. The decision, after weighing the pros and cons, was to set the center wavelength range to 842 - 948 nm for VR.

Cl 167 SC 167.7.1 P51 L16 # 69

Swanson, Steven Corning Incorporated

Comment Type TR Comment Status R

In the transmitter specification, the only difference appears to be the spectral width of the source. This is offset by a more complex receiver.

In addition, in the CFI for this project, we identified two distinct market needs, one to support the shift from ToR to MoR/EoR architectures, requiring longer, low cost server-attachment links and another support 100G/optical lane to match to emerging 100G SerDes.

100GBASE-SR1, 200GBASE-SR2 and 400GBASE-SR4 variants seem to address the second requirement but it is not clear that the 100GBASE-VR1, 200GBASE-VR2 and 400GBASE-VR4 address the first.

Use cases included SFP112 connections to for next-generation servers, costs at 50% of DR and power consumption at 50% of DR.

I have seen no evidence that VR will support any of these use cases.

#### SuggestedRemedy

Consider eliminating the VR variants completely; the complexity of supporting two port types with little difference in the cost or power makes no sense. And the VR variant has no chance of competing for server-attachment links.

Response Status C

REJECT.

Reviewed the accompanying presentation, swanson\_3db\_01\_090921.pdf.

The VR link (50m OM4 reach) was voted in motions #3 and #4 in Jan 2020.

It was also supported by an expert associated with an end user, shen 3db 01a 110520.pdf, during the discussion for the SR link (100m OM4 reach).

C/ 167 SC 167.7.1 P51 L16 # C/ 167 SC 167.7.1 P51 L28 Abbott, John Corning Incorporated Dawe, Piers Nvidia Comment Status D Comment Status D Comment Type Т Comment Type Spectral Width of VR is specified as 0.65nm. If we are looking to make 940nm option as There are two competing definitions for OMA (min) in this table. We need to explain what low cost as possible does it make sense to have a wider spectral width spec at 940nm? Or the reader is supposed to do with them. if we tighten the wavelength range back to 842-863nm can we make 850nm VCSELS SuggestedRemedy easier to make with an even wider spectral width? One way would be to use max(TECQ, TDECQ). This applies in the text and Figure 167-3 SugaestedRemedy If line 15 is 842 to 948 increase spectral width at 948 to 0.70. If line 15 is 842 to 863. Proposed Response Response Status W increase spectral width at 850nm to 0.70 PROPOSED ACCEPT IN PRINCIPLE. Proposed Response Response Status W PROPOSED REJECT. Combine the two Outer OMA, each lane (min) to one: Max RMS spectral width specification is a balance: (a) Relax value to maximize VCSEL Outer OMA, each lane (min) for max(TECQ, TDECQ) <= 1.8 dB vield, and (b) Place more burden on the receiver by lowering fiber bandwidth. -2.6 dBm for 1.8 < max(TECQ,TDECQ) <= 4.4 dB -4.4 + max(TECQ,TDECQ) A maximum of 0.65 nm for RMS spectral width is a good balance. C/ 167 SC 167.7.1 P51 L31 # 66 C/ 167 SC 167.7.1 P**51** L25 # 28 Palkert, Tom Macom Dawe, Piers Nvidia Comment Type TR Comment Status X Comment Type Т Comment Status A Based on changes made to sampling window the TDECQ for VR can be improved In general, merging cells with the same content improves readability. Here, the limits for SuggestedRemedy VR and SR look the same but they aren't, because TDECQ means two different things. Change TDECQ for VR from 4.4 to 4.0 dB SugaestedRemedy Proposed Response Response Status O Spell out the entries for VR and SR separately for this row and the next three. Response Response Status C ACCEPT IN PRINCIPLE. Make separate columns in Table 167-7 for the entries for VR and SR links according to the suggested remedy.

L27

P51

During D1.1 recirculation we changed threshold adjust from +/-1% to +/- 2% with this

Comment Status X

Response Status O

Ghiasi Quantum/Marvell

C/ 167

Ghiasi, Ali

Comment Type TR

SuggestedRemedy

Proposed Response

SC 167.7.1

change the TDECQ will improve somewhat

Suggest to make TDECQ for both SR/VR=4.1 dB See ghiasi db 01 0921 for TDECQ measurements

C/ 167 SC 167.7.1 P51 L35 # 49 C/ 167 SC 167.7.1 P51 L44 Lingle, Robert **OFS** Ghiasi, Ali Ghiasi Quantum/Marvell Comment Type Comment Status X Comment Type Comment Status D TR TR The overshoot/undershoot parameter is currently TBD. Although, it is expected that At 50G some end users had to use APC cable plants due to reflections and in the 802.3db quidance from measurements will be available later in 2021, we have quidance from we have now added the option of APC connectors. If reflections are becoming an issue 802.3cu that a value of 22% protects the receiver sufficiently from over-peaked signals. why are we promoting 12 dB glass-air termination! SuggestedRemedy SuggestedRemedy Replace TBD for VRn and SRn PMD types with 22%. The purpose of the Suggest adding 20 dB transmitt reflectance to the table and suggest to change optical return loss tolerance to 15 dB Overshoot/Undershoot spec is to protect the Rx from problematic signals from an overly pre-emphasized Tx. A very high value will penalize the Rx; a very low value will Proposed Response Response Status W unnecessarily penalize the Tx. 802.3cu determined that 22% was a reasonable balance for PROPOSED REJECT. SMF Tx. Data on VCSEL Tx later in 2021 may allow refinement, but 22% is a very Installations with PC fiber termination may not meet the maximum 15 dB return loss. reasonable value. Proposed Response Response Status O C/ 167 SC 167.7.1 P51 L45 Ghiasi. Ali Ghiasi Quantum/Marvell Comment Status X Comment Type TR P51 C/ 167 SC 167.7.1 L37 # 13 Encircled flux Greater-less than and less than match symbols show up nu and Omega with Ghiasi, Ali Ghiasi Quantum/Marvell Preview but its fine if viewed with Acrobat DC Comment Type TR Comment Status X SuggestedRemedy Transmitter excursion need a reference This seem to be an issue with FM16 that require a different way to create PDF to avoid SuggestedRemedy these issues Please refernece 167.8.8 Proposed Response Response Status O Proposed Response Response Status O SC 167.7.1 P**51** L44 C/ 167 Ghiasi Quantum/Marvell Ghiasi. Ali Comment Status X Comment Type TR Overshoot is TBD SuggestedRemedy Replace TBD overshoot with 20% See ghiasi\_db\_01\_0921 for the overshoort measuremetns

Response Status O

Proposed Response

As the channel or signal is relatively slower than for any other optical PMDs so far, we should expect higher Ceq, contributing to TDECQ, but we should not expect higher K because we have 9 taps rather than 5, and 2% threshold adjust rather than 1%. We expect that "false negatives" won't be such an issue with 2% threshold adjust, and we can set the limits closer to what we really want, with less padding for measurement issues. We should re-optimise the spec considering these things, encouraging good equalisable signals both after and before the fibre. Overshoot/undershoot should be a useful additional protection eventually but it's still evolving, and the K limit can catch some bad transmitters that it misses - and K is a free by-product of TDECQ, K' is a free by-product of TECQ. The K limit is similar to VEC in C2M and EVM in coherent: a screen for signals that are bad after equalisation.

# SuggestedRemedy

Insert rows for K'=TECQ-10.log10(Ceq') and K=TDECQ-10.log10(Ceq), limit 4 dB. For both VR and SR.

Proposed Response Status O

Cl 167 SC 167.7.1 P51 L48 # 50
Lingle, Robert OFS

Comment Type ER Comment Status X

An editor's note was added to TDECQ(max) value to indicate that some TF members preferred a slightly lower value, and to encourage further study on the next draft. Either a compelling reason to change TDECQ(max) from 4.4dB to another value within the cited range will be brought into CR on D1.2, resulting in a parameter value change, or it will not.In either case, this value can be adjusted during comment resolution as the draft progresses through WG ballot as well. There is no need to keep this editor's note in future drafts.

#### SuggestedRemedy

Remove this editor's note

Proposed Response Status O

Cl 167 SC 167.7.2 P52 L40 # 3\_\_\_\_\_\_Abbott, John Corning Incorporated

Comment Type TR Comment Status D

To achieve orignal VR objections for a low cost high data rate connection to the server, restore the receive wavelength range to 842-863; if increasing the range to make VR 850nm transceivers more robust and cost effective for short distance, increase this to 842-865nm. Choose the wavelength range for VR transmitter and receiver based on end user requirements in the data center.

### SuggestedRemedy

Change 842 to 948 to 824 to 865 (2nm wider than SR transmitter on both sides) for VR and SR  $\,$ 

Proposed Response Response Status W

#### PROPOSED REJECT.

The center wavelength (range) was discussed in the comment resolution against D1.1. The decision, weighing the pros and cons, was to set the center wavelength range to 842 - 948 nm for VR.

For SR, the center wavelength range is 844 - 863 nm.

Cl 167 SC 167.7.2 P52 L40 # 70

Swanson, Steven Corning Incorporated

Comment Type TR Comment Status D

The requirement on the receiver to support a center wavelength range of 842-948 complicates the receiver design and adds cost. It will require an AR coating, and while some claim it will not add cost, it is not trivial.

#### SuggestedRemedy

Change the center wavelength specification from 842-948 to 844-863.

Proposed Response Status W

Review the accompanying presentation, swanson\_3db\_01\_090921.pdf.

#### PROPOSED REJECT.

The center wavelength (range) was discussed in the comment resolution against D1.1. After weighing the pros and cons including the requirement of a wide band AR coating on the photodiode, the decision was to set the center wavelength range to 842 - 948 nm for VR.

C/ 167 SC 167.7.2 P**52** L44 # 11 C/ 167 SC 167.7.2 P53 L7 Ghiasi, Ali Ghiasi Quantum/Marvell Ghiasi, Ali Ghiasi Quantum/Marvell Comment Type Comment Status X Comment Status X TR Comment Type TR At 50G some end users had to use APC cable plants due to reflections and in the 802.3db During D1.1 recirculation we changed threshold adjust from +/-1% to +/- 2% with this we have now added the option of APC connectors. If reflections are becoming an issue change the TDECQ will improve somewhat and associated SECQ will be lower why are we promoting 12 dB glass-air termination! SuggestedRemedy SuggestedRemedy Suggest to make SECQ for both SR/VR=4.1 dB See ghiasi db 01 0921 for TDECQ measurements Suggest adding 20 dB receive reflectance to the table and suggest to change optical return loss tolerance to 15 dB Proposed Response Response Status O Proposed Response Response Status W PROPOSED REJECT. Installations with PC fiber termination may not meet the maximum 15 dB return loss. P53 C/ 167 SC 167.7.2 L16 Dawe, Piers Nvidia C/ 167 SC 167.7.2 P**52** L51 Comment Type T Comment Status D Ghiasi. Ali Ghiasi Quantum/Marvell "Only applies to 200GBASE-VR2, 400GBASE-VR4, 200GBASE-SR2 and 400GBASE-Comment Type TR Comment Status X SR4": it's not "applies" that should be qualified by "only". Also, consider "alien crosstalk" in Encircled flux Greater-less than and less than match symbols show up nu and Omega with a multilane module operating as single-lane PMDs. Preview but its fine if viewed with Acrobat DC Anyway, we have subclause 167.8.13 defining stressed receiver sensitivity, where the same point is made. SuggestedRemedy SuggestedRemedy This seem to be an issue with FM16 that require a different way to create PDF to avoid these issues If making an editorial improvement, change to: Applies to 200GBASE-VR2, 400GBASE-VR4, 200GBASE-SR2 and 400GBASE-SR4 only. Proposed Response Response Status O or much better and in preparation for 800GBASE-VR8 and 800GBASE-SR8. Not applicable to 100GBASE-VR1 and 100GBASE-SR1. Or, because the same module suffers the same crosstalk if used as 4 x 100GBASE-VR1 C/ 167 SC 167.7.2 P**52** L51 # 67 as when running as 1 x 400GBASE-VR4, remove the exception. Anyway, because this topic is addressed in 167.8.13 and we should not be defining things Palkert, Tom Macom piecemeal by table footnotes - delete the note. See another comment against 167.8.13. Comment Type TR Comment Status X Proposed Response Response Status W If TDECQ for VR is changed to 4.0. SECQ needs to match. PROPOSED ACCEPT IN PRINCIPLE. SuggestedRemedy Change SECQfrom 4.4 to 4.0 Delete footnote e in Table 167-8. Proposed Response Response Status 0 Review the decision along with comment #41 at the next comment resolution session (Sep 20).

CI 167 SC 167.7.3 P53 L14 # 4
Abbott, John Corning Incorporated
Comment Type TR Comment Status D

In Table 167-9 Illustrative Power Budget if the VR wavelength range is 842-948 the power budget should be executed at 842 and 948nm. The table uses 850nm (which makes sense) but do we need a presentation with power budget at 948nm? Do we need a separate 948nm column?

#### SuggestedRemedy

Suggested remedy is to leave table 167-9 as is and change table 167.7.1 (transmitter) to 842 to 863nm. 2nd option is to modify table 167-9 to include subcolumns under OM3 and OM4 for power budgets at 940 using IEC guidance EMBs and putting TBDs in the rest of the items

Proposed Response Status W

PROPOSED ACCEPT IN PRINCIPLE.

Table 167-9 can be expanded for each wavelength band for VR.

C/ 167 SC 167.7.3 P54 L45 # 36

Dawe, Piers Nvidia

Comment Type E Comment Status A

As far as I can see, Figure 167-5 presents the same information as figure 167-3 and 167-4, but does it better because the information is on a single graph so one can see the relation between transmit and receive OMAs.

# SuggestedRemedy

Delete 167-3 and 167-4, move 167-5 to become 167-3 and refer to it instead of the existing 167-3 and 167-4.

Response Status C

#### ACCEPT IN PRINCIPLE.

Keep Figure 167-5 and eliminate Figures 167-3 and 167-4. Update the references to the figures.

Implement with editorial license.

We specify that each lane has the min OMA and max TDECQ or better, and we specify SRS at min OMA and max TDECQ. The PCS distributes 10-bit symbols across the PAM4 lanes and MSB/LSB equally, so what matters is the aggregate of errors on all the lanes. Specifying this for the receiver, we will still exceed the spec in practice because of scatter on transmit parameters. Clauses 86 and 95 and the copper PMDs have this right.

### SuggestedRemedy

Change from "Stressed receiver sensitivity is defined for each lane at the BER specified in 167.1.1." to "Stressed receiver sensitivity is defined for an interface at the BER specified in 167.1.1. The interface BER is

the average of the BERs of the receive lanes when they are stressed."

After "operated as specified.", insert "To find the interface BER, the BERs of all the lanes when stressed are averaged."

In 167.8.13, delete "The BER is required to be met for each lane under test on its own."

Response Status C

ACCEPT IN PRINCIPLE.

Implement the suggested remedy with editorial license.

The case of breakout was discussed. As an example, 400GBASE-SR4 is considered a single interface, and breakout is considered a separate application. Breakout is not defined in Clause 167.

C/ 167 SC 167.8.5 P40 L13 # 54 C/ 167 SC 167.8.5 P57 L31 # 38 Tang, Yi Cisco Systems, Inc. Dawe. Piers Nvidia Comment Status X Comment Status X Comment Type TR Comment Type "The TDECQ of each lane shall be within the limits given in Table 167-7 if measured using 151.8.5, TDECQ for 400GBASE-FR4 and 400GBASE-LR4-6, has this exception: the methods specified in 121.8.5." The normalized noise power density spectrum, N(f) in Equation (121-9), is equivalent to 8023-2018 121.8.5 (Page 135, Equation 121-9): The value of Ceq (coefficient for the white noise filtered by a fourth-order Bessel-Thomson response filter with a bandwidth of reference equalizer noise enhancement) can be calculated from N(f) and Heq(f) "Where 25.5625 GHz. N(f) is the normalized noise power density spectrum equivalent to white noise filtered by a SuggestedRemedy fourthorder I suppose this applies here, too. Bessel-Thomson response filter with a bandwidth of 13.28125 GHz." Issue: the noise enabncement relates to receiver noise, so its calculation shall be based on Proposed Response Response Status O reference receiver bandwidth. SuggestedRemedy Add to the exception list: C/ 167 SC 167.8.5 P**57** L32 # 51 "- The normalized noise power density spectrum, N(f) in Equation (121-9), is equivalent to **OFS** Lingle, Robert white noise Comment Status X filtered by a fourth-order Bessel-Thomson response filter with a bandwidth of 25.5625 Comment Type ER GHz." - same as 8023cu-2021 Editor's note states: "Noise handling in the fiber emulation and the fiber response is under further study." I hope that this topic can be addressed with both a comment & supporting Proposed Response Response Status O contribution in this draft cycle. Otherwise, I think the Editor's Note has served its purpose and can be removed at this point. This topic can still be addressed in WG ballot cycle if further information becomes available. C/ 167 SC 167.8.5 P**57** L20 # 43 SuggestedRemedy Dawe. Piers Nvidia Remove this editor's note Comment Type Comment Status D Т Proposed Response Response Status O Problems with "The first filter represents the system receiver": there's no definition of "system receiver", we should not be implying that a product receiver has to be like the TDECQ reference receiver, and a filter is only a small part of a receiver.

Change to "The first filter represents a receiver front end frequency response", or similar.

#### Proposed Response Response Status W

PROPOSED ACCEPT IN PRINCIPLE.

Implement with editorial license.

CI 167 SC 167.8.5 P57 L33 # 14

Ghiasi, Ali Ghiasi Quantum/Marvell

Comment Type TR Comment Status D

To speed up TDECQ measurement and for better correlation with real DSP suggest to use MMSE optimization over full grid search

SuggestedRemedy

Use MMSE optimization to determine the TDECQ.
Use of MMSE may slighlty increase +0.1 dB the TDECQ, for exact amount see chiasi dB 01 0921

Proposed Response

Response Status W

**DISCUSS** 

Clause 121.8.5.3 defines the TDECQ measurement method using TDECQ minimization as the optimization metric.

Any change must consider impact on

PMDs outside P802.3db.

MMSE method is faster and likely to be used in practice, especially with a 9 tap reference equalizer.

Text proposed by Greg Le Cheminant:

Pth1, Pth2, and Pth3 are varied from their nominal values by up to +/-1% of OMAouter "in order to minimize the closure of each eye using a minimum mean squared error optimization." The same three thresholds are used for both the left and the right histogram.

When the larger of SERL and SERR is equal to the target SER of 4.8 x 10<sup>4</sup>, and the value of sigma\_G cannot be increased by "further reduction of eye closure through optimization" of the equalizer tap coefficients or the sub-eye threshold levels, then TDECQ is calculated.

Editor's note states: "Use of minimum mean squared error optimization in place of optimization of TDECQ has been proposed." While this is an intriuging suggetion, I hope that this topic can be addressed with both a comment & supporting contribution in this draft cycle. Otherwise, I think the Editor's Note has served its purpose and can be removed at this point. This topic can still be addressed in WG ballot cycle if further information becomes available.

SuggestedRemedy

Remove this editor's note

Proposed Response Status W

See comment #14

Cl 167 SC 167.8.5 P57 L40 # 5
Abbott, John Corning Incorporated

Comment Type T Comment Status X

Table 167-12 the fiber emulation filter needs to model mutiple kinds of pulses with the same 3dB BW, including pre-pulses, post-pulses, dual-Dirac-Delta pulses. The worst case is likely a small pre or post pulse which whos 3dB BW is X but whose 1.5dB BW extrapolated to 3dB is X/2.

SuggestedRemedy

Verify worst case assumption used in TDECQ and compare to fiber minEMBc 1.5dB BW, particularly for VR at 948.

Proposed Response Response Status O

Cl 167 SC 167.8.13 P60 L12 # 41

Dawe, Piers

Nvidia

Comment Type

T

Comment Status X

Looking ahead to 800GBASE-VR8 and 800GBASE-SR8, this might be better stated as an exception. Anyway, what if a multilane module is running as multiple 100GBASE-VR1? Formally, it's "alien crosstalk" but it's just the same.

SuggestedRemedy

Proposed Response Response Status W

**DISCUSS** 

In section 167.8.13, suggest using "For a receiver in a multilane device" in place of "For 200GBASE-VR2, 400GBASE-VR4, 200GBASE-SR2 and 400GBASE-SR4"

Review the exact wording to be used at the next comment resolution session (Sep 20).

C/ 167	SC	167.10.2.1	P <b>63</b>	L <b>24</b>	# <u>7</u> 1	-
Swanson, Steven			Corning Incorporated			
Comment T	уре	TR	Comment Status D			•
		•	matic dispersion specificati		,	

OM3/OM4 and OM5. There is NO difference in the chromatic dispersion of these fibers. In fact the study that led to the specification of OM5 used OM3 and OM4 chromatic dispersion values to set the value for OM5.

A contribution has been submitted to correct this inconsistency in IEC and will be complete long before this standard is published.

# SuggestedRemedy

For OM3 and OM4, eplace 1295 </= lambda naught </= 1340 with 1297 </= lambda naught </= 1328

Replace 0.105 for 1295 </= lambda naught </= 1310 and 0.000375 Î (1590 û lambda naught) for 1310 </= lambda naught </= 1340 with û 412/(840(1 û (lambda naught/840)4))

#### Proposed Response Response Status W

PROPOSED ACCEPT IN PRINCIPLE.

C/ 167	SC 167.10.3.	3 P <b>65</b>	L <b>4</b>	# 72
Swanson, Steven		Corning Incorporated		
Comment	Type TP	Comment Status D		

The suggestion to support two options, Option A for angled physical contact fiber interface and Option B for flat physical contact fiber interface for the MDI requirement for 200GBASE-VR2,400GBASE-VR4, 200GBASE-SR2 and 200GBASE-SR4 is a bad idea and will cause problems in the market.

#### SuggestedRemedy

Pick one, either angled or non-angled but not both.

Proposed Response Response Status W

PROPOSED REJECT.

This comment is similar to comment #74 against Draft 1.1.

The response to that comment included, "Option B was included in case non-angled connectors are needed by large enterprise end users in the future."

Option A is included based on contributions xie\_3db\_01\_051321, shen\_3db\_01a\_110520, and parsons\_3db\_adhoc\_01\_062520

C/ Front m SC Front matte	er <i>P</i> 17	L <b>48</b>	# 15
Dawe, Piers	Nvidia		
Comment Type E	Comment Status X		
These examples, P802.3	bj and IEEE P802.3bk, a	re history now.	
SuggestedRemedy			
Change to the list of post including cw and ck; this		erlap with this one	e, as best we know it,
Proposed Response	Response Status O		

C/ Front m